TECHNICAL REPORT ON MINERAL RESOURCE ESTIMATE

GETTY ZINC - LEAD DEPOSIT GAYS RIVER AREA HALIFAX COUNTY, NOVA SCOTIA NTS 11E03B

Prepared For: ACADIAN MINING CORPORATION Prepared By: Mercator Geological Services Limited

Effective Date: December 12, 2007



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Prepared By: Michael P. Cullen, M.Sc., P. Geo, Chrystal Kennedy, B. Sc.(Hons.), P.Geo., Matthew Harrington B. Sc. (Hons.) Mercator Geological Services Limited Effective Date: December 12, 2007

Report Date: March 25, 2008



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Summary

The Getty zinc-lead deposit is held by Acadian Mining Corporation (Acadian) under terms of a Special Exploration Licence issued by the Province of Nova Scotia in 2007. The deposit is located in the Musquodoboit Basin of central Nova Scotia, Canada and is adjacent to Acadian's Scotia Mine zinc-lead deposit. Scotia Mine currently produces approximately 2200 tonnes per day from open pit operations and entered production in May, 2007. Mercator Geological Services Limited (Mercator) was retained by Acadian in 2007 to review and validate results of previous diamond drilling on the Getty property and to use this information as the basis for a resource estimate compliant with Canadian Institute of Mining, Metallurgy and Petroleum Standards for Mineral Resources and Reserves and disclosure requirements of National Instrument 43-101.

The Getty deposit was discovered in 1972 through diamond drilling by Getty Mining Northeast Limited (Getty) and forms an extension to the adjacent Scotia Mine zinc-lead deposit at Gays River. Both deposits are hosted by dolomitized carbonate banks of the Carboniferous Windsor Group's Gays River Formation. These banks developed along basement highs or ridges near the paleo-basin margin and were overstepped by interbedded evaporites, carbonates and siliciclastic rocks that comprise younger Windsor Group stratigraphy.

Results of the resource estimate completed by Mercator are presented in Table 1 below and are in accordance with CIMM Standards and disclosure requirements of National Instrument 43-101.

| Table 1: Mineral Resource Estimate for Getty Deposit – December 12 th , 200 | 07 |
|--|----|
|--|----|

| Resource Category | Equivalent Zn% Threshold* | Tonnes (Rounded) | Lead % | Zinc % | Zinc% + Lead % |
|----------------------|------------------------------|------------------|--------|--------|----------------|
| Inferred | 2.00% | 4,160,000 | 1.40% | 1.81% | 3.21% |
| Inferred | 2.50% | 2,860,000 | 1.60% | 2.06% | 3.66% |
| Inferred | 3.00% | 1,970,000 | 1.82% | 2.26% | 4.08% |

*Note: Zn Equivalent calculated as Zn Equivalent = (Zn% + Pb%) based on averaged July to October 2007 zinc and lead market pricing

The deposit is defined by 184 historic drill holes of 1970's vintage, 181 of which were completed by Getty and three of which were completed by Imperial Oil Limited (Esso). The current resource outline includes 68 of these holes. The deposit is located approximately 700 metres west of Acadian Mining's Scotia Mine complex and is comprised of zinc-lead mineralization similar to that present at Scotia Mine, this being predominantly disseminated to locally sub-massive sphalerite and galena occurring within dolomitized carbonate.

The Mercator estimate is based on a three dimensional block model developed using Surpac© Version 6.01 modelling software and validated results for the 184 historic diamond drill holes. The model utilizes 1 meter down-hole assay composites of lead and zinc values that were calculated from drill hole database records. Model blocks are 2.5 meters x 2.5 meters x 2.5 meters with sub-blocking at 1.25 meters x 1.25 meters x 1.25 meters. The block model is coordinated to Acadian's local Scotia Mine Grid and extends from 6000 meters East to 7145 meters East, from 6450 meters North to 7150 meters North and from the 150 meter grid elevation to the 700 meter grid elevation. Zinc and lead grades were assigned to the block model using inverse distance squared (ID²) interpolation methodology completely constrained within a wire-framed resource solid developed from interpretation of geological sections and associated assay data. The wireframed solid reflects limits of assay defined mineralization occurring within the hosting dolomitized carbonate bank. An omni-directional search ellipse with a range of 100 meters was used for block grade interpolation and a maximum of 21 sample composites was established for estimation of individual block grades, with no more than 7 composites coming from a single drill hole. No drill hole limit was established for block assignment. Specific gravity (SG) values for blocks were calculated from associated composite grades using the formula SG = 1 / (Pb% / (86.6 * 7.6) + Zn% / (67.0 * 4.0) +(1 - Pb % / 86.6 - Zn % / 67.0) / 2.7), which was recently used by MineTech International Ltd. (Roy et. al., 2006) for resource and reserve estimation purposes at the adjacent Scotia Mine. The zinc equivalent calculation was based on averaged market values over the period July 2007 through October 2007.

The deposit model was checked against grade plans and sections and also using Nearest Neighbour grade interpolation, all of which returned acceptable results. Four diamond drill holes were also completed by Acadian to twin historic holes within the resource outline. Results from these holes correlated acceptably with the historic holes as did core sampling results for one Getty drill hole that was re-sampled by Mercator during the course of the resource estimation and data validation program.

Infill drilling has been recommended for the deposit to establish a nominal hole density of 50 meters by 50 meters to support definition of higher order mineral resources. At the effective date of this report Acadian was advancing a +100 hole diamond drilling program to meet this end. Results of recent exploration by Acadian west of Getty, in the Carrolls Farm area, are interpreted as indicating presence of a continuous series of mineralized carbonate banks extending to the southwest from the Getty deposit's west flank. Potential for an additional mineralized bank also exists to the northwest of the deposit and in both instances airborne magnetometer survey results support target

definition. Core drilling investigations have been recommended for both areas, with the southwest extension opportunity being best defined and of highest priority.

1

1.0 Introduction and Terms of Reference

This report on estimation of mineral resources for the Getty zinc-lead deposit, located in central Nova Scotia, Canada, was prepared by Mercator Geological Services Limited (Mercator) on behalf of Acadian Mining Corporation (Acadian). The resource estimate was prepared in accordance with disclosure requirements set out under National Instrument 43-101 and is considered compliant with Canadian Institute of Mining, Metallurgy and Petroleum Standards for Mineral Resources and Reserves *Definitions and Guidelines (CIMM Standards)*. Terms of reference were established through discussions between Acadian and Mercator in early 2007 at which time it was determined that the resource estimate was to be based upon historical diamond drilling data that had been digitally compiled by previous holders of the property. This database was to be validated by Mercator prior to use in the resource estimation process.

Historic exploration reports and previous resource estimates pertaining to the property were first compiled by Mercator from records stored at the Scotia Mine facility and from government assessment record archives. This field of information included drill logs with assay information and drill plans completed by Getty Northeast Mines Limited (Getty) and Imperial Oil Limited (Esso) in the 1970's. Mercator also designed and implemented a core drilling program for the Getty deposit, on Acadian's behalf, that was in progress at the report date, and is responsible for associated core logging, sampling, quality control and quality assurance procedures. With the exception of 2 validation drill holes completed in 2007, results of the on-going drilling program are not reflected in the current resource estimate.

All authors have met with Acadian staff with respect to the current Getty resource estimate and authors Kennedy and Cullen have visited the property on numerous occasions. Author Kennedy provides day to day project supervision for the current Acadian drill program and Cullen, Harrington and Kennedy are responsible, in conjunction with Acadian staff, for review and interpretation of data generated by the current drilling program.

2.0 Reliance on Other Experts

2.1 General

No other experts were relied upon with respect to preparation of this report.

2.1 Disclaimer

This report was prepared by Mercator for Acadian and information, conclusions and estimates contained herein are based upon information available to Mercator at the time of report preparation. This includes data made available by Acadian, as well as government and public record sources. Information contained in this report is believed reliable but in part the report is based upon information not within Mercator's control. Mercator has no reason, however, to question the quality or validity of data used in this report. Comments and conclusions presented herein reflect Mercator's best judgment at the time of report preparation. Mercator is not providing professional opinion with respect to mineral exploration titles, environmental liabilities, mineral property agreements or surface title issues.

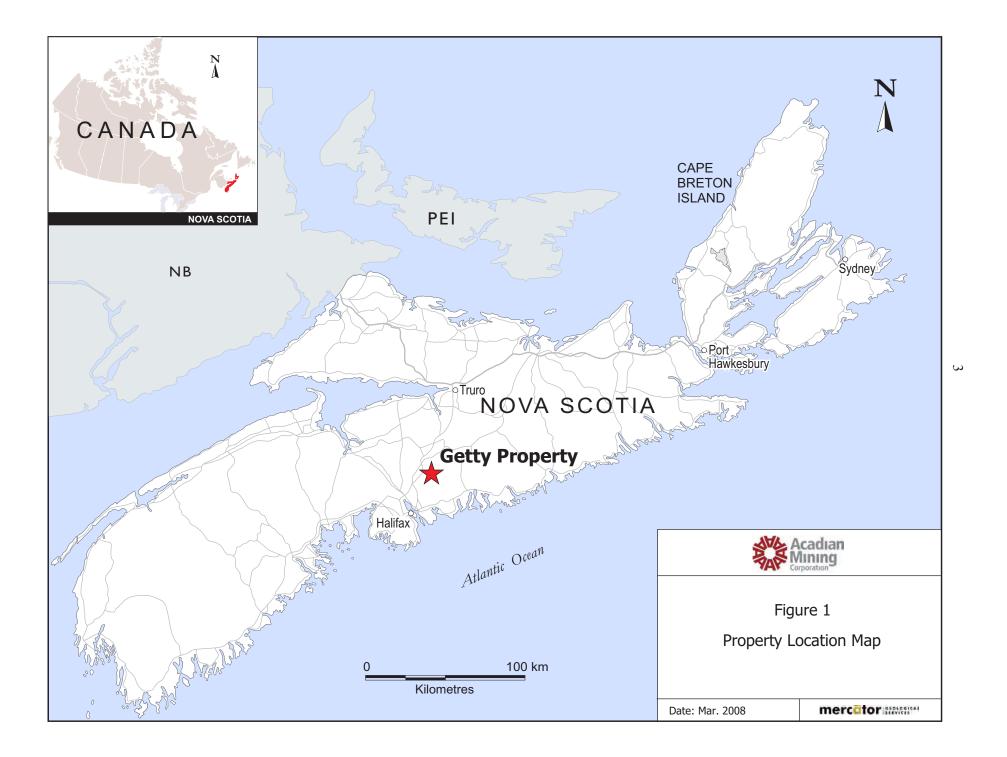
3.0 Property Description and Location

3.1 General

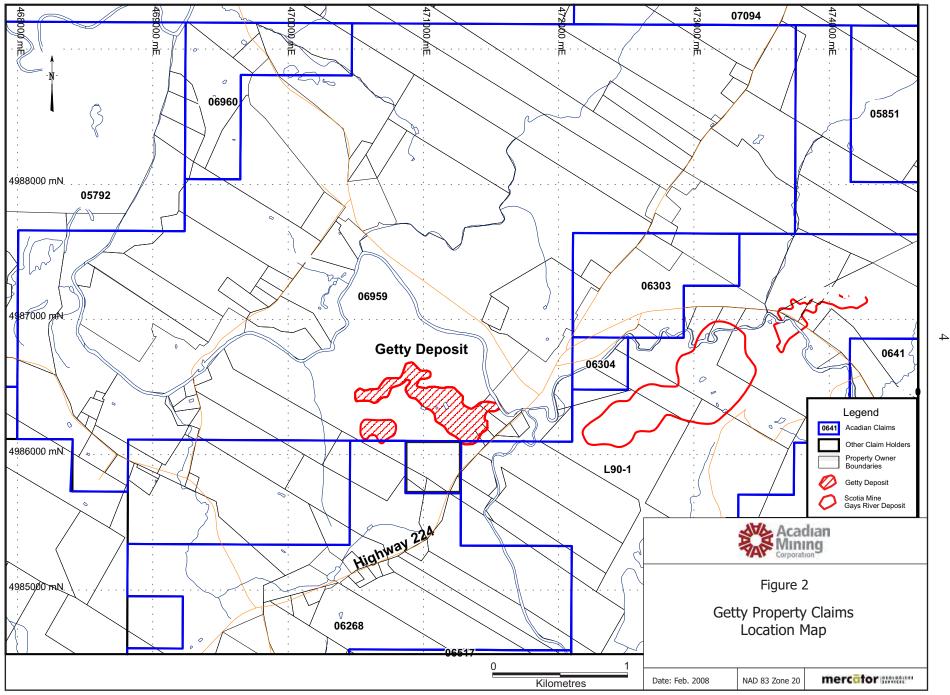
The Getty deposit is located at Gays River, Halifax County, approximately 45 kilometers northeast of the provincial capital city of Halifax. The area is directly accessible from paved provincial Highway 277 and is approximately 1700 meters northwest of Acadian's Scotia Mine complex (Figures 1 and 2).

The deposit occurs within Exploration Licence 6959 and Licence 6960 which were issued to Acadian on October 20th, 2006 as a result of tendering by Nova Scotia Department of Natural Resources (NSDNR). These licences include eighty-five claims that are further described in Table 2. They are part of a larger contiguous holding consisting of several Acadian exploration licences and mining titles.

In 1990 lands covering the deposit were placed under closure by NSDNR (1990, c. 18, s. 22; 1999 (2nd Sess.), c. 12, s. 6.) and these were subsequently opened for staking on September 12th, 2006. Multiple applications for exploration licences covering the deposit were received at that time by the Registrar of Mineral and Petroleum Titles, and all claims were therefore put up for tender under provisions of section 34 of the Act (1990, c. 18, s. 34.). Acadian Gold Corp., now Acadian Mining Corp., submitted the winning bid for this tender and was awarded the exploration licences detailed in Section 3.1, Table 2. Details of bids received and associated work requirements have been deemed confidential by the Minister of Natural Resources.







| Licence | No. Of | Claims Tract NTS Map | | Anniversary | |
|---------|--------|----------------------|------|-------------|-------------|
| No. | Claims | Claims | Hact | 1415 Wiap | Date |
| 6959 | 80 | ABCDEFGHJKLMNOPQ | 30 | 11E3B | 20-Oct-2008 |
| | | ABCDEFGHJKLMNOPQ | 31 | 11E3B | " |
| | | ABGHJKPQ | 32 | 11E3B | " |
| | | ABCGHJK | 42 | 11E3B | " |
| | | ABCDEFGHJKLMNOPQ | 43 | 11E3B | " |
| | | ABCDEFGHJKLMNOPQ | 44 | 11E3B | ٠. |
| 6960 | 5 | FLOPQ | 42 | 11E3B | " |

Table 2: Details of Getty Claim Group

At the effective date of this report both exploration licences described above were in good standing as represented in records of the Nova Scotia Department of Natural Resources. This assertion does not constitute a legal search of title by Mercator with respect to ownership or status of the licences, but Mercator has no reason to question their indicated status.

Acadian advised Mercator that surface rights to lands covering the Getty deposit are owned under separate titles by Allan Benjamin, David Benjamin and Heather Killen and that the company has established access agreements to these lands, as necessary, to allow exploration activities to be carried out. Mercator did not review the access agreements for purposes of this report but accepts that permission to enter the lands for exploration purposes has been established.

3.2 Agreement with Globex Resources Ltd.

Acadian advised Mercator that Licence 6960 and Licence 6959 that cover the Getty deposit, plus certain peripheral claims in the area, are subject to an agreement between Acadian and Globex Resources Ltd., dated October 10th 2006, that provides Globex with a 1% Net Smelter Return (NSR) royalty interest in the associated claims plus 25,000 shares. Agreement terms also allow Acadian to purchase 50% of the NSR for \$300,000 CDN. Mercator did not review or confirm terms of the Acadian-Globex agreement for purposes of this report.

3.3 Summary of Exploration Title And Regulatory Information

Mineral exploration licences in Nova Scotia are issued under the province's Mineral Resources Act (1990 and as subsequently amended) (the Act) and provide a licencee with exclusive right to explore for specified minerals within the licenced area, subject to terms

and conditions of the Act. Individual claims held under a mineral exploration licence measure 16.188 hectares in surface area (~forty acres) and are renewable on a yearly basis. No equivalence to "patented claim status" exists under the Act. Retention of claims in good standing from year to year requires filing of annual renewal fees and documents for each exploration licence as well as meeting minimum yearly work commitment and reporting requirements. Under normal circumstances, fees and minimum work requirements set out under provision of the Act vary according to the year of licence issue and are summarized in Table 3. Payment of cash in lieu of work on a claim or claims can be made once in any five year period.

Table 3: Standard Claims Renewal Fees and Work Requirements

| Year of Issue | Renewal Fee | Assessment Expenditure |
|---------------|--------------------|------------------------|
| 2 through 10 | \$10.68 per claim | \$200.00 per claim |
| 11 through 15 | \$21.36 per claim | \$400.00 per claim |
| 16 through 25 | \$85.44 per claim | \$800.00 per claim |
| 26 and beyond | \$170.88 per claim | \$800.00 per claim |

An exploration licence conveys an exclusive right to explore for named minerals but does not provide certainty with regard to land access or ownership of minerals. Access to lands is at the discretion of surface title holders and a Mining Lease or Special Mining Lease must be granted by the government to establish ownership of mineral resources for which production is planned. Mining activities can only be initiated after an Environmental Approval has been granted and various permits relating to industrial, environmental and engineering aspects of the proposed mining operation have been obtained.

As noted earlier, the claims that encompass the Getty deposit were previously under a closure (1990, c. 18, s. 22; 1999 (2nd Sess.), c. 12, s. 6.) but were opened for staking September 12, 2006. Subsequent to more than one application for exploration licence being received simultaneously by the Registrar of Mineral and Petroleum Titles (the Registrar), these claims were put up for tender under the provisions of section 34 of the Act (1990, c. 18, s. 34.). Acadian Gold, subsequently Acadian Mining submitted the winning bid and awarded the exploration claims detailed above in Section 3.1, Table 2. The details of the bids and work requirements have been deemed confidential by the Minister of Natural Resources at this time but it is appropriate to note that work requirements under terms of the successful bid substantially exceed those set out in Table 3 for exploration licences acquired under the normal staking process.

4.0 Accessibility, Climate, Physiography and Infrastructure

4.1 Accessibility

The property is located at Gays River, Halifax County, approximately 45 kilometers northeast of the provincial capital city of Halifax. The area is directly accessible from paved provincial Highway 277 and is approximately 1700 meters northwest of Acadian's Scotia Mine complex (Figure 2). Access to the Trans Canada Highway (Route 102) is possible at Enfield, approximately 15 kilometers to the west and Robert Stanfield International Airport is located twenty kilometres southwest of the mine site. On the property scale, access to the deposit area is excellent, being provided by several private roads, field access trails and forestry trails associated with land holdings that adjoin Highway 224 (Figure 2).

4.2 Climate

The property is situated in central Nova Scotia where northern temperate zone climatic conditions are present and are moderated by relative proximity to the Atlantic Ocean Distinct seasonal variations occur, with winter conditions of freezing and potentially substantial snowfall expected from late November through late March. Spring and fall seasons are cool, with frequent periods of rain. Summer conditions can be expected to prevail from late June through early September, with modest rainfall.

The following climate information reported for nearby Robert Stanfield International Airport during the 30 year period ending in 2000 characterizes seasonal precipitation and temperature trends in the area. The average July daily mean temperature for the reporting period was 18.6 degrees Celsius with a corresponding average maximum daily temperature of 23.6 degrees Celsius. Average daily winter temperature for January was minus 6 degrees Celsius with a corresponding average daily minimum being 10.6 degrees. Mean annual temperature is 6.3 °C, and mean annual precipitation is 1,452.2 mm. Climate conditions permit many exploration activities, such as core drilling and geophysics, to be efficiently carried out on a year-round basis. Other activities, such as geochemical surveys and geological mapping are typically limited by winter snow cover.

4.3 Physiography

Cleared farmland and intervening small woodlots characterize the property area and the north-flowing Gays River follows a prominent valley along the east and north sides of the property. A small north flowing stream also occurs near the west property boundary and lesser seasonal drainages are present locally. Maximum topographic relief is approximately 55 meters above the Gays River valley bottom which has an average

elevation in this area of approximately 10 meters above sea level (ASL). Most elevation change occurs along the narrow river valley corridor and rolling farmland with mixed forested areas is otherwise present. Almost all of the area underlain by the resource estimate consists of cleared farmland.

4.4 Infrastructure

The property area is rural and has been extensively development for agricultural purposes in the past. The largest local employers are an open pit gypsum mine and rail shipment facility operated by National Gypsum Limited at nearby Milford, and the Scotia Mine zinc-lead mining operation operated by Acadian on the adjoining property to the southeast. Forestry industry interests are also represented in the immediate area, which occurs entirely within the Halifax Regional Municipality. Access to mainline rail facilities is possible at nearby Enfield and direct access to deep-water shipping facilities with post-Panamax capacity is present through the ice-free deepwater port of Halifax. Year-round deep water access is also possible at the port of Sheet Harbour that is accessible via paved provincial highways and located 100 kilometers to the southeast of the Getty property.

Halifax is the provincial capital and in combination with surrounding communities forms a major center of population, government, business, education, industry and transportation services. Robert Stanfield International Airport is located approximately 20 kilometers southwest of the property and provides daily domestic and international airline service. Access to the regional electrical grid is also possible.

In summary, the Getty property is well positioned with respect to existing infrastructure and support services that could be beneficial to future mining at the site. The most significant infrastructure factor is direct proximity to Acadian's Scotia Mine complex, located approximately 1700 meters to the southeast.

5.0 History

5.1 Introduction

Records of intermittent lead and zinc exploration in the Gays River area date to the late 1800's and the following brief summary of exploration activities reflects information gathered from various assessment and open file reports obtained from the NSDNR archives. This chronological review of exploration history includes investigations that pertain to areas not included within the Getty deposit limits, as described in this report.

These were included to better illustrate character and results of exploration in the surrounding area.

5.2 Summary of Exploration Activities

Pertinent aspects of the area's history of exploration and economic assessment are summarized below and reflect review of assessment report and mineral occurrence file records archived at NSDNR as well as other public record information. Three historic mineral resource estimates are included in the summary and results of these are more fully considered in report section 5.3.

- First reports of zinc-lead mineralization in the Gays River area date to the late 1800's and from this time until the 1950's exploration consisted of limited amounts of mapping, pitting, trenching and sampling with up to 3% lead values being reported. Most activities focused on the area immediately around the adjacent Scotia Mine site, particularly along the South Gays River, where outcropping Gays River Formation dolomite hosting low grade zinc and lead mineralization was trenched and drilled in the 1950's in the "Gays River Lead Mines Area" (Campbell, 1952). However, with the exception of regional soil geochemical surveying by Pennaroya Ltd. in 1964 (Rabinovitch, 1967) that did not identify the Getty deposit, no substantial mineral exploration efforts appear to have been carried out on the current Getty property prior to it's acquisition by Getty in 1972.
- Exploration in the current deposit area was initiated in 1972 by Getty and joint venture partner Skelly Mining Corporation under terms of an option purchase agreement with Millmore-Rogers Syndicate. The adjoining Gays River property (now Acadian's Scotia Mine) was optioned by Imperial Oil Limited (Esso) and Cuvier Mines Limited (Cuvier) from Millmore-Rogers Syndicate at approximately the same time. The Esso-Cuvier property was immediately investigated by core drilling that ultimately resulted in definition of the Gays River zinc-lead deposit that was placed in production by Esso in 1978. Between 1978 and 1981, 554,000 tonnes of zinc/lead ore was mined with an average grade of 2.12% zinc and 1.36% lead (Roy et. al., 2006). Esso ceased production in 1982 after encountering substantial problems with both mining conditions and water inflows.
- Discovery of the Getty zinc-lead deposit is attributed to drill hole GGR-12 which was completed in 1972 and intersected 4.63 meters of dolomite grading 15.48% combined zinc-lead, beginning at a down hole depth of 93.11 meters. Subsequent

completion of over 200 holes by Getty and Imperial on and around the property served to delineate a nearly continuous mineralized zone measuring approximately 1300 meters in length and up to 200 meters in width (Comeau, 1973, 1974; Comeau and Everett, 1975).

- Getty retained MPH Consulting Limited (MPH) to assess three development scenarios for the deposit and Riddell (1976) reported results of this work, which showed that production of 375,000 tonnes per year would be necessary to support a viable, stand-alone open pit operation.
- In 1980 economic aspects of developing the deposit based on an in-house tonnage and grade model were assessed by Esso (MacLeod, 1980). This study concluded that mining through open-pit methods as an ore supplement to the Gays River deposit would be economically viable, provided that important operating assumptions were met. The earlier MPH work was also reviewed at this time and some economic models updated. None of the work indicated that profitable stand-alone development of the deposit could be expected under market conditions of the time. George (1985) subsequently reviewed earlier evaluations and also reached a negative conclusion.
- Claims covering the Getty deposit were placed under closure in 1987 by the Nova Scotia government and a tender was subsequently let for acquisition of exploration rights to the property. In 1990 Westminer Canada Limited (Westminer), was deemed the successful bidder and awarded a Special Exploration Licence for further assessment of the deposit.
- In 1992 Westminer completed a resource estimate and preliminary economic assessment of the deposit based on Getty drilling results, with potential development in conjunction with the adjacent Gays River deposit being considered (Hudgins and Lamb, 1992). Results showed that that milling of about 550 tonnes per day of Getty ore could be undertaken at a low cost if excess milling capacity was being filled by such material. Westminer also indicated that zinc oxide production from the deposit would result in a substantially better financial return to the mine in comparison with a conventional smelter contract for sulphide concentrates. Attempted renewals of the Getty Special Exploration Licence by Westminer for three consecutive years were not successful.
- Pasminco Resources Canada Company (Pasminco) acquired the adjacent Scotia Mine deposit and infrastructure in 1999 through purchase of Savage Resources Inc., and in 2000 Pasminco submitted an application to NSDNR for a Special

Mining Lease covering the deposit. No lease was issued and the closed status of the property was maintained.

- Between 1992 and September 2006 claims comprising the Getty property were maintained under government closure and no work was carried out on the property.
- In September, 2006 the provincial government tendered exploration rights to the closed Getty property and Exploration Licence 6959 and Licence 6960 were subsequently issued to Acadian on October 20th, 2006 as successful bidder under the tendering process.

5.3 Historic Mineral Resource or Reserve Estimates

Three historic estimates of tonnage and grade for in-situ mineralization comprising the Getty deposit are available in the public record. The earliest of these was prepared for Getty by MPH Consulting Limited (Riddell, 1976) and was revised in 1980 as part of a Mine Valuation Study carried out for Esso (MacLeod, 1980). Subsequently, Westminer developed an in-house resource estimate and preliminary economic assessment of the deposit, based on historic drilling results (Hudgins and Lamb, 1992).

Results of the historic estimates are presented below in Table 4 and all pertain to areas currently covered by Acadian exploration licences. These estimates pre-date National Instrument 43-101 and have not been classified under current Canadian Institute of Mining, Metallurgy and Petroleum Standards for Reporting of Mineral Resources and Reserves: *Definitions and Guidelines* (the CIMM standards). On this basis they should not be relied upon.

Table 4: Historic Tonnage and Grade Estimates for Getty Deposit

| Reference | Tonnes | Zn + Pb % | Zn % | Pb % |
|------------------------|-----------|-----------|------|------|
| Riddell(1976) | 4,470,400 | 3.71 | 1.87 | 1.84 |
| MacLeod(1980) | 3,149,600 | 2.97 | 1.60 | 1.37 |
| Hudgins and Lamb(1992) | 4,490,000 | 3.20 | 1.87 | 1.33 |

Riddell(1976) used a 2% (zinc% + lead%) cut-off, Macleod (1980) used 1.5% zinc cut-off and Hudgins and Lamb (1992) used a 1.5% zinc-equivalent cut-off defined as zinc equivalent = zinc% +(lead % x 0.60). The Riddell (1976) and MacLeod (1980) estimates reflect drill-hole-centered polygonal methods of volume estimation along with subjectively determined specific gravity factors reflecting general experience. Both estimates include length-weighted drill hole grade assignments to polygons with

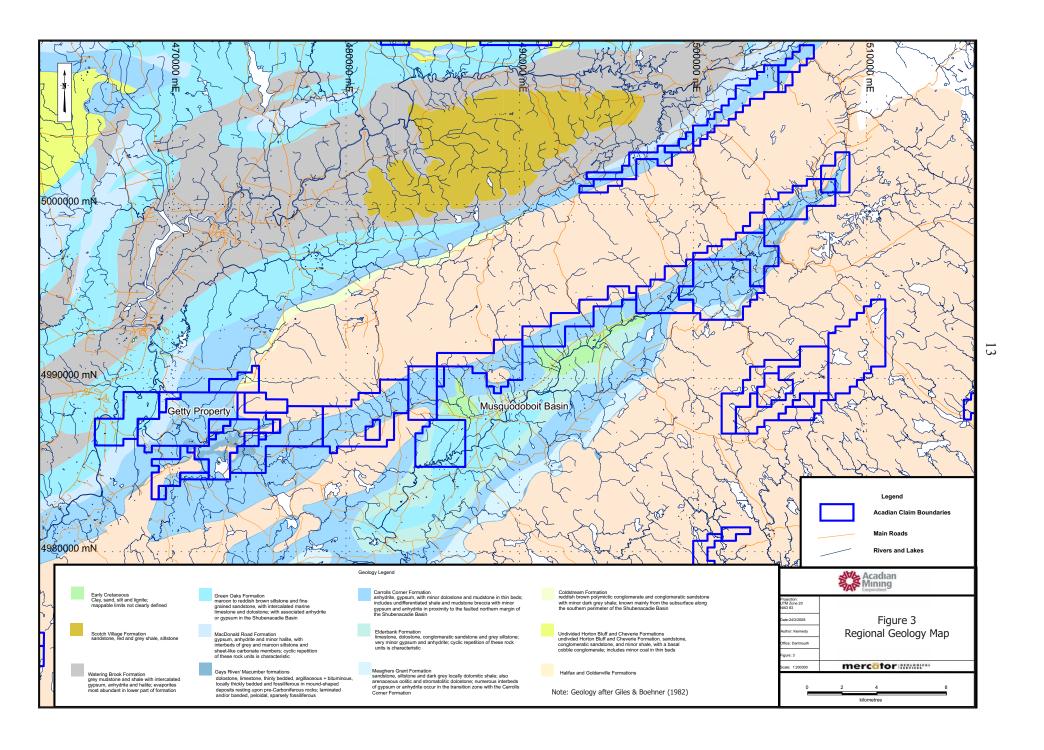
subsequent tonnage-weighting to determine deposit grades. In contrast, Hudgins and Lamb (1992) used Surpac© deposit modeling software, a cross sectional method of volume estimation, a single assigned specific gravity factor of 2.75 g/cm³ and calculated average deposit zinc and lead grades as the length-weighted averages of all qualifying drill hole intercepts. Further discussion of these resource estimates and related programs directed toward economic viability assessments appears in section 16.4 of this report.

6.0 Geological Setting

Carboniferous age sedimentary sequences in central Nova Scotia occur near the current southern margin of the extensive Maritimes basin, development of which began after the mid-Devonian Acadian Orogeny (Figure 3). Northeast trending faulted sub-basins evolved over much of the current central Nova Scotia area, where sedimentation from latest Devonian through Mississippian time was initially terrigenous clastic in nature, evolving to mixed marine carbonates, evaporites and clastics. Horton Group rocks record the early terrigenous and lacustrine clastic phase of deposition while overlying Windsor Group rocks record multiple transgressive-regressive marine depositional cycles. Pennsylvanian sedimentation marks further evolution of the Maritimes basin to predominance of clastic fluvial /lacustrine or shallow marine clastic conditions (Fralick and Schenk, 1981).

The Getty deposit is hosted by lower Mississippian age dolostone of the Windsor Group's Gays River Formation. Well defined carbonate banks characterize this formation and in most instances are associated with well-defined paleo-basement high features. On depositional basin scale, Gays River Formation bank carbonates and laminated limestone of the laterally equivalent Macumber Formation mark the onset of marine depositional conditions after a prolonged period of predominantly terrigenous clastic sedimentation represented by Horton Group siliciclastic rocks.

Carboniferous strata in Central Nova Scotia occur within the Shubenacadie and Musquodoboit sub-basins of the larger Maritimes basin and were described by Giles and Boehner (1982). Geometry of both sub-basins was significantly influenced by strong northeast trending structural grain in basement sequences of the Cambro-Ordovician Meguma Group. Deformation was heterogeneously distributed across the sub-basins and at present is now represented by northeast trending normal and thrust faults which are locally associated with open to moderately folded structural domains. Deformation features are essentially absent near the southern margins of the basins but become more prevalent and pervasive toward the northern limits, where effects of the regionally significant Cobequid-Chedabucto fault system are represented.



Minor faults or fracture zones may be present at Getty but no structural complexity is evident in either the surface morphology or drill logs.

7.0 Deposit Geology

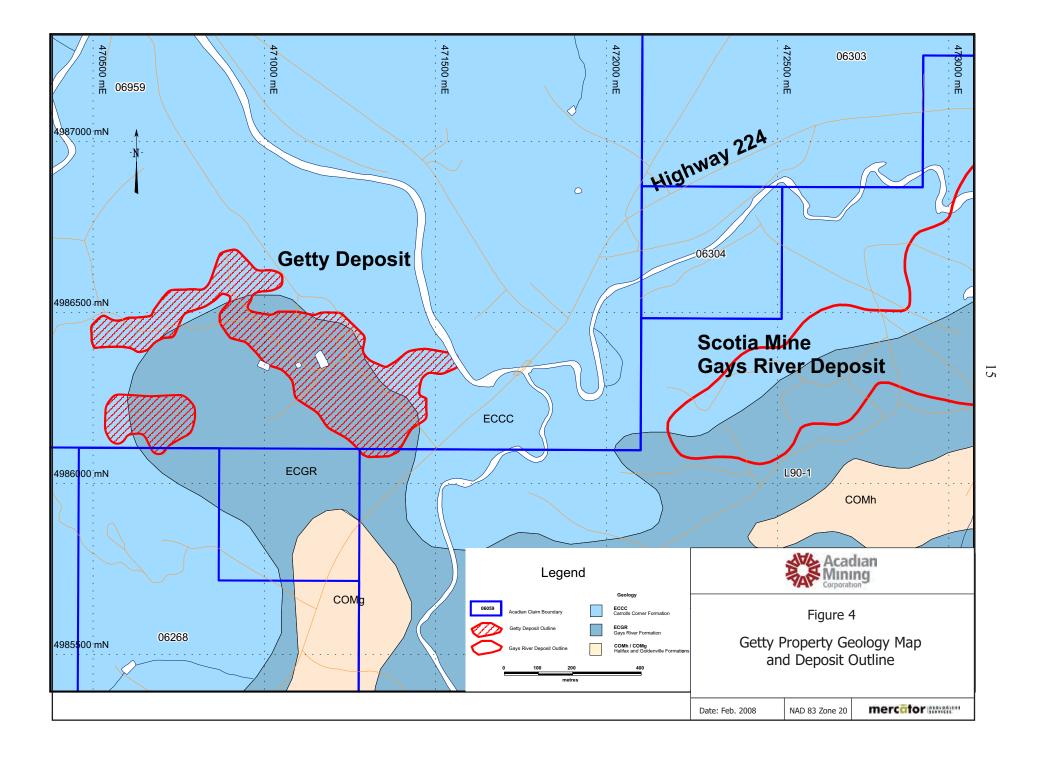
7.1 Stratigraphy

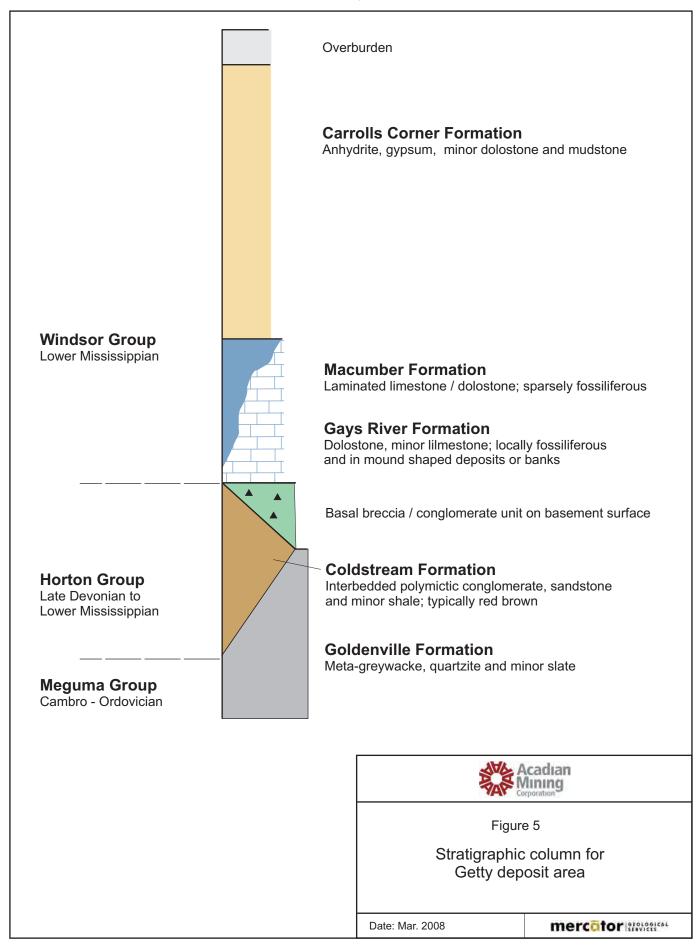
Geology in the Getty deposit area has been interpreted from compiled results of Giles and Boehner (1982) plus results of various mapping and diamond drilling campaigns carried out in the area. The actual deposit does not outcrop, but was delineated by Getty through drilling (eg. Bryant, 1975, Comeau, 1973, 1974; Palmer and Weir, 1988a,b).

As represented in Figure 4, the Getty deposit is hosted by a northwest trending Gays River Formation carbonate bank complex that occurs as a direct extension to the larger, northeast trending carbonate bank that hosts Scotia Mine's zinc lead resources and reserves. Both banks developed along paleo-basement highs comprised of Cambro-Ordovician age Goldenville Formation quartzite and greywacke. At Getty the host dolostone ranges in true thickness from less than a meter to a maximum of about 45 meters.

The carbonate host sequence occurs above a thin sedimentary breccia or conglomerate unit comprised predominantly of Goldenville Formation debris with a small carbonate matrix component resting unconformably on Goldenville Formation basement. Carrolls Corner Formation evaporites lie stratigraphically above the Gays River Formation and are comprised locally of gypsum and anhydrite with minor amounts of interbedded dolomitic limestone and siltstone. With possible exception of local clay and sand accumulations of Cretaceous age, Carrolls Corner Formation rocks are the youngest sequences of the local bedrock section. Figure 5 presents a stratigraphic column for the deposit area.

Historical and the current drilling on the Getty property has shown that evaporite cover at the Gays River Formation contact was in many instances preferentially removed by erosion and karst-related solution processes during Cretaceous time, leaving a trough or trench parallel with the carbonate contact in many areas. Stratified Cretaceous fill sedimentary material followed by Quaternary material of glacio-fluvial origin infilled this trough, and is termed "Trench" material on the adjacent Scotia Mine property. Similar material exists in some areas adjacent to the Getty deposit but in many instances is difficult to distinguish from less consolidated overburden material that is of glacial origin.





7.2 Deposit Type

Description

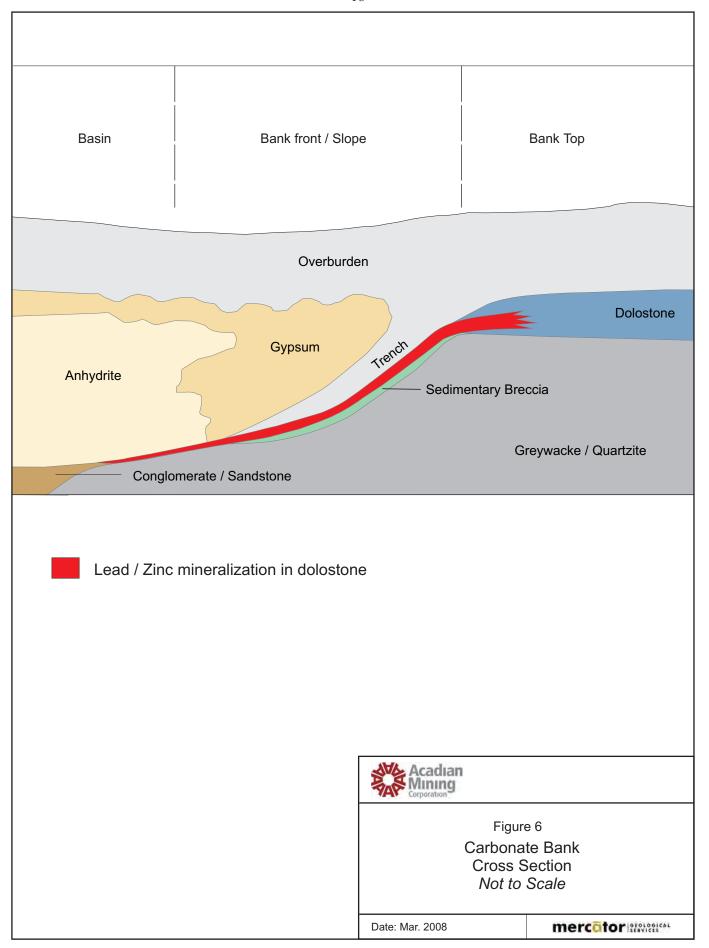
The Getty deposit carbonate bank forms a northwest extension to the adjacent Gays River bank that hosts Scotia Mine zinc-lead resources and reserves. While broadly similar, carbonate bank slopes at Getty are generally gentler than those seen at Gays River. Figure 6 depicts a typical bank cross section illustrating occurrence of thickest carbonate on the bank top, with progressive thinning down dip on the paleo-topographic high. Variations existed locally in basement paleo-slope angles and appear to have directly influenced corresponding carbonate bank morphology. Areas with steep basement slopes tend to show rapid thinning of carbonate away from the thicker bank tops, with correspondingly steep contact surfaces with overlying evaporites. Gentle slope areas show greater lateral and down-dip continuation of thicker carbonate and corresponding lower average contact dips with the overlying evaporite. Based on the drilling carried out to date at Getty, the maximum carbonate thickness encountered along the basement high trend is 45.48 meters in drill hole GGR-221.

Gays River Formation carbonate banks include intricately intercalated algal, peloidal and coraline lithfacies, with abundance of bindstone, bafflestone, packstone and micrite. These facies show transition downdip to thin (typically <5 meters), variably laminated algal/silty carbonates that are lateral equivalents to laminated carbonates of the Macumber Formation. The latter occurs basinward of the underlying Horton Group's stratigraphic pinchout and is not present in the deposit area.

Genetic Model

The adjacent Scotia Mine deposit has been the subject of extensive academic and government research and reporting since its discovery in 1971. Much of this work was summarised by Roy et. al. (2006) and the deposit is a considered an example of the Mississippi Valley Type (MVT) class of carbonate hosted, stratabound, base metal deposits. Prominent examples of the paleo-basement high deposit setting along the Viburnum Trend of Southeast Missouri, but are characterised in this area by dominance of lead mineralization over that of zinc (Sangster et. al., 1998; Akande and Zentilli, 1983; Machern and Hannon, 1974).

Localization of base metals within the Getty bank complex is believed to have resulted from interaction between metal-bearing basinal fluids, potentially sourced in the Horton Group stratigraphic section or in basement sequences, and chemical reductants, possibly



including hydrocarbon, that were present at sites of deposition within the bank. Kontak (1998, 2000) reported on fluid inclusion and other studies of ore from the adjacent Scotia Mine property and concluded that saline brines in the 100° C to ≤ 250° C temperature range were involved in the main mineralizing process and that these temperatures are higher than those typically seen in MVT districts. Héroux, et. al (1994) studied organic maturation and clay mineral crystallinity characteristics of Gays River Formation rocks of the Musquodoboit and Shubenacadie basins and identified a corridor of higher interpreted heat flow that occurs in part over the Scotia Mine and Getty deposit areas and is consistent with the higher fluid temperatures previously noted. It is clear that zinc and lead mineralization were superimposed on lithified and dolomitized host rocks (Akanade and Zentilli, 1985; Kontak, 1998).

8.0 Mineralization

Zinc and lead sulphide mineralization are found throughout the Getty carbonate bank, along with trace amounts of iron sulphide in isolated areas. Base metal sulphides are also present to a lesser extent in carbonate matrix of the underlying conglomerate/breccia unit and within calcite or micrite filled fractures and joints present in underlying Goldenville Formation greywackes. While not extensively reported to date, galena has also been documented locally at the Scotia Mine deposit in thin (<20cm thick) discordant, steeply dipping veins that generally trend north-south (B. Mitchell, personal communication, 2007).

Drilling to date on the Getty deposit has shown that massive to submassive high grade mineralization like that commonly present along steep bank front zones at Scotia Mine is not present to a significant degree at Getty (Bryant, 1975). However, a clear association of higher zinc and lead grades with dolostone intervals on the northeast and north slopes of the Getty bank is recognized and lower grades over thicker intervals occur within the carbonate sections at the top of the bank. Mineralization is more poorly developed along the southwest side of the bank.

Sphalerite is the predominant base metal sulphide phase present and is typically honey yellow to buff or beige in colour and finely crystalline. Based on drill core observations, Bryant (1975) specified the following four modes of sphalerite occurrence within the deposit, with the first being the most common: (a) disseminated mineralization showing concentrations from trace to 10% or more, (b) semi-massive and massive mineralization as seams and replacements along bedding surfaces or laminae, (c) massive, porosity filling or surface coating mineralization in fossiliferous and vuggy carbonate, (d) mineralization associated with secondary calcite in small stringers and veinlets.

Silver is a trace constituent of the Getty sulphide assemblage but is not present at levels of economic significance. This parallels the situation at adjacent Scotia Mine where Roy et. al. (2006) reported historic silver values in mill concentrates that were typically less than 40 parts per million.

9.0 Exploration

At the effective date of this report Acadian was conducting a diamond drilling program on the Getty property that is planned to total approximately 100 drill holes. The purpose of the program is to upgrade geological confidence in the deposit and to provide a basis for future estimation of higher category mineral resources. Mercator is providing site supervision, logging, sampling and quality control/quality assurance services to Acadian for this on-going program. With the exception of four holes completed by Acadian as twins to historic drill holes, for the specific purpose of comparison with historic records, results of the on-going drilling program are not discussed in the current resource estimate. Acadian plans to update to the current estimate after completion of the drilling program and interpretation of results.

10.0 Drilling

Historic diamond drilling information pertaining to the Getty deposit was compiled by Westminer in a digital database containing information for approximately 181 vertical holes totalling 16,875 meters of drilling. The Westminer database was originally prepared to support the resource estimate reported by Hudgins and Lamb (1992) and to this end, collar coordinates, lithologic codes, geologic legend and individual drill core assay interval results were compiled from original drill logs, checked for errors, and entered into the original digital database. All historic holes were initially coordinated to reference grid but Mercator subsequently transformed all drill hole local Getty coordinates into the Scotia Mine grid using historic tie points for which Acadian surveyors provided up to date mine grid coordination. Universal Transverse Mercator (UTM) coordinates (Zone 20, NAD 83 Datum) for all holes were also calculated by Mercator for all holes in the project database and a listing of drill hole coordinates and orientation data for the deposit in the block model grid system appears in Appendix 2. Mercator staff physically checked all drill hole entries in the database against the original hard copy logs.

The Getty project drilling database includes results of 184 historic drill holes completed during the 1970's, 181 of which were drilled by Getty and total 16,875 meters of drilling. The three remaining holes were completed by Esso during the same time period and total 157 meters of drilling. The resource outline pertinent to this report includes 68 of the

historic drill holes. As stated previously, results of the diamond drilling program currently underway at Getty are not included in the current resource, but four twin holes completed by Acadian in 2007 were used to check integrity of historic drill hole data. Results of this twinning program are discussed in report section 12.2.3 that deals with quality control and quality assurance issues. A plan showing locations of the current resource outline as well as historic drill collars and collars of the four Acadian twin holes is included in Appendix 4.

11.0 Sampling Method and Approach

11.1 Getty and Esso Programs: 1972 to 1975

Government assessment reports were reviewed to identify core logging and sampling procedures applicable to the Getty and Esso drilling programs carried out between 1972 and 1975. These showed that drill core was typically logged by staff geologists who produced hard copy lithologic logs for each drill hole. Detailed information related to lithology and mineralization was systematically recorded in the logs along with complete records of core sampling and major analytical results. There is no specific description of sample marking, cutting, handling, tagging or shipping protocols, but industry standard marking and tagging of sample intervals is evident in the archived drill holes viewed and sampled by Mercator staff in 2007 at the Nova Scotia Department of Natural Resources core library in Stellarton, Nova Scotia (core library). Half-core samples were typically submitted for analysis and sample intervals reflected visually determined mineralized zone limits. A sample interval of 5 feet was commonly used but no standard appears to have been established by either company. Non-mineralized carbonate was rarely sampled. Core was logged in imperial measure and drill logs were transformed to metric equivalents subsequently during the digital data entry process.

Core from the original Getty drilling program was placed in marked core boxes and retained in covered storage in the local area until 1984. At that time NSDNR took procession of the core and it was archived at the core library in Stellarton. Esso core was stored at the Gays River mine site, with mineralized intervals typically retained in covered storage and the remaining non-mineralized intervals stored out of doors where rapid deterioration of boxes and core took place. Core storage facilities established by Esso deteriorated over the years and in some cases have been demolished. No accurate records exist of archived core or of core salvaged from the deteriorated buildings. As a result, it is unclear whether core from the Esso holes completed at Getty is included in the non-inventoried remnants of archived core that currently exists at the Scotia Mine facility. With no evidence to the contrary, it is assumed that this core has been lost or destroyed and is not available for review at present.

11.2 Acadian Re-sampling of Getty Hole GGR-125

Historic drill hole GGR-125 was completed by Getty in 1972 and was chosen for resampling by Mercator staff during a 2007 visit to the Stellarton core library and sample interval and assay comparison tables appear in section 13.2.2 of this report. Quarter core samples of the previously sampled carbonate intervals were collected from Getty hole GGR-125, ensuring a quarter of the core remained for archival purposes. An additional nineteen holes where summarily examined and one hole, GGR-212 was re-logged in detail, but only GGR-125 was re-sampled (Table 5).

| Getty Historic Hole | Acadian Twin Hole (2007) Comment | | | | | | |
|---------------------|----------------------------------|--------------------------|--|--|--|--|--|
| GGR 125 | NA | Re-sampled | | | | | |
| GGR 212 | S1025 | Re-logged and Re-drilled | | | | | |
| GGR 190 | S1021 | Re-drilled | | | | | |
| GGR 215 | S1043 | Re-drilled | | | | | |
| GGR 37 | S1059 | Re-drilled | | | | | |

Table 5: Historic drill holes twinned or re-sampled in 2007

11.3 Acadian Twin Hole Sampling

As part of the ongoing Acadian drill program approximately 10% of the historical holes. are planned for twinning. Four twinned holes were completed prior to the effect date of this report and were continuously sampled through the carbonate and basal breccia intervals using a nominal 1.0 meter sample length. Half core samples from the twin holes were cut at the Acadian core logging facility at Scotia Mine and then placed in prenumbered plastic sample bags along with a corresponding paper sample tag, the number of which was recorded in the core log and sample record logs for the drill hole. After insertion of quality control samples, all bagged samples were checked for sequence, placed in sealed plastic buckets and shipped to Eastern Analytic in Newfoundland by commercial transport for analysis of zinc and lead. Results of this sampling program are discussed in report section 13.2.2.

12.0 Sample Preparation, Analyses and Security

12.1 Getty And Esso Programs

Reports documenting the Getty and Esso drilling programs in the Getty deposit area do not provide detailed descriptions of sample preparation methodologies, analytical procedures or security considerations. However, both Getty and Esso were major, reputable exploration companies carrying out exploration programs in various settings at

that time. More specifically, Esso was also in the process of defining reserves at the adjacent Gays River mine at the time and appears to have employed the same operating protocols for Getty drilling as were applied at the adjacent development property. Mercator is of the opinion that, while not specifically detailed in historic reporting, procedures employed by both Getty and Esso for sample preparation, record keeping, chemical analysis, and security, would have met industry standards of the day. This assertion is supported by review of original drill logs and supporting data, physical review of archived core and through recognition that both companies completed resource estimate and preliminary development assessments based on the same historic drilling results.

12.2 Acadian Mining Programs

12.2.1 Sample Security and Chain of Custody

In accordance with the sample protocol established by Mercator for Acadian's 2007-2008 Getty drilling program, all drill core from twin holes was delivered from the drill site to the secure and private core logging facility at Acadian's Scotia Mine by either Logan Drilling Limited staff or Mercator field staff. Drill core logging was carried out by a Mercator geologist who also marked core for sampling and supervised core splitting by a technician using a rock saw. Sample tag numbers from a three tag sample book system were used for the program, with one tag showing corresponding down hole sample interval information placed in the sampled core boxes at appropriate locations, one tag lacking down hole interval information placed in the core sample bag for shipment to the laboratory, and the third tag with sample interval information retained in the master sample book for archival reference and database entry purposes. After sampling, core boxes were closed and placed in storage at the Scotia Mine site. Sealed sample bags were placed in an ordered sequence prior to insertion of quality control samples, preparation of sample shipment documentation, checking, and placement in plastic buckets for shipment by commercial courier to Eastern Analytical Limited (Eastern), a recognized commercial laboratory located in Springdale Newfoundland. Prepared pulps were retained for 30 days at the laboratory and coarse reject material was stored for 90 days before being shipped back to Acadian for secure archival storage.

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In the case of historic drill hole GGR-125, archived half core from the hole was accessed at the NSDNR core library in Stellarton and cut using a diamond saw to produce quarter core samples. The sample interval was recorded using the same three tag system described for the Acadian core and samples were processed as described above for the twin hole core samples. Samples were sent to Eastern via commercial courier where laboratory analysis was completed. Prepared pulps were retained for 30 days at the

laboratory and coarse reject material was stored for 90 days before being shipped back to Acadian for secure archival storage.

12.2.2 Core Sample Preparation

Core samples received by Eastern were organized and labelled and then placed in drying ovens until completely dry. Dried samples were crushed in a Rhino Jaw Crusher to consist of approximately 75% minus 10 mesh material. The crushed sample was riffle split until 250 to 300 grams of material was separated and the remainder of the sample was bagged and stored as coarse reject. The 250 – 300 gram split was pulverized using a ring mill to consist of approximately 98% minus 150 mesh material. All samples underwent ICP analysis, for which a 0.500g portion of the pulverized material was required. Those samples containing greater than 2200 ppm of zinc or lead were then processed using ore grade analysis for which 0.200g of pulverized material was required. Laboratory sample preparation equipment was thoroughly cleaned between samples in accordance standard laboratory practise.

Check sample splits of pulverised core were submitted to the ALS Chemex laboratory facility in Sudbury, Ontario as part of the projects quality control and assurance protocol. This material was prepared in approximately 100 gram bagged splits by Eastern and returned to Mercator for subsequent submission to ALS Chemex. Since the received split material had already been pulverised, further preparation was limited to homogenization and splitting of a 0.4g portion for subsequent analysis.

12.2.3 Core Sample Analysis

Eastern Analytical procedures outlined below pertain to all core samples from the resampling and twinning programs completed by Acadian in 2007 and descriptions are for assay quality determinations. Additional details appear in Appendix 2.

- ICP Analysis: A 0.500 gram sample is digested with 2ml HNO3 in a 95°C water bath for ½ hour, after which 1ml HCL is added and the sample is returned to the water bath for an additional ½ hour. After cooling, samples are diluted to 10ml with deionized water, stirred and let stand for 1 hour to allow precipitate to settle.
- For ore grade analysis base metals (lead, zinc, copper), a 0.200g sample is digested in a beaker with 10ml of nitric acid and 5ml of hydrochloric acid for 45 minutes. Samples are then transferred to 100ml volumetric flasks and analyzed on the Atomic Absorption Spectro-Photometer (AA). The lower detection limit is 0.01% and the upper detection limit is >2200 ppm lead or zinc.

• For silver, a 1000mg sample is digested in a 500ml beaker with 10ml of hydrochloric acid and 10ml of nitric acid with the cover left on for 1 hour. Covers are then removed and the liquid is allowed to evaporate leaving a moist paste. 25ml of hydrochloric acid and 25ml of deionised water are then added and the solution is gently heated and swirled to dissolve the solids. The cooled material is transferred to 100ml volumetric flask and is analyzed using AA. The lower detection limit is 0.01oz/t of silver with no upper detection limit.

Analytical procedures for check samples sent to ALS Chemex are outlined briefly below and in greater detail in Appendix 2.

 A prepared sample is digested in 75% aqua regia for 120 minutes. After cooling, the resulting solution is diluted to volume (100 ml) with de-ionized water, mixed and then analyzed by inductively coupled plasma - atomic emission spectrometry or by atomic absorption spectrometry.

13.0 Data Verification

13.1 Review and Validation of Project Data Sets

Review by Mercator of all government assessment reports and internal Acadian files available from the Scotia Mine site established that typed lithologic logs with complete assay records from the Getty drilling era were available. However, original sample record books, laboratory reports and other associated information were not found. The digital drill hole database used for the Westminer's 1992 resource estimate was obtained from Acadian and validated against the original hard copy drill log and assay record entries, Checking of digital records included manual inspection of individual database lithocode entries against source hard copy drill logs as well as use of automated validation routines that detect specific data entry logical errors associated with sample records, drill hole lithocode intervals, collar tables and down hole survey tables. Drill hole intervals were also checked for sample interval and assay value validity against the original drill logs. Database entries were found to be of consistently acceptable quality but minor lithocode and assay entry corrections were made by Mercator. These were incorporated to create the validated and functional drilling database used in the resource estimate. As noted earlier, original assays certificates were not found for any of the historic drilling programs and no records of the laboratories to which samples were submitted for analysis, or methods of analysis, were documented in any of the historic drilling reports reviewed for the resource estimate.

As part of the validation process, Mercator staff visited the NSDNR Core Library in Stellarton, Nova Scotia to review core from the archived Getty drill holes. Nineteen holes where examined but only one hole GGR-212 was re-logged in detail and one hole, GGR-125, was completely re-sampled. These provided additional verification of historical assays and logging results. Results of this and related programs are presented below under separate headings.

13.2 Quality Control and Quality Assurance (QA/QC)

13.2.1 Historic Drilling Programs

Assessment reports documenting Getty and Esso drilling programs do not specifically address QA/QC issues. No evidence was noted of independent certified standards being submitted with core samples from either company nor is there any evidence of systematic submission of blank samples or systematic provision for duplicate sample splits to be prepared and analysed. Similarly, detailed descriptions of sample preparation methodologies, analytical procedures or security considerations are not present in any of the historic documentation reviewed for this report. This situation is not uncommon in reporting at the time in the 1970's, when reliance was placed to a substantial degree on standards, duplicate samples and other quality assurance and control procedures implemented by the commercial laboratories providing analytical work.

As noted earlier, both Getty and Esso were major, reputable companies at the time of their drilling programs on the Getty deposit and that Esso was completing reserve delineation and mine planning work for the adjacent Gays River (Scotia Mine) project that entered commercial production in 1979. Both companies are considered credible and Mercator's review of drill logs and associated sample data did not reveal any points of obvious concern with respect to use of historic results for the project.

Notwithstanding the above, the lack of laboratory assay certificates and information on sampling and laboratory procedures necessitated a review of and re-sampling of archived Getty core and the twinning of a number of Getty-era drill holes within the resource area. These safeguards were implemented and results are discussed below.

13.2.2 Overview Of Acadian Programs

Mercator, on behalf of Acadian, established and administered a quality control and quality assurance program for the Getty 2007-8 drill project. All drill core samples including samples associated with the twinned and re-sampled historic drill holes were subject to project quality control and assurance protocols. In total, 4 twinned holes and one re-sampled historic drill hole were completed prior to this report and were subject to

the project protocols. The program includes insertion of blind certified standards and inhouse blanks, as well as completion of duplicate analyses on core splits and submission of check sample materials to an alternate lab for analysis. Details of each program component are presented below.

(a) Certified Standard Samples

Certified standards were obtained from the Canadian Resource Laboratories of Delta, BC for use in the 2007 drilling program, these being CDN-SE-1 and CDN-SE-2. At the onset of the program, only CDN-SE-1 was used. The second standard was introduced in Hole S1035 and from then on the standards were alternated in sequence. Standards, consisting of pre-packaged prepared sample pulp material weighing approximately 50 grams, were inserted at intervals of every 35th sample and recorded as such. At first, standards were numbered in sequence with the sample stream; however, as of mid September 2007 a separate sample book and associated tags were used.

Table 6a (CDN-SE-1 Standard Results) presents results for the certified standard (CDN-SE-1) blindly submitted with samples from the twinned and re-sampled holes. The zinc result for the hole S1025 sample was slightly below the acceptable 2.65 % ± 0.20 parameter (2.33% vs 2.45%) for the CDN-SE-1 standard and lead in the GGR-125 standard was slightly below (1.80% vs 1.83%) the acceptable 1.92 \pm 0.09% parameter for CDN-SE-1. These slight departures do not represent major errors with respect to the sample data and would have minimal impact on anticipated grade of the deposit. On this basis the associated data are interpreted as being of acceptable quality for resource estimate use. Table 6b details expected parameters for the CDN-SE-1 and 2 standards.

Table 6a: CDN-SE-1 Standard Results for Re-sampled and Twinned Holes

| Hole | Sample | Comments | Zn ppm | Zn % | Cu ppm | Pb ppm | Pb% |
|---------|--------|---------------|--------|------|---------|--------|------|
| S1025 | 56039 | Standard SE-1 | >2200 | 2.33 | 911.54 | >2200 | 1.96 |
| GGR 125 | 33209 | Standard SE-1 | >2200 | 2.60 | 976.924 | >2200 | 1.8 |

Table 6b: CDN Laboratories Ltd Standards: Recommended Values

| Standard | Gold g/t | Silver g/t | Copper % | Lead % | Zinc % |
|----------|-------------------|--------------------------|-------------------|-------------------|-----------------|
| CDN-SE-1 | 0.480 ± 0.034 | 712 +/- 57 g/t | 0.097 ± 0.005 | 1.92 ± 0.09 | 2.65 ± 0.20 |
| CDN-SE-2 | 0.242 ± 0.018 | $354 \pm 21 \text{ g/t}$ | 0.049 ± 0.003 | 0.957 ± 0.044 | 1.34 ± 0.11 |

Date of Certification: May 15th, 2007

(b) Blind Blank Samples

Blank samples of comparable weight to normal 1.0 m half core samples were systematic inserted at intervals of every 20th sample in the laboratory submission stream. These blank samples formed part of the continuous sample number series. Blank samples consisted of non-mineralized anhydrite half-core collected from Acadian drill hole CBB-3. These samples were blind to the receiving laboratory.

Table 7 presents associated zinc and lead analytical results for pertinent blank samples and show that levels of both metals are very low, with those for zinc not exceeding 89 ppm and those for lead not exceeding 32 ppm. Total range of results for zinc is 67.40 ppm and for lead is 24.69 ppm. Review of adjacent sample values showed no obvious cross contamination between blank samples and those of proceeding or subsequent higher grade samples. On this basis no substantial problem is considered to exist with sample cross-contamination arising from laboratory sample preparation procedures. However, the anhydrite used for blanks has a low background level of both zinc and lead and Mercator is currently sourcing a blank with lower metal values.

Table 7: Blind Blank Sample Results

| Hole | Sample | Comments | Zn ppm | Pb ppm |
|--------------|--------|----------|--------|--------|
| S1021 | 47010 | Blank | 21.60 | 7.19 |
| S1025 | 56040 | Blank | 29.47 | 24.12 |
| S1025 | 56060 | Blank | 33.00 | 31.88 |
| GGR 125 | 33211 | Blank | 89.00 | 20.23 |
| Sample Range | | | 67.40 | 24.69 |

(c) Quarter Core Duplicate Samples

Every 40^{th} sample of the Acadian core sample sequence was quarter split and one quarter of the archive half core was submitted to Eastern Analytical, in addition to the standard half sample, as part of the normal sample numbering sequence. Due to the limited number of samples comprising the twin hole and historic re-sampling programs, only 2 sets of quarter samples pertain to this report. Results for these are presented in Table 8 and show that variability at the level of \pm .01% occurs within the grade range of the samples. This variation in part reflects heterogeneity of sample material but also includes analytical error plus other potential errors that in combination resolve at less than the \pm error margins for project certified standards for assay quality results. A larger population of sample results with larger grade range is necessary to identify factors contributing to the noted variation and this should be an on-going project goal.

Zn % **Comments** Zn ppm Pb ppm Pb% Hole Sample S1021 47011 236.01 0.02 80.12 0.01 S1021 47012 1/4 dup of 47011 94.49 0.00 0.01 24.07 S1025 56041 170.21 0.02 68.00 0.01 S1025 56042 1/4 dup of 56041 107.00 87.83 0.01 0.01

Table 8: Quarter Core Duplicate Sample Results

(d) Duplicate Sample Splits

A duplicate split of prepared pulp material was requested from every 25^{th} sample of the normal core sample stream and the laboratory was instructed to complete and report zinc and lead levels for these splits. Splits were labelled 'A and B' respectively and Table 9 presents results for core samples included in the twin and historic re-sample programs. These show variation in the \pm .01% (zinc) and \pm .02% (lead) ranges which are considered acceptable with respect to deposit grade ranges of interest.

Table 9: Duplicate Sample Split Results

| Hole | Sample | Comments | Zn ppm | Zn % | Cu ppm | Pb ppm | Pb% |
|-------|--------|----------------|---------|------|--------|--------|------|
| S1021 | 47002A | pulp duplicate | 675.693 | 0.07 | 12.32 | 53.444 | 0.01 |
| S1021 | 47002B | pulp duplicate | 595.226 | 0.06 | 10.712 | 35.046 | 0.00 |
| S1025 | 56027A | pulp duplicate | >2200 | 0.57 | 12.32 | 336.06 | 0.03 |
| S1025 | 56027B | pulp duplicate | >2200 | 0.56 | 12.55 | 479.70 | 0.05 |
| S1025 | 56052A | pulp duplicate | >2200 | 0.35 | 11.32 | >2200 | 0.29 |
| S1025 | 56052B | pulp duplicate | >2200 | 0.34 | 10.87 | >2200 | 0.29 |

(e) Check Samples

A check sample split was prepared from the same crushed sample material used to prepare the duplicate split samples noted above. This material was pulverised to -100 mesh, labelled, placed in a sealed envelope and returned to Mercator. All check samples were then sent to ALS Chemex in Sudbury, ON for independent analysis of zinc and lead levels. Table 10 presents results for sample splits analyzed at the two laboratories. Results for two of the samples (5627A and 56052A) are consistent and acceptable, varying by a maximum of 0.02% for lead and 0.01% for zinc. The third sample, 56052A, shows zinc variation of 0.15% and lead variation of 0.11%, both of which are slightly higher than desirable. Based on these limited results, re-analysis of the split materials has been recommended, with results to be considered in the on-going QA/QC program.

ALS **ALS** Eastern Eastern Analytical Chemex **Analytical** Chemex Hole Sample (Zn %) (Zn %) (Pb %) (Pb %) S1021 47002A 0.07 0.01 0.07 0.01 S1025 56027A 0.57 0.60 0.03 0.01 S1025 56052A 0.35 0.20 0.29 0.18

Table 10: Laboratory Check Sample Results

(f) Re-sampling and Twinning of Historic Drill Holes

As noted previously, 4 historic drill holes were twinned and one historic drill hole was resampled as part of the ongoing Acadian QA/QC program (Table 11).

| Getty Historic Hole (1973) | Acadian Twin Hole (2007) | Description |
|----------------------------|--------------------------|-----------------------|
| GGR 125 | NA | Re-sampled |
| GGR 212 | S1025 | Re-logged; Re-drilled |
| GGR 190 | S1021 | Re-drilled |
| GGR 215 | S1043 | Re-drilled |
| GGR 37 | S1059 | Re-drilled |

The four Acadian holes completed as twins to earlier Getty holes showed generally good correlation with respect to logged bedrock geology. Assay results for entire dolomite intervals are broadly comparable but discrepancies are present. Table 12 presents comparative lithologic units based on logging of the twinned holes and Table 13 presents corresponding assay results. While sampled interval lengths differ between holes, the weighted average grades calculated for main sections of mineralized dolostone in historic holes GGR-190 and GGR-037 show low grade mineralization with zinc grades varying by 0.30% or less and lead grades varying by 0.08% or less with corresponding twin holes S1029 and S1059. In contrast, historic hole GGR-215 returned a thinner dolostone intercept than seen in twin hole \$1043 (1.65 meters versus 4.55 meters), comparable high grade lead value (4.81% versus 5.7%) and lower zinc value (2.25% versus 7.00%). S1043 was presumed to be drilled approximately 10 meters from the historic collar location and this alone could account for the grade and lithological thickness differences noted above. It is also possible that a discrepancy exists between the actual historic hole location and that recorded in the database and this possibility should be addressed in an ongoing manner through continuation of the drill hole twinning program. Notably, both GGR-215 and S1043 intersected higher grade zones of zinc and lead mineralization in comparably thin sections of the carbonate bank at directly comparable elevations, suggesting spatial proximity of the holes.

In the case of re-sampled Getty drill hole GGR-125, for which quarter core samples were submitted for analysis, the total weighted average grades for 19.20 meters of re-sampled dolostone showed very good agreement with corresponding weighted averages based on original Getty values, with zinc varying by 0.14% and lead by only 0.01% (Table 13, Figures 7 and 8). A sample length discrepancy of only 10 centimeters was recognized.

Combined results of the resample and twin hole programs indicate that generally acceptable correlation exists between the data sets tested. However, some discrepancies do exist and it is recommended that the twin hole program be expanded by at least 5 holes and that at least 5 additional historic holes be re-sampled to better constrain the relationship between the old and new data sets.

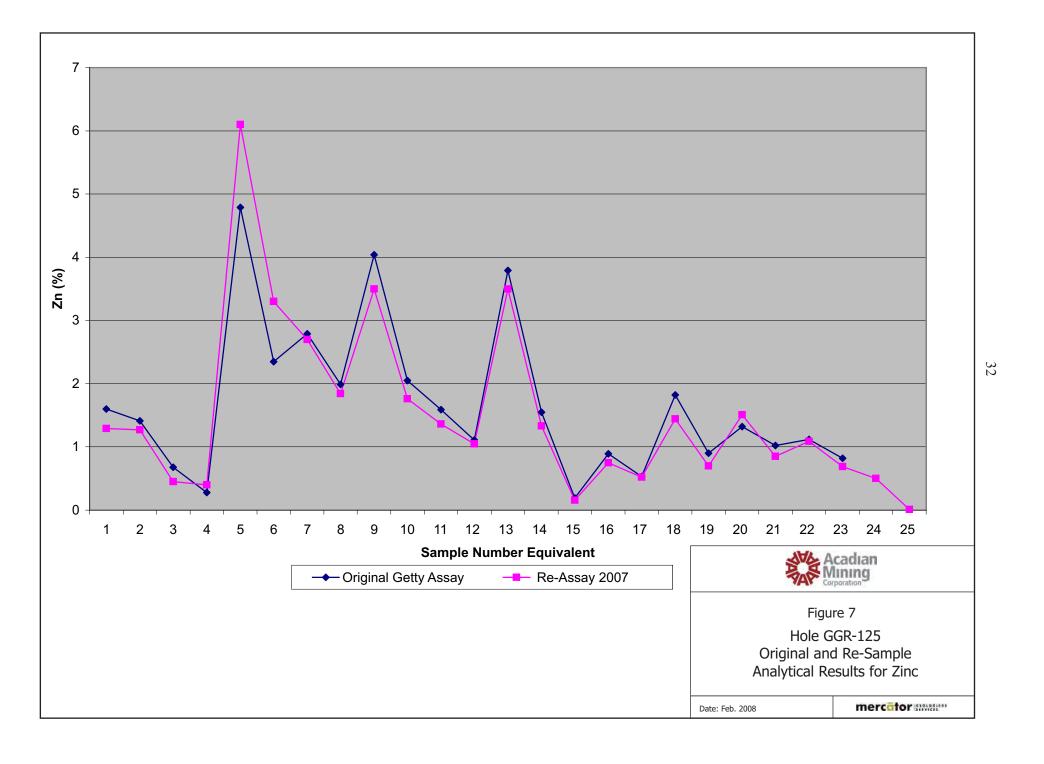
Table 12: Comparative Lithology: Historic Holes And Twin Holes

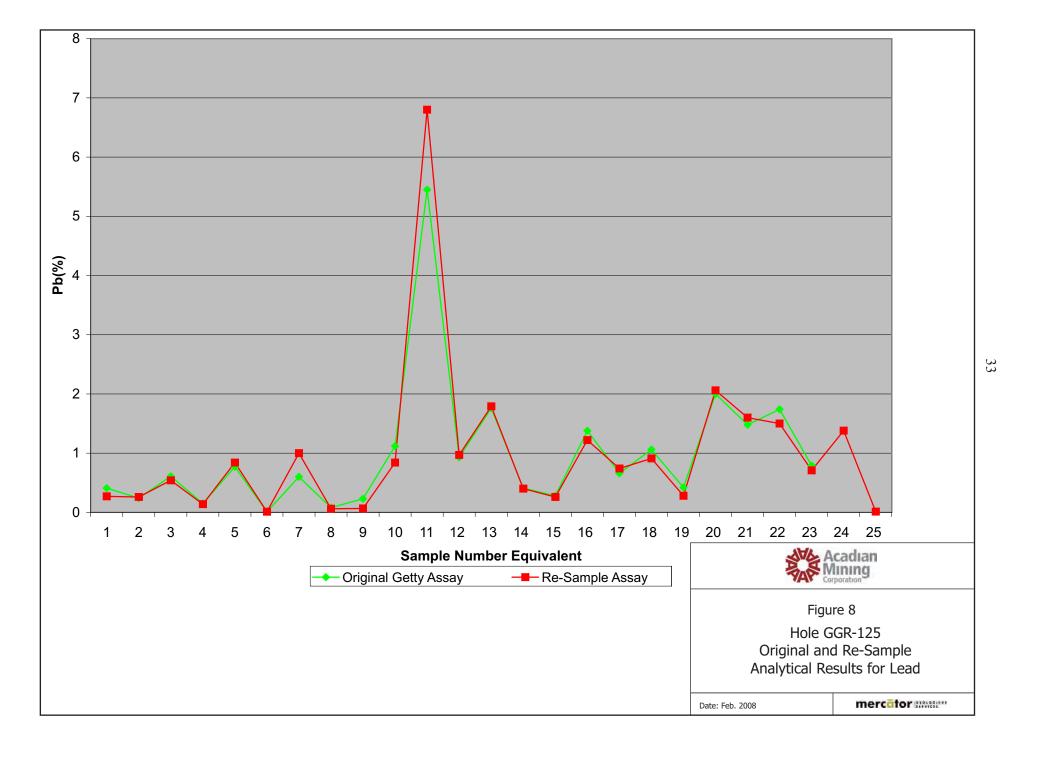
| Hole | From | To (m) | Width | Lithology | Twin | From | To | Width | Lithology |
|--------|-------|--------|-------|------------|-------|-------|-------|-------|------------|
| | (m) | | (m) | | Hole | (m) | (m) | (m) | |
| GGR190 | 0.00 | 26.97 | 26.97 | overburden | S1021 | 0.00 | 23.80 | 23.80 | overburden |
| | 26.82 | 35.72 | 8.90 | dolostone | | 23.80 | 34.45 | 10.65 | dolostone |
| | 35.72 | 43.43 | 7.71 | breccia | | 34.45 | 36.46 | 2.01 | breccia |
| | 43.43 | 48.16 | 4.73 | greywacke | | 36.45 | 41.00 | 4.55 | greywacke |
| GGR212 | 0.00 | 28.96 | 28.96 | overburden | S1025 | 0.00 | 25.10 | 25.10 | overburden |
| | 28.96 | 54.25 | 25.29 | dolostone | | 25.10 | 58.40 | 33.30 | dolostone |
| | 54.25 | 58.30 | 4.05 | greywacke | | 58.40 | 62.00 | 3.60 | greywacke |
| GGR215 | 0.00 | 48.16 | 48.16 | overburden | S1043 | 0.00 | 44.00 | 44.00 | overburden |
| | 48.16 | 65.50 | 17.34 | gypsum | | 44.00 | 60.40 | 16.40 | gypsum |
| | 65.50 | 67.15 | 1.65 | dolostone | | 60.40 | 64.95 | 4.55 | dolostone |
| | 67.15 | 68.64 | 1.49 | breccia | | 64.95 | 65.90 | 0.95 | breccia |
| | 68.64 | 72.24 | 3.60 | greywacke | | 65.90 | 66.40 | 0.50 | greywacke |
| GGR037 | 0.00 | 39.94 | 39.94 | overburden | S1059 | 0.00 | 38.50 | 38.50 | overburden |
| | 39.94 | 69.49 | 29.55 | dolostone | | 38.50 | 66.35 | 27.85 | dolostone |
| | 69.49 | 75.59 | 6.10 | greywacke | | 66.35 | 71.00 | 4.65 | greywacke |

Note: Twin hole S1043~10m SW of GGR215

Table 13: Comparative Assay Results: Historic Holes And Twin Holes

| Hole | From | To | Width | Zn | Pb | Twin | From | To | Width | Zn | Pb |
|---------|-------|-------|-------|------|----------|----------|-------|-------|-------|----------|------|
| | (m) | (m) | (m) | % | % | Hole | (m) | (m) | (m) | % | % |
| GGR125 | 44.20 | 63.34 | 19.14 | 1.63 | 0.92 | resample | 44.20 | 63.40 | 19.20 | 1.49 | 0.93 |
| GGR 190 | 26.82 | 35.72 | 8.90 | 0.66 | 0.02 | S1021 | 23.80 | 34.45 | 10.65 | 0.25 | 0.01 |
| GGR 215 | 65.47 | 68.64 | 3.17 | 2.25 | 5.17 | S1043 | 62.50 | 65.90 | 3.40 | 7.00 | 4.81 |
| GGR037 | 39.94 | 69.51 | 29.57 | 1.1 | 1.37 | S1059 | 38.50 | 66.35 | 27.85 | 1.41 | 1.24 |





14.0 Adjacent Properties

Acadian's Scotia Mine complex adjoins the Getty property to the east and drilling results clearly show that the Getty deposit occurs in a contiguous extension of the carbonate bank complex that hosts zinc-lead mineralization at Scotia Mine. At the effective date of this report Acadian was mining the Scotia Mine deposit through open pit methods and Roy et. al. (2006) reported in detail on mine reserves as well as feasibility study results (Table 14). All Scotia Mine reserves are compliant with both the CIMM Standards and NI 43-101 and Acadian disclosed that mill throughput had reached an average of 2,000 tonnes per day during the last quarter of 2007, primarily processing low grade ore from initially developed areas of the mine. A mine life of 6 years for open pit production followed by slightly over 2 years of underground production from the deposit's Northeast Zone is represented in the feasibility study.

Table 14: Roy et. al. (2006) Scotia Mine Reserves: Effective July 13, 2006

| Category | Туре | Tonnes | Zinc % | Lead % |
|--------------|-------------|-----------|--------|--------|
| Proven | Surface | 1,750,000 | 3.2 | 1.3 |
| Probable | Surface | 1,690,000 | 2.5 | 1.0 |
| | Underground | 1,150,000 | 5.7 | 3.2 |
| | Subtotal | 2,840,000 | 3.8 | 1.9 |
| Total Proven | Surface and | 4,590,000 | 3.6 | 1.7 |
| + Probable | Underground | | | |

Note: 0.75% zinc equivalent cutoff; 15% dilution and 90% mining recovery; zinc equivalent = zinc% + (0.43 x lead %)

The Getty deposit is located 1700 meters west of the Scotia Mine mill and zinc-lead mineralization hosted by carbonate bank dolomite has been shown through drilling to be present continuously in the sub-surface between the two deposits. However, comparison of Scotia Mine reserve and resource figures with Getty deposit resource figures presented in this report shows that substantially higher metal grades are present at Scotia Mine.

Approximately 1.5 kilometers to the southwest of the Getty deposit, on adjacent exploration claims also held by Acadian, the Carrolls Farm zinc-lead prospect was recently discovered by Acadian in dolomitized carbonate bank lithologies. The historic Carrolls Corner zinc-lead prospect occurs in a comparable geological setting 700 meters further to the west and in combination, these may reflect a continuously mineralized trend extending from Scotia Mine, through the Getty deposit and then to the Carrolls Farm and Carrolls Corner areas. The latter two areas have not been investigated in detail by core drilling to date and do not have associated mineral resources. However, they

present good potential for future delineation of mineral resources and require additional investigation.

15.0 Mineral Processing and Metallurgical Testing

No mineral processing or metallurgical studies have been carried out to date by Acadian on Getty deposit material and no historic studies are known to the authors. However, similarity of this deposit to that at Scotia Mine is well documented and metallurgical similarities can be assumed for purposes of general discussion. Roy et. al. (2006) present results of metallurgical studies completed on the Scotia Mine deposit and these should also be relevant as guides with respect to the Getty deposit. At Scotia Mine lead and zinc are recovered by conventional flotation methods after crushing and grinding, with average recoveries of 90% for zinc at a concentrate grade of 60% zinc and 95% for lead at a concentrate of 75% lead.

16.0 Mineral Resource and Mineral Reserve Estimates

16.1 General

The definition of mineral resource and associated mineral resource categories used in this report are those recognized under National Instrument 43-101 and set out in the Canadian Institute of Mining, Metallurgy and Petroleum Standards on Mineral Resources and Reserves *Definitions and Guidelines* (the CIMM Standards). Assumptions, metal threshold parameters and deposit modeling methodologies associated with the current Getty resource estimate are discussed below in report sections 16.2 through 16.4.

16.2 Geological Interpretation Used In Resource Estimation

All areas of zinc-lead mineralization included in the current resource are restricted to the Getty deposit carbonate bank and occur within dolomitized Gays River Formation lithologies. For resource model purposes the Getty deposit is considered an extension of the adjacent Scotia Mine deposit and both are classified as carbonate-hosted, stratabound zinc-lead deposits of the Mississippi Valley Type (MVT). Mineralization is localized in carbonate bank lithofacies that developed above and around paleo-topographic basement highs comprised of Cambro-Ordovician Goldenville Formation greywacke and slate. By definition, Gays River Formation lithologies are laterally equivalent to laminated and thin bedded limestones of the Macumber Formation.

Zinc and lead mineralization of economic proportions is exclusively developed within dolomitized carbonate bank lithologies at Getty and is considered directly comparable to that seen on the adjacent Scotia Mine property. Sphalerite and galena are the dominant sulphide minerals present but trace amounts of marcasite/pyrite occur locally, typically as cavity-lining phases that post-date the zinc-lead mineralizing stage. Silver does not occur in economic proportions in this district but does report to Scotia Mine concentrates at levels of about one ounce per tonne. A similar presence at Getty may exist. Barite is absent from the deposit, as is celestite, but traces of fluorite have been reported (Kontak, 1998, 2000; Sangster et. al., 1998).

As noted earlier, several types of lead and zinc mineralization are represented in the related Scotia Mine and Getty deposits, the most important of which are (1) submassive to massive replacements of carbonate bank lithofacies by sphalerite and galena, typically along steeply dipping carbonate bank front intervals that face the open paleo-basin, (2) disseminated, replacement and porosity filling phases within various carbonate bank lithologies adjacent to and within bank-front intervals, and (3) in rare vein and irregular vug settings or as matrix mineralization between greywacke clasts or boulders in a basal breccia unit that typically separates carbonate bank lithologies from basement greywacke. The dominant type of mineralization in the Getty deposit is disseminated in nature.

16.3 Methodology of Resource Estimation

16.3.1 Overview Of 2007 Estimation Procedure

The Getty mineral resource estimate is based on a three dimensional block model developed using Surpac © Version 6.0.1 modeling software and the validated project drill hole database. The database includes results from 181 historic diamond drill holes completed by Getty as well as 4 holes completed by Esso The four historic holes twinned by Acadian in 2007 were not included. The current resource outline includes 68 historic holes.

The first step in development of the resource model was creation of a set of interpreted geological cross sections presenting lithocoded rock types interpreted from drill logs as well as lead and zinc core sample assay interval data. These served to establish an understanding of carbonate bank geometry and grade distribution trends present in the deposit and were later augmented by contour plans depicting overburden depth, dolomite thickness and basement surface configurations. Sections were created using the local project grid at a nominal spacing of 100 meters, with adjustment of this spacing made as necessary to provide complete coverage of the deposit. Geological and grade distribution models developed from the sections were used to guide and assess subsequently developed versions of the three-dimensional block model.

Assay results from the validated project database were initially assessed through calculation of distribution statistics for both zinc and lead populations after compositing to a common 1.0 meter support base. In total, 1154 composites were created from 928 original core samples. Frequency distribution and probability plots for the composite data set were also prepared and results were interpreted as showing that the few high grade samples present were reflections of valid mineralization styles for which block-scale correlations could be reasonably expected. This assertion reflects observations made during underground mining of high grade portions of the adjacent Scotia Mine deposit. Composites showing high zinc and lead grades occur in several areas along the north-facing bank front area of the Getty deposit, as is the case at Scotia Mine, but these are typically lower in grade, thinner and spatially less extensive than similar high grade areas at Scotia Mine. On the basis of combined factors, no requirement for high grade capping of assay results in the Getty data set was established.

The Getty deposit model was developed within a three-dimensional constraint (or solid) created in Surpac© initially based on a combination of two contributing parameters, these being (1) a minimum meter % (zinc plus lead) value of 4.00 with a minimum downhole intercept length of 3.0 meters, and (2) lateral limits to the deposit solid defined on the basis of midpoints between mineralized and non-mineralized drill holes. The cut-off was assigned as a reflection of the deposit's near-surface location and associated potential for open pit development.

While not as complex as that at Scotia Mine, the carbonate bank front configuration at Getty is still irregular and the solid developed for deposit modelling purposes is characterised by numerous promontories and re-entrants. This is particularly true along north-facing bank front intervals that show spatial association with areas of best zinc and lead mineralization. This configuration approximates a series of variably-oriented panels of dipping mineralization that, although correlative, how strike and dip changes along the length of the deposit.

Spatial variability of mineralized zone trends at Getty prevented development of experimental variograms for lead and zinc data sets that reflected continuity of the mineralized zone to the degree seen in the original geological cross section model. This issue was addressed by Roy et. al. (2006) at the Scotia Mine deposit through three-dimensional transformation of their deposit model that "unfolded" the various mineralized segments to a common surface. Transformed data supported acceptable variogram models and these were subsequently used to establish parameters for grade interpolation into their block model.

In contrast to the method used at Scotia Mine, mineralized trend variability along the Getty deposit was addressed in the current model through use of a discrete mineralized zone solid constraint and an omni-directional search ellipse for interpolation of lead and zinc grades within the solid. Geometric aspects of the mineralized zones were used to establish an interpolation ellipse range and block grades were assigned within the resource solid using inverse distance squared (ID²) interpolation methodology.

Results of the grade interpolation process were checked against geological cross sections to assess conformity and to provide validation of the final deposit block model. A further check on the resource model was completed using nearest neighbour grade interpolation methodology on the deposit solid. Resource figures reflecting several minimum grade thresholds calculated for the block model and combined results constitute the final resource estimate documented in this report.

Report subsections 16.3.2 through 16.3.10 below provide additional information regarding the estimation procedures and parameters summarized above.

16.3.2 Capping of High Grade Assay Values

Zinc and lead grades for all drill core samples were reviewed and descriptive statistics calculated for both the raw data set and that reflecting 1 meter composite support. The latter are presented below in Table 15 and include only those holes that intercept the deposit solid. Distribution and probability plots were also prepared for this data set and are included in Appendix 3 along with similar plots for the block model..

Table 15: Descriptive Statistics: 1 Meter Drill Core Composites Within Resource Solid

| Parameter | Zinc | Lead |
|--------------------------|-------|-------|
| Mean | 1.19 | 0.87 |
| Variance | 1.399 | 2.282 |
| Standard Deviation | 1.183 | 1.511 |
| Coefficient of Variation | 0.99 | 1.732 |
| Maximum | 11.30 | 18.54 |
| Minimum | 0.00 | 0.00 |
| Number | 1154 | 1154 |

Maximum zinc and lead grades at 1 meter composite support are 11.30% and 18.54%-respectively and reflect zones of higher grade mineralization that are considered spatially coherent and correlative at block scale within the deposit. These form a meaningful part of the grade distribution spectrum of the deposit and are associated with valid geological

domains. On this basis, high grade lead and zinc values were not capped for use in the current resource estimate.

16.3.3 Compositing of Drill Hole Data

One meter down-hole composites of raw core sample assay values were created for each drill hole, with this length representing the dominant sample interval used by Acadian in the on-going 2007-2008 drilling program. Historic drilling program sample length statistics are presented in Table 16 and review of associated rank and percentile figures show that 99 percent of the historic samples measure less than 2.0 meters in length, 76 percent measure 1.52 meters or less in length and 34 percent measure less than 1.0 meter in length. Average length of historic samples is 1.2 meters.

Table 16: Descriptive Statistics: Historic Core Sampling Intervals

| 1 | 1 & |
|--------------------------|-------|
| Parameter | Value |
| Mean | 1.20 |
| Variance | 0.208 |
| Standard Deviation | 0.456 |
| Coefficient of Variation | 0.378 |
| Maximum | 4.26 |
| Minimum | 0.09 |
| Number | 928 |

Sampling of high grade intervals in historic drill holes was typically carried out based on geological contacts with no minimum sample length parameters applied. This is probably reflected in samples from historic programs with lengths of less than 0.5 meters. In total, 1154 assay composites at 1 meter support were calculated from the historic drill hole data set. These were used in the main ID² resource block model and were also used to define the resource solid wireframes and to calculate corresponding weighted average zinc and lead grades for drill hole intercepts within the solid. The weighted average intercept grades were used in the Nearest Neighbour interpolation check model and appear in Appendix 3 along with a listing of the 1 meter composites and calculated sub-samples that occur within the solid.

16.3.4 Calculation of Equivalent Zinc

A zinc equivalent parameter was calculated to provide definition of resource solids. For this purpose, zinc equivalent was established as zinc equivalent = (zinc % + lead %) on the basis of estimated averages of monthly London Metal Exchange spot market values for the two metals for the period July through October 2007. This factor allowed direct

comparison of current resource estimate figures with those of earlier workers who had independently quoted the combined Zn + Pb metal parameter. At the effective date of this report London Metal Exchange spot prices for lead were substantially higher than those for zinc (~\$1.58US/lb lead versus \$1.22US/lb.zinc – see Appendix 2 for support data), with this relationship being opposite to that seen earlier in 2007 when zinc was trading at substantially higher levels than lead. This highlights the need for caution when considering equivalent metal calculation parameters and their potential for impact on resource evaluations.

With respect to the Getty block model, zinc and lead grades were separately interpolated into the model and zinc equivalent values that appear in the resource statement were calculated from the average metal values defining the resource. As noted earlier, zinc equivalent values for 1 meter drill core composites were also used to guide development of model solid limits.

16.3.5 Variography

An initial assessment of variography for the deposit area was carried out by creation of experimental variograms within the main northwest trending portion of the deposit that corresponds with mineralization developed along the contact between overlying evaporite and extending southwest into the dolomitized bank complex proper. This forms a broad corridor of northwest striking, northeast dipping mineralized carbonate that shows restriction of most mineralization to a relatively narrow, 150 meter elevation corridor. Substantial irregularities of the mineralized carbonate's trend are present in this corridor and take the form of promontories and re-entrants that have associated variations in strike and dip components. A similar configuration marks the northwest end of the main deposit where bank front carbonate faces and dips to the northwest along a strike length of approximately 500 meters before merging with the western side of the deposit that faces and dips to the southwest along the west side of the basement high.

The assay data set associated with the assemblage of multiple mineralized zone segments described above did not provide meaningful variography on the scale of the entire deposit and on this basis, an alternative approach was necessary to define grade interpolation ellipse parameters for the resource model. Due to complexity of process, no attempt was made to transform and "unfold" the deposit prior to calculation of experimental variograms in the manner used at Scotia Mine by Roy et. al.(2006).

16.3.6 Setup of October 2007 Three Dimensional Block Model

Block model total extents were defined in local grid coordinates as being from 6000 meters East to 7145 meters East and from 6450 meters North to 7150 meters North. The model extends in elevation from 150 meters to 700 meters relative to the Scotia Mine local grid that has a datum of mean sea level plus 500.11 meters. The nominal topographic surface in the Getty deposit area occurs between the 550 meter and 520 meter local grid elevations and all resource solids respect the bedrock/overburden surface defined by the resource drill hole data set. As noted earlier, drill holes in the Getty database are coordinated to both the Scotia Mine local grid and to UTM Zone 20 (NAD83) and collar coordinates for the local grid are reported in Appendix 2. The local grid closely reflects the 3° Modified Transverse Mercator (MTM) projection for Nova Scotia (ATS 77 datum) and transformation details appear in Appendix 2.

A standard block size for the model was established at 2.50 meters x 2.50 meters, with sub-blocking at 1.25 meter x 1.25 meter x 1.25 meter to better fit the model along geological, topographic and peripheral solid limits. Descretization within blocks was 1 x 1x 1 and no block rotation was applied. The chosen block size reasonably reflects the laterally continuous but potentially variable character of mineralization within the deposit and allows definition of thinner zones of mineralization present in some areas. The chosen block size also provides a meaningful approximation of a mining unit size that might be applicable in development of this style of base metal deposit.

The major lithologic units incorporated in the Getty geological model were discussed in report section 6.0 and all historic drill holes were lithocoded using the lithocode system originally established by Westminer for the Scotia Mine deposit. This system is also being used in the current Getty deposit drilling program by Acadian and a listing of lithocodes and descriptions appears in Appendix 2.

Resource estimation was completely constrained within a deposit solid developed from systematic wireframing of mineralized envelope limits on geological cross sections cut through the deposit. Wireframes were joined to create the grade constraint solid and then checked to correct any geometric inconsistencies. A minimum metal % (zinc + lead) value of 4.0 and minimum 3.0 meter down hole sample length was used initially to define sectional wireframe limits with slight modifications locally required after inspection of the resultant solid. Lateral or down-dip deposit limits were commonly created at midpoints between holes that mark the mineralized zone to non mineralized zone transition.

16.3.7 Material Densities

Density factors for the block model were assigned using a calculation method incorporating both an assigned value for the dolomite host rock and a value developed from relative proportions of zinc and lead occurring in sphalerite and galena present in a core sample composite. Values were generated from interpolated metal block grades within the deposit solid and assigned to associated blocks. These values were multiplied by corresponding block volumes and results summed to obtain tonnage values for the block model. The density calculation formula used for the block model appears below and follows application by Roy et. al. (2006) in feasibility study reporting for the adjacent Scotia Mine project. The density calculation recognizes a base dolostone value of 2.7 g/cm³ plus a contribution based on zinc and lead content, assumed to be present only as sphalerite and galena. The density factor calculation appears below:

Factor: 1/(Pb %/(86.6x7.6g/cm3) + Zn %/(67.0x4.0g/cm3) + (1-Pb%/86.6 - Zn%/67.0)/2.7g/cm3)

Note: 86.6 = weight percent of Pb in galena, 67.0 = weight percent of Zn in sphalerite

No historic collection of density data for either the Scotia Mine or Getty deposits was identified in exploration records but Acadian is currently establishing a core sample density database through systematic analysis of core samples from the on-going 2007-2008 drilling program. For purpose of review, descriptive statistics for the drill hole composite density values used in the current block model are presented in Table 17.

Table 17: Descriptive Statistics: Block Model Density Values

| Parameter | Value |
|--------------------------|-------|
| Mean | 2.824 |
| Variance | 0.009 |
| Standard Deviation | 0.094 |
| Coefficient of Variation | 0.033 |
| Maximum | 3.543 |
| Minimum | 2.700 |
| Number | 91180 |

16.3.8 Interpolation Ellipse and Resource Estimation

Inverse Distance Squared (ID²) grade interpolation was used to assign block model metal grades, with blocks being fully constrained by limits of the resource solid. Since useful variogram models were not generated for the deposit data set, a range value for the grade interpolation ellipse was established on the basis of the deposit geological model

reflected in the resource grade constraint solid and its interaction with an isotropic interpolation ellipse. Samples within the deposit solid were considered to form a continuous mineralized zone within which adjacent samples at higher and lower elevations as well as in laterally adjacent sites within the solid were considered valid contributors to block grade. No metal zonation trends had been defined on the deposit scale that would negate this approach. A maximum of 21 sample composites was established for estimation of individual block grades with no more than 7 composites coming from a single drill hole. These including sample parameters ensured both multiple drill hole inclusion in block grade estimations and lateral grade projection between drill holes in the dip and strike orientations. A 100 meter range was chosen for the search ellipse after assessment of trial run results for 50 meter, 75 meter and 125 meter ranges. The 100 meter model produced grade distribution patterns most closely resembling those expected from the geological model and consistent with the authors' experience in the district.

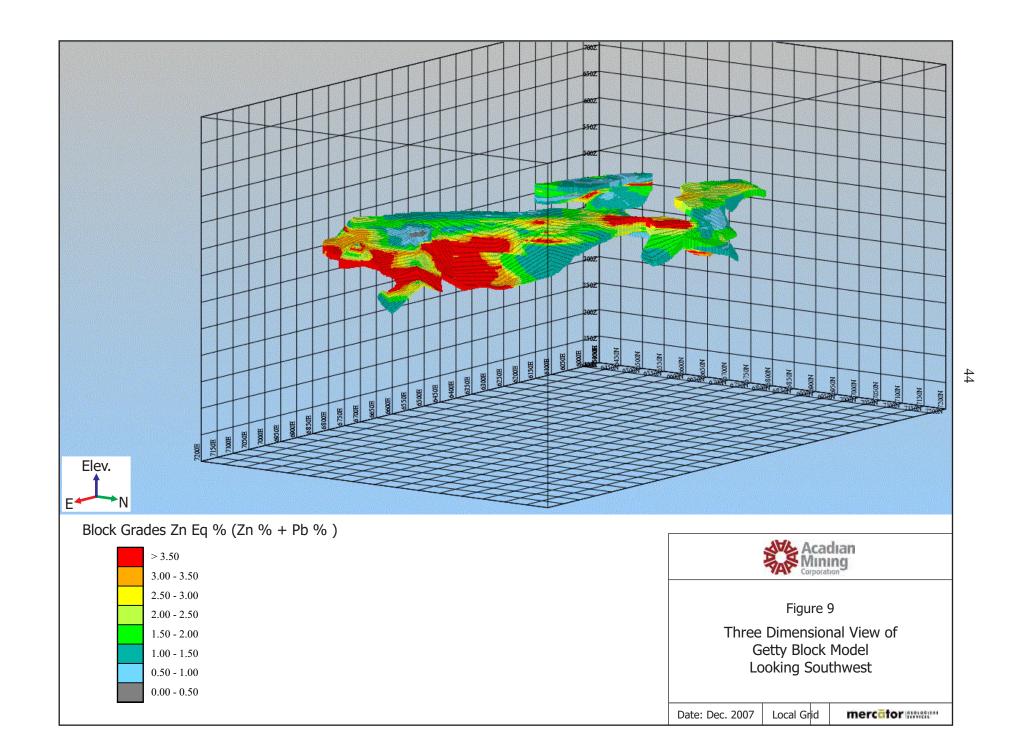
A single pass of ID² grade interpolation using an isotropic search ellipse having a 100 meter range described above was completed and results were reported at grade thresholds of 1.50%, 2.00%, 2.50% and 3.00% zinc equivalent. Resulting grade distribution within the model was assessed against a set of vertical geological and grade cross sections cut through the deposit at 100 meter intervals and also against a set of horizontal sections cut through the model at 10 meter elevation intervals. Results were considered acceptable against the geological model

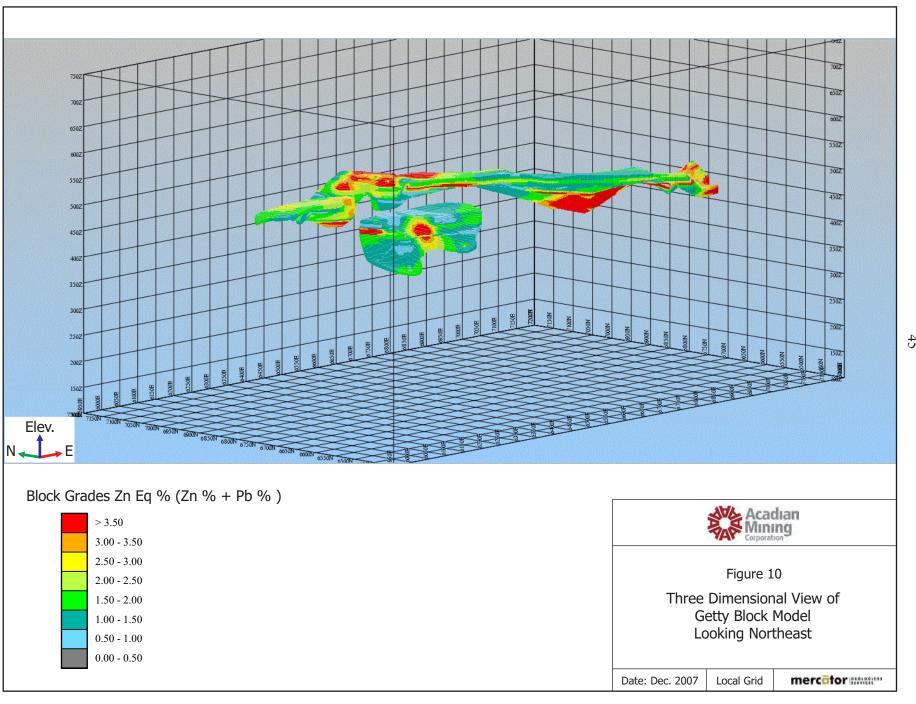
Block grade, block density and block volume parameters estimated for the deposit were combined to arrive at the final deposit tonnage and grade estimate that is presented in Table 18 below. Results are considered compliant with Canadian Institute of Mining, Metallurgy and Petroleum Standards on Mineral Resources and Reserves: *Definitions and Guidelines* (the CIMM Standards) as well as disclosure requirements of National Instrument 43-101. All resources are classified in the Inferred category and factors supporting such classification are discussed below in report sections 16.3.9 and 16.3.10. Figures 9, 10 and 11 present perspective views of the block model and a detailed plan

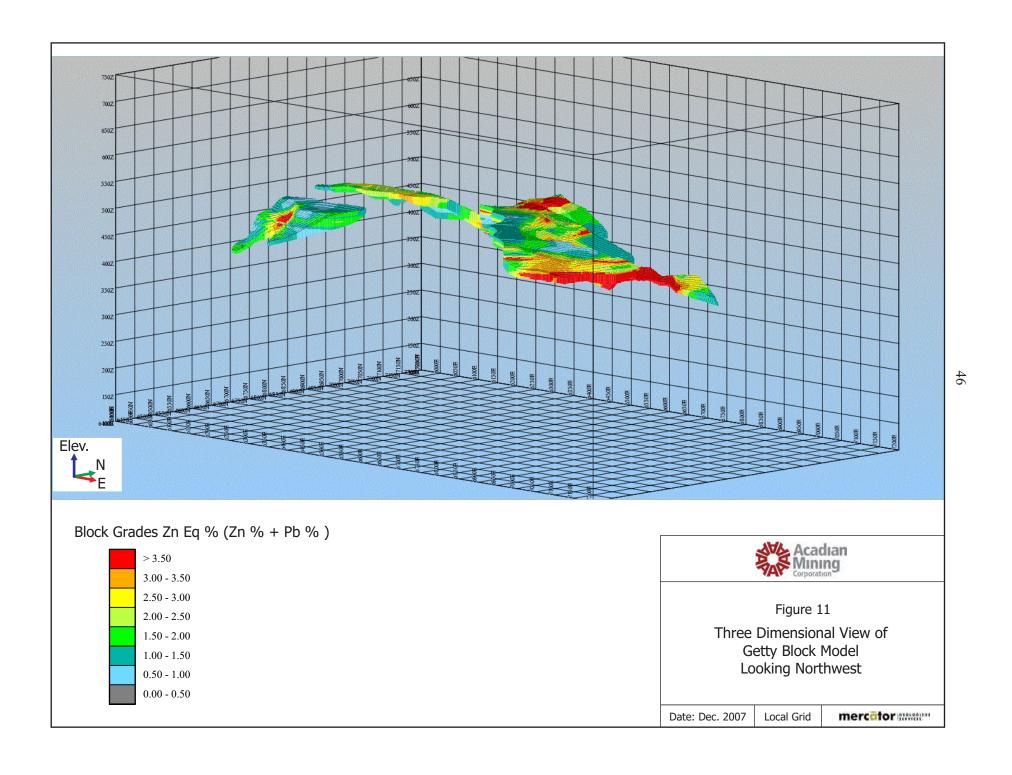
Table 18: Mineral Resource Estimate For Getty Deposit – December 12th, 2007

| Resource Category | Zn Equivalent % Threshold* | Tonnes (Rounded) | Lead % | Zinc % | Zinc% + Lead % |
|----------------------|-------------------------------|------------------|--------|--------|----------------|
| Inferred | 2.00 | 4,160,000 | 1.40% | 1.81% | 3.21% |
| Inferred | 2.50 | 2,860,000 | 1.60% | 2.06% | 3.66% |
| Inferred | 3.00 | 1,970,000 | 1.82% | 2.26% | 4.08% |
| Inferred | 3.50 | 1,300,000 | 2.09% | 2.42% | 4.51% |

*Note: Zn Equivalent calculated as Zn Equivalent = (Zn% + Pb%) based on averaged July to October 2007 zinc and lead market pricing







projection is included in Appendix 4 along with a set of horizontal sections at 10 meter vertical increments and 3 representative vertical cross sections through the model.

16.3.9 Resource Category Definitions

Definitions of mineral resource and associated mineral resource categories used in this report are those recognized under National Instrument 43-101 and set out in the Canadian Institute of Mining, Metallurgy and Petroleum Standards On Mineral Resources and Reserves *Definitions and Guidelines* (the CIMM Standards). These are set out below:

Mineral Resource

A "Mineral Resource" is a concentration or occurrence of natural, solid, inorganic or fossilized organic material in or on the earth's crust in such form and quantity and of such a grade or quality that it has reasonable prospects for economic extraction. The location, quantity, grade, geological characteristics and continuity of a Mineral Resource are known, estimated or interpreted from specific geological evidence and knowledge.

Inferred Mineral Resource

An "Inferred Mineral Resource" is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics, can be estimated on the basis of geological evidence and limited sampling and reasonably assumed, but not verified, geological and grade continuity. The estimate is based on limited information and sampling gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes.

<u>Indicated Mineral Resource</u>

An "Indicated Mineral Resource" is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters to support mine planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings, and drill holes, that are spaced closely enough for geological and grade continuity to be reasonably assumed.

Measured Mineral Resource

A "Measured Mineral Resource" is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters, to support production planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings, and drill holes, that are spaced closely enough to confirm both geological and grade continuity.

16.3.10 Resource Classification

All mineral resources presented in the current estimate have been assigned to the Inferred resource category. This reflects consideration of several factors, including drill hole spacing and geological interpretations, but the most important contributing factor is the historic nature of essentially all geological logs and assay data used in the estimate, and inability to provide a complete validation record for the historic drilling results back to originally associated laboratory certificates. In balance, validation of the earlier results through Acadian's hole twinning and core-re-sampling programs showed no reason to doubt the earlier data set and at least three major mining firms have used the same data to calculate grade and tonnage estimates for the deposit. In combination, these factors are considered to provide an adequate technical basis for classification of the current resource estimate to the Inferred category.

16.3.11 Validation Of Model

Visual Comparison To Geological Sections

Results of block modeling were compared on a section by section basis with corresponding interpreted geological and grade distribution sections prepared prior to block model development. This showed that block model grade patterns show reasonable correlation with those interpreted from the geological sections and that the stratabound character of the mineralization was being properly represented. Results of visual inspection are interpreted as showing an acceptable degree of consistency between the block model and the independently derived sectional interpretation., thusly providing a measure of validation against the geological model developed for the deposit.

Comparison of Composite Database and Block Model Grades

Descriptive statistics were calculated for the entire drill hole composite population intercepting the deposit solid and these were compared to values calculated for corresponding block model figures. The mean drill hole composite grades of 1.19% zinc and 0.87% lead were found to compare acceptably with the 1.27% zinc and 0.87% lead corresponding grades of the total block model, thereby providing a general check on the model with respect to the underlying total assay composite population. Table 19 presents results of the comparison.

Table 19: Drill Hole Composite Grades And Total Resource Solid Grade Comparison

| Parameter | Total Solid Gra | nde | 1 Meter Composites | | |
|-----------|-----------------|------|--------------------|------|--|
| Element | Zn % Pb % | | Zn % | Pb % | |
| Mean | 1.27 | 0.87 | 1.19 | 0.87 | |

Comparison of With Nearest Neighbour Grade Interpolation Model

The ID² block model was checked using Nearest Neighbour (NN) grade interpolation methodology within the same resource solid used for the ID² method. At the 2% zinc equivalent threshold this resulted in definition of 4,270,000 tonnes (rounded) at an average zinc grade of 1.72% and average lead grade of 1.45% (Table 20). These results generally confirm the 4,160, 000 tonnes at 1.81% zinc and 1.40% lead reported for the ID² method. At higher threshold values, grades from the NN model exceed those for ID² with associated category tonnages being lower. This was an anticipated result of the method comparison and with this in mind, overall results of the NN model at the lowest threshold value were considered a reasonable check on the preferred ID² model results. Weighted average drill hole ntercepts used in the NN estimate appear in Appendix 2.

Table 20: Results Of Nearest Neighbour Block Model Estimate

| *Equivalent Zn% Threshold | Tonnes (Rounded) | Pb % | Zn % | *Zinc +Pb % |
|---------------------------|------------------|------|------|-------------|
| 2.00 | 4,270,000 | 1.45 | 1.72 | 3.18 |
| 2.50 | 3,450,000 | 1.62 | 1.81 | 3.42 |
| 3.00 | 1,780,000 | 2.05 | 2.05 | 4.09 |
| 3.50 | 890,000 | 2.43 | 2.46 | 4.89 |

*Note: Zn Equivalent calculated as Zn Equivalent = (Zn% + Pb%) based on averaged July to October 2007 zinc and lead market pricing

16.4 Comments On Previous Resource or Reserve Estimates

Three historic mineral resource estimates were reviewed for purposes of this report and these were referenced previously in section 5.2. The first was prepared in 1976 for Getty

by MPH Consulting Limited (Riddell, 1976) and apparently followed earlier in-house estimates by Getty. Subsequently, an in-house assessment was prepared by Esso (MacLeod, 1980) and in 1992 Westminer also completed an estimate (Hudgins and Lamb, 1992). Results of these programs are presented in Table 21 below and, as noted earlier, all are historic in nature, pre-date NI 43-101 and are not compliant with current CIMM Standards. As such, they should not be relied upon.

Table 21: Historic Tonnage And Grade Estimates - Getty Zn-Pb Deposit (Estimates Are Not Compliant With NI 43-101 or CIMM Standards)

| Reference | Cutoff | Tonnes | Pb % | Zn % | Zn + Pb % |
|---------------------------|---------------|-----------|------|------|-----------|
| Riddell (1976) | 2% Zn + Pb | 4,005,000 | 1.84 | 1.87 | 3.02 |
| *MacLeod (1980) | 1.5% Zn +Pb | 3,078,000 | 1.37 | 1.60 | 2.97 |
| **Hudgins and Lamb (1992) | **1.5% Zn Eq. | 4,500,000 | 1.33 | 1.87 | 3.20 |

^{*} Diluted and Minable; **Zn Eq. = Zn% + 0.60 xPb%

Support documents provided for the historic estimates showed that those of Getty and Esso were based on drill-hole-centered polygonal methods with tonnage weighting to establish final deposit grade. A single density factor of 11.5 cubic feet per ton (~2.78g/cm3) was used in the Riddell (1976) estimate and this appears to have been used by MacLeod (1980) before application of a 10% tonnage reduction factor to drill hole intercepts. Westminer employed a cross-sectional method using Surpac© mining software to determine resource area limits and volume and used a single density factor of 2.75g/cm3 to estimate tonnage. Deposit grade was calculated as the length-weighted average of all drill hole intercepts but spatial distribution of grade within the deposit was not specifically addressed.

A summary review of supporting file information for the historic estimates was completed for current purposes and it is apparent that the noticeably lower tonnage figure quoted by Esso reflects exclusion of certain drill holes based on the report's development potential assumptions. The higher lead grade in the MPH estimate is also notable but main contributing factors were not clearly identified.

Riddell (1976) completed a preliminary economic assessment for open pit development of a 3.6 million ton (3.3 million tonne) portion of the deposit at a diluted grade of 1.28% Pb and 1.74% Zn. Modeling parameters included options of a stand-alone mill, custom milling of ore at Esso's adjacent Gays River site and development of a jointly-owned mill complex in association with Esso. Analysis showed that a 20 year model producing at 182,000 tons per year with a dedicated mill was uneconomic. However, 10 year projects producing at 375,000 tons per year were financially attractive in both the custom milling and jointly owned mill models.

In 1980 Esso reported on economic aspects of developing the deposit based on an insitu tonnage and grade model of 3.1 million diluted tons (2.8 million tonnes) grading 1.37% Pb and 1.60% Zn (MacLeod, 1980). This study concluded that mining the deposit through open-pit methods as an ore supplement to the Gays River deposit was economically viable, provided that important operating assumptions were met. Positive Net Present Value figures at 15% discounting were returned for 1000 and 1250 ton per day production rates, with the Gays River operation absorbing certain operating and capital cost components. George (1985) again reviewed deposit economics for Getty and used economic analysis applied to tonnage and grade curves to show that a deposit size of approximately 8 million tons was necessary to justify stand-alone profitable development at realizable metal grades. The earlier MPH work was also reviewed and some of the economic models updated. None of the work indicated that profitable stand-alone development of the deposit could be expected under existing market conditions of the time.

Hudgins and Lamb (1992) reported on preliminary economic analysis of a 3.9 million tonne portion of the total resource at their assigned grade and concluded that a positive economic case could be made for development of the property as a "top-up" source of feed for the Gays River concentrator. Assumptions included sharing of various operating costs with the Gays River operation and that the full 1500 tonne per day capacity of the Gays River concentrator would not be required for underground production from that Esso property, thereby providing excess capacity for Getty ore.

In review, each of the historic estimates reflects specific assumptions considered appropriate at the time of preparation. This includes exclusion of certain historic drill holes, establishment of different maximum depth criteria and use of differing minimum grade and width cut off values. The current estimate does not directly reflect any of the parameter sets used in the early programs and results are therefore different. However, all historic programs model the Getty deposit as a relatively low grade accumulation of lead and zinc having potential for open pit development. From the grade and tonnage perspective the earlier estimates are generally consistent with results of the current estimate and provide useful and relevant views of the deposit under historic market conditions.

17.0 Other Relevant Data and Information

17.1 Environmental and Surface Title Liabilities

The Getty deposit underlies an area of predominantly cleared land with limited peripheral forest cover that is being actively used for agricultural purposes. This primarily reflects

one dairy farming operation with associated infrastructure. No obvious environmental liabilities with respect to current land use in the deposit area deposit were known to the authors at the report date and no such liabilities had been communicated by Acadian personnel. However, this comment does not constitute a professional opinion with respect to environmental status of the property. Presence of the Gays River watercourse along a portion of the deposit's eastern margin has required enhanced diligence with respect to surface exploration activities such as drilling and the authors surmise that proximity to the river will remain an important consideration in any development evaluation or planning efforts.

In addition to the above, status and details of surface rights, titles and land access agreements were not reviewed by the authors for purposes of this report. However, Acadian has advised that no difficulties exist to date on this front and that the company has established access agreements to allow all current work programs to be carried out. On a related point, surface rights holders in Nova Scotia typically hold title to gypsum and limestone occurring on their lands. In some instances gypsum and/or limestone rights have been severed from the surface title or legal agreements have been made that bear on their ownership. While current status of gypsum title was not investigated by the authors for report purposes, this point is noted as being relevant to assessment of future development options for the deposit. As in the preceding case, no professional opinion is being provided with respect to surface or mineral right titles.

18.0 Interpretation and Conclusions

The Getty zinc lead deposit is a carbonate hosted, stratabound lead – zinc deposit of the Mississippi Valley Type (MVT) that exists as an extension to the Scotia Mine zinc-lead deposit located approximately 1700 meters to the southeast. Dolomitized carbonate bank lithologies are continuously present, variably mineralized and correlative between the two deposits, but mineral resource limits for the deposits do not adjoin at present. Both are developed in carbonate bank lithologies of the Gays River Formation that occur along discrete paleo-topographic highs consisting of Cambro-Ordovician Goldenville Formation greywacke. Bank morphology in the Getty area differs from that at Scotia Mine by having generally shallower bank-front slopes. The Scotia Mine deposit has higher overall lead and zinc resource grades than Getty and these reflect higher proportions of submassive to massive sphalerite and galena along moderate to steeply dipping (40° o to 70°) bank-front intervals. Lack of comparable high grade material in moderate to steeply dipping bank font intervals accounts for the lower average zinc and lead resource grades that apply to the Getty deposit.

Review and validation of historic Getty exploration data and incorporation of results from core re-sampling and twinning programs completed for the current estimate showed that historic data were of acceptable quality for resource estimation purposes. On this basis, a fully constrained three dimensional block model for the deposit was developed using Surpac© 6.02 deposit modeling software. Block size was established as 2.5 meters by 2.5 meters x 2.5 meters with sub-blocking at 1.25 meters by 1.25 meters by 1.25 meters. Grade interpolation was accomplished using Inverse Distance Squared (ID²) methodology using an omni-directional interpolation ellipse with a range of 100 meters. The model was fully constrained within a deposit solid based on a minimum meter % zinc equivalent (zinc % + lead %) value of 4.00 and a 3.0 meter minimum downhole intercept length parameter. The cutoff criteria for the solid reflects relatively near-surface position of most deposit tonnage and associated potential for open pit development. Table 22 below reports the resource estimate, all of which has been classified in the Inferred category based on factors reflecting quality of historic drilling data and historic drill hole spacing.

Table 22: Mineral Resource Estimate For Getty Deposit – December 12th, 2007

| Resource Category | Zn Equivalent % Threshold* | Tonnes (Rounded) | Lead % | Zinc % | Zinc% + Lead % |
|----------------------|-------------------------------|------------------|--------|--------|----------------|
| Inferred | 2.00 | 4,160,000 | 1.40% | 1.81% | 3.21% |
| Inferred | 2.50 | 2,860,000 | 1.60% | 2.06% | 3.66% |
| Inferred | 3.00 | 1,970,000 | 1.82% | 2.26% | 4.08% |
| Inferred | 3.50 | 1,300,000 | 2.09% | 2.42% | 4.51% |

*Note: Zn Equivalent calculated as Zn Equivalent = (Zn% + Pb%) based on averaged July to October 2007 zinc and lead market pricing

19.0 Recommendations

Based on results of the resource estimation program summarized above, the following recommendations are provided with respect to future exploration and resource delineation programs for the Getty deposit.

- 1. Additional twinning and re-sampling of historic drill holes should be completed to provide coverage over the entire extent of the deposit outline. This should include a minimum of 5 additional twin holes and re-sampling of at least 5 additional historic holes. Results should be closely assessed against earlier logs and assay data.
- 2. The QA/QC program should be modified slightly to include insertion of standard and blank samples in direct sequence with all higher grade intercepts, regardless of their location relative to the systematized insertions currently in place.

An additional certified standard in the 5% to 8% zinc and 1% to 4% lead range should be procured for such use.

- 3. A project database of specific gravity data should be established with representation across the complete grade range of the deposit. Data should be acquired from every Acadian drill hole and include representation of the nonmineralized host rock sequences such as anhydrite, gypsum, basal breccia and Goldenville Formation greywacke.
- 4. Upgrading of current Inferred category resources to higher resource categories will require additional core drilling at closer hole spacing. Based on configuration of the bank structure and location/alignment of historic holes, the current Acadian hole spacing of 50 meters by 50 meters should provide sufficient data and confidence in correlation to support delineation of Indicated resources. Establishment of Measured category parameters should reflect review of the 50 meter by 50 meter drilling pattern results.
- 5. A digital elevation database should be developed for the deposit area with resolution in the 1.0 meter or less range. Data could be cost-effectively acquired by a ground crew using survey quality Differential Geographic Positioning System (DGPS) methods.
- 6. Getty deposit limits are well defined at present but work by Acadian to the west in the Carrolls Farm and Carrolls Corner areas indicates presence of a series of mineralized carbonate banks that extend southwesterly from the Getty deposit's west flank. Potential for similar extensions is also present to the northwest of the deposit. These areas should be tested by core drilling on a priority basis with the southwest extension opportunity considered highest in relative priority.

| Respectfully submitted, [Original signed by] | [Original signed by] |
|---|---|
| Michael P. Cullen, M.Sc. (Geol.), P. Geo. Senior Geologist | Chrystal Kennedy, B.Sc. (Geol.), P. Geo. Senior Project Geologist |
| [Original signed by] | |
| Matthew Harrington, B.Sc. (Geol.) Geologist | Date: March 25, 2008 |

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Appendix 1: Statements of Qualifications

MERCATOR GEOLOGICAL SERVICES LIMITED

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CERTIFICATE of AUTHOR

- I, Michael P. Cullen, P. Geo. do hereby certify that:
 - 1. I am currently employed as a Senior Geologist by:

Mercator Geological Services Limited 65 Queen St Dartmouth, Nova Scotia, Canada B2Y 1GA

- 2. I graduated with a Masters Degree in Science (Geology) from Dalhousie University in 1984. In addition, I obtained a Bachelor of Science degree (Honours, Geology) in 1980 from Mount Allison University.
- 3. I am a registered member in good standing of the Association of Professional Geoscientists of Nova Scotia, registration number 064.
- 4. I have worked as a geologist in Canada and internationally since graduation from university.
- 5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101
- 6. I am one of the qualified person responsible for preparation of the technical report entitled:

TECHNICAL REPORT ON
MINERAL RESOURCE ESTIMATE
GETTY ZINC - LEAD DEPOSIT
GAYS RIVER AREA
HALIFAX COUNTY, NOVA SCOTIA
CANADA
NTS 11E03B

Effective Date: December 12, 2007

7. I have visited the Getty Property on numerous occasions since September, 2006 and most recently visited the property on September 17th, 2007 at which time diamond drill core was examined and Acadian's core logging facility at the Scotia Mine site was also visited. Since September, 2006 I

- have participated in numerous meetings with Mercator and Acadian staff regarding Getty deposit geology.
- 8. I am responsible for supervision of all aspects of report preparation and specifically responsible for report sections 1, 6, 7, 8, 16, 17, 18 and 19.
- 9. I previously reviewed and reported on historic Getty deposit drilling results on behalf of Savage Zinc Inc., this work being carried out by Mercator Geological Services Limited on a fee for service basis in 2001.
- 10. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.
- 11. I am independent of the issuer applying all of the tests in section 1.5 of National Instrument 43-101.
- 12. I have read National Instrument 43-101 and Form 43-101F1, and believe that this Technical Report has been prepared in compliance with that instrument and form.
- 13. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 25th Day of March, 2008

[Original signed and sealed by]

Michael P. Cullen, M. Sc., P. Geo. Senior Geologist Mercator Geological Services Limited

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CERTIFICATE of AUTHOR

- I, Chrystal Kennedy, B.Sc. (Geol.), P. Geo. do hereby certify that:
 - 1. I am currently employed as a Senior Geologist by:

Mercator Geological Services Limited 65 Queen St Dartmouth, Nova Scotia, Canada B2Y 1GA

- 2. I graduated with a Bachelor of Science Degree (Adv. Major Geology) from Dalhousie University in 1996. In addition, I obtained a Bachelor of Science degree (Honours, Biology) in 1993 from Dalhousie University.
- 3. I am a registered member in good standing of the Association of Professional Geoscientists of Nova Scotia, registration number 105.
- 4. I have worked as a geologist in Canada since 1996.
- 5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101
- 6. I am one of the qualified persons responsible for preparation of the technical report entitled:

TECHNICAL REPORT ON
MINERAL RESOURCE ESTIMATE
GETTY ZINC - LEAD DEPOSIT
GAYS RIVER AREA
HALIFAX COUNTY, NOVA SCOTIA
CANADA
NTS 11E03B

Effective Date: December 12, 2007

7. I have visited the Getty Property on numerous occasions since September,

7. I have visited the Getty Property on numerous occasions since September, 2006 and most recently visited the property on Febuary 11, 2008. I am currently responsible for supervision of a diamond drilling program being carried out on the Getty property by Acadian Mining Corp. I have

examined core logging and sampling facilities at Acadian's Scotia Mine site and have participated in numerous meetings with Mercator and Acadian staff regarding Getty deposit geology.

- 8. I am responsible for preparation of report sections 2, 3, 4, 9, 10, 11, 12, 15, and 20 and contributed to sections 5, 6, 7, 8, 16, 18 and 19.
- 9. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.
- 10. I am independent of the issuer applying all of the tests in section 1.5 of National Instrument 43-101.
- 11. I have read National Instrument 43-101 and Form 43-101F1, and believe that this Technical Report has been prepared in compliance with that instrument and form.
- 12. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 25th Day of March, 2008

[Original signed and sealed by]

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CERTIFICATE of AUTHOR

- I, Matthew Harrington, B.Sc. (Geol.), do hereby certify that:
 - 1. I currently reside in Halifax, Nova Scotia Canada and am employed as a Geologist by:

Mercator Geological Services Limited 65 Queen St Dartmouth, Nova Scotia, Canada B2Y 1GA

- 2. I graduated with a Bachelor of Science (Geol.) degree from Dalhousie University in Halifax, Nova Scotia, Canada in 2003.
- 3. I have worked as a geologist in Canada for 4 years since graduation from university and have been employed by Mercator geological Services since 2003.
- 4. I participated in preparation of the Getty deposit mineral resource estimate and three dimension block model described in the technical report named below. My participation was supervised by Mr. Michael P. Cullen, P. Geo. and Ms. Chrystal Kennedy, P. Geo.

TECHNICAL REPORT ON
MINERAL RESOURCE ESTIMATE
GETTY ZINC - LEAD DEPOSIT
GAYS RIVER AREA
HALIFAX COUNTY, NOVA SCOTIA
CANADA
NTS 11E03B
Effective Date: December 12, 2007

- 5. I have not visited the property that is the subject of this Technical Report.
- 6. I specifically contributed to report sections 16, 18 and 19.
- 7. I have no prior involvement with the property that is the subject of the Technical Report.
- 8. I am independent of the issuer applying all of the tests in section 1.5 of National Instrument 43-101.

9. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 25th Day of March, 2008

[Original signed by]

Matthew Harrington, B. Sc. (Geol.) Geologist Mercator Geological Services Limited

Appendix 2: Drilling Related Dcouments

Drill Hole Collar Coordinate and Survey Listing
Listing of 1 Meter Assay Composites Within Resource Solid
Listing Of Nearest Neighbour Drill Hole Intercepts
Acadian Lithocode Descriptions
LME Metal Pricing Summary
Laboratory Procedure Summaries

ACADIAN MINING CORP.

Table A-1: Getty Resource Estimate - December 2007

Listing of Getty Project Drill Holes With Coordinates and Survey Data

| | Local Grid | Local Grid | Local Grid | | | | Included in December | |
|---------|-------------|--------------|---------------|-----------|-----|---------|-----------------------|-------------|
| Hole Id | Easting (m) | Northing (m) | Elevation (m) | Depth (m) | Dip | Azimuth | 2007 Resource Outline | Drilled By |
| GGR012 | 7617.83 | 6616.13 | 519.66 | 101.04 | -90 | 0 | NO | Getty Mines |
| GGR013 | 7374.23 | 6621.59 | 513.62 | 169.50 | -90 | 0 | NO | Getty Mines |
| GGR014 | 7497.14 | 6613.84 | 514.26 | 144.80 | -90 | 0 | NO | Getty Mines |
| GGR015 | 7121.37 | 6641.60 | 523.93 | 112.80 | -90 | 0 | NO | Getty Mines |
| GGR017 | 7732.86 | 6672.02 | 535.00 | 144.50 | -90 | 0 | NO | Getty Mines |
| GGR018 | 6983.94 | 6653.60 | 535.38 | 67.40 | -90 | 0 | NO | Getty Mines |
| GGR019 | 6877.31 | 6658.86 | 542.96 | 66.80 | -90 | 0 | YES | Getty Mines |
| GGR020 | 6630.77 | 6628.38 | 561.67 | 62.80 | -90 | 0 | NO | Getty Mines |
| GGR021 | 6756.30 | 6628.57 | 549.68 | 57.30 | -90 | 0 | YES | Getty Mines |
| GGR022 | 6931.49 | 6641.35 | 539.06 | 71.02 | -90 | 0 | YES | Getty Mines |
| GGR023 | 7063.97 | 6652.07 | 527.74 | 85.04 | -90 | 0 | NO | Getty Mines |
| GGR024 | 7014.19 | 6765.62 | 526.58 | 78.94 | -90 | 0 | YES | Getty Mines |
| GGR025 | 6872.51 | 6764.38 | 543.16 | 139.60 | -90 | 0 | NO | Getty Mines |
| GGR025A | 6874.55 | 6768.11 | 543.13 | 139.60 | -90 | 0 | YES | Getty Mines |
| GGR026 | 6760.72 | 6759.28 | 547.53 | 93.30 | -90 | 0 | YES | Getty Mines |
| GGR027 | 6636.42 | 6755.27 | 554.53 | 56.40 | -90 | 0 | YES | Getty Mines |
| GGR028 | 6516.48 | 6760.60 | 554.96 | 56.10 | -90 | 0 | NO | Getty Mines |
| GGR029 | 6397.32 | 6757.72 | 553.31 | 39.01 | -90 | 0 | NO | Getty Mines |
| GGR030 | 6252.36 | 6777.16 | 537.09 | 21.80 | -90 | 0 | NO | Getty Mines |
| GGR031 | 5985.54 | 6755.89 | 525.36 | 96.01 | -90 | 0 | NO | Getty Mines |
| GGR032 | 7116.82 | 6775.98 | 513.72 | 98.80 | -90 | 0 | YES | Getty Mines |
| GGR033 | 6882.52 | 7005.26 | 537.00 | 164.00 | -90 | 0 | NO | Getty Mines |
| GGR033A | 6852.04 | 7004.99 | 540.00 | 170.08 | -90 | 0 | NO | Getty Mines |
| GGR034 | 6760.61 | 7004.18 | 543.37 | 164.59 | -90 | 0 | NO | Getty Mines |
| GGR035 | 6639.07 | 7006.17 | 545.10 | 94.20 | -90 | 0 | NO | Getty Mines |
| GGR035A | 6602.04 | 7005.14 | 545.95 | 98.15 | -90 | 0 | YES | Getty Mines |
| GGR036 | 6633.62 | 6884.17 | 550.51 | 91.44 | -90 | 0 | YES | Getty Mines |
| GGR037 | 6510.67 | 6997.37 | 553.07 | 75.60 | -90 | 0 | YES | Getty Mines |
| GGR038 | 6508.73 | 6889.20 | 557.08 | 97.54 | -90 | 0 | YES | Getty Mines |
| GGR039 | 6382.04 | 6996.25 | 550.32 | 118.90 | -90 | 0 | NO | Getty Mines |
| GGR039A | 6432.71 | 6986.68 | 552.83 | 106.70 | -90 | 0 | YES | Getty Mines |
| GGR040 | 6761.69 | 6882.26 | 545.84 | 85.34 | -90 | 0 | YES | Getty Mines |
| GGR041 | 6899.25 | 6871.29 | 542.00 | 73.20 | -90 | 0 | NO | Getty Mines |

ACADIAN MINING CORP.

Table A-1: Getty Resource Estimate - December 2007

Listing of Getty Project Drill Holes With Coordinates and Survey Data

| | Local Grid | Local Grid | Local Grid | | | | Included in December | |
|---------|-------------|--------------|---------------|-----------|-----|---------|-----------------------|-------------|
| Hole Id | Easting (m) | Northing (m) | Elevation (m) | Depth (m) | Dip | Azimuth | 2007 Resource Outline | Drilled By |
| GGR041A | 6909.55 | 6879.00 | 540.97 | 73.15 | -90 | 0 | NO | Getty Mines |
| GGR042 | 6266.96 | 6987.61 | 538.50 | 105.20 | -90 | 0 | NO | Getty Mines |
| GGR043 | 6514.17 | 7123.92 | 548.00 | 101.35 | -90 | 0 | NO | Getty Mines |
| GGR044 | 6383.33 | 7131.90 | 547.00 | 115.80 | -90 | 0 | NO | Getty Mines |
| GGR044A | 6381.49 | 7133.41 | 549.50 | 103.63 | -90 | 0 | NO | Getty Mines |
| GGR044B | 6364.81 | 7123.51 | 552.00 | 115.82 | -90 | 0 | NO | Getty Mines |
| GGR045 | 6300.51 | 7122.33 | 539.00 | 149.40 | -90 | 0 | NO | Getty Mines |
| GGR046 | 6393.02 | 6898.50 | 550.11 | 87.50 | -90 | 0 | NO | Getty Mines |
| GGR066 | 7423.52 | 7697.41 | 550.00 | 289.00 | -90 | 0 | NO | Getty Mines |
| GGR067 | 7259.03 | 7513.06 | 550.00 | 151.80 | -90 | 0 | NO | Getty Mines |
| GGR068 | 7621.99 | 6731.08 | 522.00 | 169.20 | -90 | 0 | NO | Getty Mines |
| GGR069 | 4505.94 | 7103.97 | 550.00 | 125.00 | -90 | 0 | NO | Getty Mines |
| GGR070 | 7470.33 | 6887.33 | 520.00 | 143.60 | -90 | 0 | NO | Getty Mines |
| GGR071 | 6454.22 | 7215.44 | 542.50 | 152.10 | -90 | 0 | NO | Getty Mines |
| GGR072 | 7467.61 | 6884.87 | 522.00 | 135.33 | -90 | 0 | NO | Getty Mines |
| GGR073 | 4976.98 | 6988.36 | 550.00 | 342.60 | -90 | 0 | NO | Getty Mines |
| GGR074 | 7386.33 | 7250.53 | 545.00 | 154.84 | -90 | 0 | NO | Getty Mines |
| GGR075 | 6321.39 | 7311.50 | 545.00 | 128.02 | -90 | 0 | NO | Getty Mines |
| GGR076 | 6215.32 | 7241.67 | 532.00 | 176.50 | -90 | 0 | NO | Getty Mines |
| GGR077 | 7339.51 | 7615.58 | 550.00 | 212.80 | -90 | 0 | NO | Getty Mines |
| GGR078 | 6159.59 | 6995.19 | 534.00 | 100.00 | -90 | 0 | NO | Getty Mines |
| GGR079 | 6270.65 | 6877.94 | 535.97 | 57.91 | -90 | 0 | YES | Getty Mines |
| GGR080 | 5771.97 | 6744.24 | 520.00 | 139.90 | -90 | 0 | NO | Getty Mines |
| GGR081 | 6179.99 | 6868.08 | 539.73 | 60.96 | -90 | 0 | YES | Getty Mines |
| GGR082 | 6030.22 | 6872.73 | 531.00 | 64.01 | -90 | 0 | NO | Getty Mines |
| GGR083 | 5515.72 | 6869.69 | 519.00 | 94.50 | -90 | 0 | NO | Getty Mines |
| GGR084 | 5516.76 | 6752.95 | 519.00 | 212.80 | -90 | 0 | NO | Getty Mines |
| GGR086 | 5802.28 | 6865.83 | 525.00 | 140.21 | -90 | 0 | NO | Getty Mines |
| GGR087 | 6186.70 | 6757.68 | 532.00 | 33.53 | -90 | 0 | NO | Getty Mines |
| GGR088 | 5907.53 | 6993.26 | 528.00 | 103.02 | -90 | 0 | NO | Getty Mines |
| GGR089 | 5882.51 | 6756.20 | 520.00 | 113.70 | -90 | 0 | NO | Getty Mines |
| GGR090 | 6867.27 | 6903.62 | 540.00 | 145.70 | -90 | 0 | NO | Getty Mines |
| GGR091 | 5903.42 | 7009.68 | 519.00 | 138.84 | -90 | 0 | NO | Getty Mines |

ACADIAN MINING CORP.

Table A-1: Getty Resource Estimate - December 2007

Listing of Getty Project Drill Holes With Coordinates and Survey Data

| l | Local Grid | Local Grid | Local Grid | | | | Included in December | |
|---------|-------------|--------------|---------------|-----------|-----|---------|-----------------------|-------------|
| Hole Id | Easting (m) | Northing (m) | Elevation (m) | Depth (m) | Dip | Azimuth | 2007 Resource Outline | Drilled By |
| GGR092 | 6530.99 | 6636.98 | 565.00 | 79.20 | -90 | 0 | NO | Getty Mines |
| GGR093 | 6337.78 | 6631.60 | 548.00 | 50.30 | -90 | 0 | YES | Getty Mines |
| GGR094 | 6259.53 | 6621.77 | 539.00 | 44.81 | -90 | 0 | YES | Getty Mines |
| GGR095 | 6150.25 | 7120.69 | 532.00 | 136.60 | -90 | 0 | NO | Getty Mines |
| GGR096 | 6148.19 | 6631.45 | 531.00 | 93.00 | -90 | 0 | YES | Getty Mines |
| GGR097 | 6023.20 | 6633.69 | 526.00 | 146.30 | -90 | 0 | NO | Getty Mines |
| GGR098 | 6027.76 | 7149.78 | 531.00 | 133.50 | -90 | 0 | NO | Getty Mines |
| GGR099 | 5904.37 | 6627.76 | 523.00 | 210.31 | -90 | 0 | NO | Getty Mines |
| GGR101 | 6022.32 | 6526.09 | 528.00 | 149.40 | -90 | 0 | NO | Getty Mines |
| GGR102 | 6145.95 | 6540.59 | 531.00 | 105.20 | -90 | 0 | YES | Getty Mines |
| GGR103 | 6267.52 | 6512.10 | 542.00 | 86.90 | -90 | 0 | YES | Getty Mines |
| GGR104 | 7248.46 | 6642.73 | 522.00 | 131.10 | -90 | 0 | NO | Getty Mines |
| GGR105 | 7241.90 | 6764.60 | 522.00 | 125.00 | -90 | 0 | NO | Getty Mines |
| GGR109 | 7373.99 | 6752.36 | 517.00 | 146.30 | -90 | 0 | NO | Getty Mines |
| GGR110 | 6572.52 | 7246.36 | 540.00 | 122.53 | -90 | 0 | NO | Getty Mines |
| GGR111 | 6219.00 | 6937.00 | 535.14 | 96.93 | -90 | 0 | NO | Getty Mines |
| GGR112 | 6456.54 | 6940.85 | 552.00 | 100.60 | -90 | 0 | NO | Getty Mines |
| GGR113 | 6349.37 | 6951.91 | 547.67 | 80.80 | -90 | 0 | NO | Getty Mines |
| GGR113A | 6314.64 | 6952.33 | 543.03 | 88.10 | -90 | 0 | YES | Getty Mines |
| GGR114 | 6209.94 | 7058.12 | 533.00 | 157.90 | -90 | 0 | NO | Getty Mines |
| GGR115 | 6333.37 | 7059.83 | 541.00 | 131.70 | -90 | 0 | NO | Getty Mines |
| GGR116 | 6455.35 | 7062.64 | 544.35 | 92.70 | -90 | 0 | YES | Getty Mines |
| GGR117 | 6577.28 | 7063.57 | 545.03 | 90.22 | -90 | 0 | NO | Getty Mines |
| GGR118 | 6578.24 | 6941.57 | 553.45 | 94.50 | -90 | 0 | NO | Getty Mines |
| GGR119 | 6700.49 | 6943.29 | 548.00 | 118.90 | -90 | 0 | NO | Getty Mines |
| GGR121 | 6696.06 | 7064.87 | 544.00 | 129.54 | -90 | 0 | NO | Getty Mines |
| GGR122 | 6823.62 | 6944.38 | 545.50 | 128.02 | -90 | 0 | NO | Getty Mines |
| GGR123 | 6945.04 | 6822.98 | 539.79 | 137.80 | -90 | 0 | NO | Getty Mines |
| GGR124 | 6833.02 | 6816.70 | 547.51 | 129.54 | -90 | 0 | YES | Getty Mines |
| GGR125 | 6937.67 | 6695.79 | 540.02 | 69.50 | -90 | 0 | YES | Getty Mines |
| GGR126 | 6694.59 | 6818.27 | 548.15 | 73.20 | -90 | 0 | YES | Getty Mines |
| GGR129 | 6815.65 | 6701.67 | 548.50 | 103.02 | -90 | 0 | YES | Getty Mines |
| GGR130 | 6576.21 | 6825.64 | 557.60 | 70.10 | -90 | 0 | YES | Getty Mines |

ACADIAN MINING CORP.

Table A-1: Getty Resource Estimate - December 2007

Listing of Getty Project Drill Holes With Coordinates and Survey Data

| | Local Grid | Local Grid | Local Grid | | | | Included in December | |
|---------|-------------|--------------|---------------|-----------|-----|---------|-----------------------|-------------|
| Hole Id | Easting (m) | Northing (m) | Elevation (m) | Depth (m) | Dip | Azimuth | 2007 Resource Outline | Drilled By |
| GGR131 | 6457.44 | 6818.60 | 553.00 | 64.01 | -90 | 0 | NO | Getty Mines |
| GGR132 | 6335.52 | 6817.52 | 540.00 | 42.70 | -90 | 0 | NO | Getty Mines |
| GGR133 | 6696.64 | 6693.62 | 552.13 | 78.33 | -90 | 0 | YES | Getty Mines |
| GGR134 | 6574.48 | 6701.11 | 559.04 | 45.11 | -90 | 0 | NO | Getty Mines |
| GGR135 | 6216.08 | 6811.66 | 537.60 | 48.80 | -90 | 0 | YES | Getty Mines |
| GGR136 | 6091.68 | 6813.84 | 530.62 | 45.50 | -90 | 0 | YES | Getty Mines |
| GGR137 | 6455.47 | 6696.96 | 552.00 | 42.10 | -90 | 0 | NO | Getty Mines |
| GGR138 | 5969.78 | 6814.28 | 523.00 | 90.22 | -90 | 0 | NO | Getty Mines |
| GGR139 | 6335.06 | 6697.72 | 541.00 | 28.04 | -90 | 0 | NO | Getty Mines |
| GGR140 | 7065.07 | 6699.63 | 535.00 | 70.10 | -90 | 0 | NO | Getty Mines |
| GGR141 | 6211.64 | 6694.50 | 524.00 | 23.80 | -90 | 0 | NO | Getty Mines |
| GGR142 | 6089.10 | 6696.63 | 531.00 | 75.30 | -90 | 0 | NO | Getty Mines |
| GGR143 | 7423.62 | 6827.17 | 520.00 | 143.30 | -90 | 0 | NO | Getty Mines |
| GGR144 | 7352.98 | 6887.51 | 519.00 | 146.30 | -90 | 0 | NO | Getty Mines |
| GGR145 | 5967.81 | 6692.33 | 525.00 | 140.21 | -90 | 0 | NO | Getty Mines |
| GGR146 | 6097.88 | 6939.98 | 533.00 | 63.40 | -90 | 0 | NO | Getty Mines |
| GGR147 | 5968.70 | 6936.19 | 527.00 | 100.00 | -90 | 0 | NO | Getty Mines |
| GGR149 | 7660.88 | 6676.87 | 529.00 | 140.21 | -90 | 0 | NO | Getty Mines |
| GGR150 | 7556.06 | 6672.89 | 525.00 | 151.18 | -90 | 0 | NO | Getty Mines |
| GGR151 | 7434.11 | 6674.86 | 519.00 | 149.40 | -90 | 0 | NO | Getty Mines |
| GGR152 | 7313.45 | 6704.27 | 520.00 | 130.50 | -90 | 0 | NO | Getty Mines |
| GGR153 | 7682.07 | 6555.44 | 526.00 | 103.33 | -90 | 0 | NO | Getty Mines |
| GGR154 | 7682.07 | 6555.44 | 526.00 | 76.20 | -90 | 0 | NO | Getty Mines |
| GGR155 | 7730.30 | 6615.91 | 537.00 | 118.90 | -90 | 0 | NO | Getty Mines |
| GGR156 | 7069.18 | 6580.18 | 527.00 | 84.73 | -90 | 0 | NO | Getty Mines |
| GGR157 | 6942.75 | 6576.04 | 538.07 | 56.70 | -90 | 0 | YES | Getty Mines |
| GGR158 | 6816.85 | 6575.43 | 546.07 | 45.11 | -90 | 0 | YES | Getty Mines |
| GGR159 | 6703.38 | 6576.94 | 556.78 | 40.84 | -90 | 0 | NO | Getty Mines |
| GGR160 | 7438.26 | 6551.44 | 519.00 | 143.30 | -90 | 0 | NO | Getty Mines |
| GGR161 | 6072.52 | 6571.03 | 527.00 | 106.10 | -90 | 0 | NO | Getty Mines |
| GGR162 | 6072.00 | 6624.00 | 527.00 | 111.30 | -90 | 0 | NO | Getty Mines |
| GGR163 | 6163.00 | 6572.00 | 530.00 | 83.10 | -90 | 0 | NO | Getty Mines |
| GGR164 | 6123.56 | 6693.72 | 530.00 | 35.81 | -90 | 0 | NO | Getty Mines |

ACADIAN MINING CORP.

Table A-1: Getty Resource Estimate - December 2007

Listing of Getty Project Drill Holes With Coordinates and Survey Data

| | Local Grid | Local Grid | Local Grid | | | | Included in December | |
|---------|-------------|--------------|---------------|-----------|-----|---------|-----------------------|-------------|
| Hole Id | Easting (m) | Northing (m) | Elevation (m) | Depth (m) | Dip | Azimuth | 2007 Resource Outline | Drilled By |
| GGR165 | 6156.06 | 6783.26 | 532.56 | 31.40 | -90 | 0 | NO | Getty Mines |
| GGR166 | 6152.40 | 6820.75 | 536.88 | 39.93 | -90 | 0 | YES | Getty Mines |
| GGR167 | 6152.32 | 6850.95 | 539.70 | 43.90 | -90 | 0 | YES | Getty Mines |
| GGR168 | 6154.95 | 6905.77 | 536.57 | 58.52 | -90 | 0 | NO | Getty Mines |
| GGR169 | 6221.54 | 6575.10 | 536.00 | 71.32 | -90 | 0 | YES | Getty Mines |
| GGR170 | 6190.61 | 6626.03 | 535.00 | 60.40 | -90 | 0 | YES | Getty Mines |
| GGR171 | 6275.49 | 6815.46 | 538.00 | 39.93 | -90 | 0 | NO | Getty Mines |
| GGR172 | 6274.69 | 6845.40 | 537.44 | 55.80 | -90 | 0 | YES | Getty Mines |
| GGR173 | 6275.35 | 6906.94 | 537.02 | 69.80 | -90 | 0 | YES | Getty Mines |
| GGR174 | 6396.93 | 6870.49 | 545.00 | 84.73 | -90 | 0 | NO | Getty Mines |
| GGR176 | 6481.52 | 6883.13 | 555.85 | 102.60 | -90 | 0 | YES | Getty Mines |
| GGR177 | 6483.93 | 6912.73 | 556.44 | 90.83 | -90 | 0 | YES | Getty Mines |
| GGR178 | 6483.19 | 6942.88 | 555.89 | 78.33 | -90 | 0 | YES | Getty Mines |
| GGR179 | 6482.30 | 6971.60 | 554.91 | 86.30 | -90 | 0 | YES | Getty Mines |
| GGR180 | 6480.15 | 7005.28 | 552.81 | 72.54 | -90 | 0 | NO | Getty Mines |
| GGR181 | 6482.35 | 7031.82 | 550.13 | 77.82 | -90 | 0 | YES | Getty Mines |
| GGR182 | 6483.12 | 6847.47 | 554.18 | 80.99 | -90 | 0 | YES | Getty Mines |
| GGR183 | 6537.83 | 6896.69 | 557.70 | 80.50 | -90 | 0 | YES | Getty Mines |
| GGR184 | 6555.95 | 6919.19 | 556.60 | 80.50 | -90 | 0 | NO | Getty Mines |
| GGR190 | 6614.28 | 6731.29 | 555.01 | 48.20 | -90 | 0 | NO | Getty Mines |
| GGR191 | 6656.29 | 6776.18 | 553.42 | 63.40 | -90 | 0 | YES | Getty Mines |
| GGR192 | 6678.02 | 6796.82 | 550.77 | 72.24 | -90 | 0 | YES | Getty Mines |
| GGR193 | 6719.08 | 6841.98 | 548.09 | 78.64 | -90 | 0 | YES | Getty Mines |
| GGR205 | 6706.16 | 6610.49 | 554.92 | 46.94 | -90 | 0 | NO | Getty Mines |
| GGR206 | 6779.26 | 6654.11 | 548.47 | 70.71 | -90 | 0 | YES | Getty Mines |
| GGR208 | 6846.62 | 6719.39 | 545.11 | 109.73 | -90 | 0 | YES | Getty Mines |
| GGR209 | 6868.71 | 6740.56 | 544.05 | 122.22 | -90 | 0 | YES | Getty Mines |
| GGR210 | 6882.05 | 6782.73 | 543.07 | 124.40 | -90 | 0 | NO | Getty Mines |
| GGR211 | 7031.21 | 6634.64 | 533.26 | 61.30 | -90 | 0 | YES | Getty Mines |
| GGR212 | 6898.35 | 6651.37 | 541.45 | 100.60 | -90 | 0 | NO | Getty Mines |
| GGR213 | 6921.08 | 6674.85 | 540.35 | 61.00 | -90 | 0 | YES | Getty Mines |
| GGR214 | 6972.24 | 6727.87 | 536.30 | 74.70 | -90 | 0 | YES | Getty Mines |
| GGR215 | 6998.48 | 6750.40 | 537.70 | 72.24 | -90 | 0 | YES | Getty Mines |

ACADIAN MINING CORP.

Table A-1: Getty Resource Estimate - December 2007

Listing of Getty Project Drill Holes With Coordinates and Survey Data

| | Local Grid | Local Grid | Local Grid | | | | Included in December | |
|--------------|-------------|--------------|---------------|-----------|-----|---------|-----------------------|--------------|
| Hole Id | Easting (m) | Northing (m) | Elevation (m) | Depth (m) | Dip | Azimuth | 2007 Resource Outline | Drilled By |
| GGR216 | 7040.53 | 6787.83 | 517.25 | 65.23 | -90 | 0 | YES | Getty Mines |
| GGR217 | 6395.36 | 6946.57 | 551.48 | 127.41 | -90 | 0 | YES | Getty Mines |
| GGR219 | 6844.98 | 6598.95 | 545.17 | 55.50 | -90 | 0 | YES | Getty Mines |
| GGR220 | 6341.10 | 6567.32 | 552.00 | 77.11 | -90 | 0 | YES | Getty Mines |
| GGR221 | 6262.40 | 6573.02 | 540.00 | 72.54 | -90 | 0 | YES | Getty Mines |
| GGR222 | 6096.97 | 6850.50 | 537.10 | 42.10 | -90 | 0 | YES | Getty Mines |
| GGR223 | 6091.52 | 6784.73 | 531.34 | 44.50 | -90 | 0 | NO | Getty Mines |
| GGR224 | 6737.45 | 6863.75 | 546.37 | 80.80 | -90 | 0 | NO | Getty Mines |
| GGR225 | 6461.57 | 6627.83 | 547.00 | 53.95 | -90 | 0 | NO | Getty Mines |
| GGR226 | 6461.74 | 6574.48 | 562.00 | 70.41 | -90 | 0 | NO | Getty Mines |
| GGR227 | 6403.58 | 6572.10 | 562.00 | 76.20 | -90 | 0 | NO | Getty Mines |
| GGR228 | 6404.57 | 6627.62 | 557.00 | 52.43 | -90 | 0 | NO | Getty Mines |
| GGR229 | 6276.38 | 6784.08 | 538.00 | 30.80 | -90 | 0 | NO | Getty Mines |
| GGR230 | 6157.91 | 6600.75 | 530.00 | 53.04 | -90 | 0 | YES | Getty Mines |
| GGR231 | 6158.85 | 6563.26 | 530.00 | 72.54 | -90 | 0 | YES | Getty Mines |
| S277 | 6997.39 | 6500.29 | 530.42 | 108.81 | -90 | 0 | NO | Imperial Oil |
| S526 | 6941.67 | 6520.86 | 535.42 | 68.58 | -90 | 0 | YES | Imperial Oil |
| S527 | 6881.68 | 6517.20 | 541.85 | 52.73 | -90 | 0 | YES | Imperial Oil |
| S528 | 6818.68 | 6517.20 | 545.96 | 35.66 | -90 | 0 | NO | Imperial Oil |
| - | D 4 | | | | | | | |
| | By Acadian | 0044.04 | 555.04 | 44.00 | 100 | | NO | 0 |
| S1021-07 | 6731.32 | 6614.94 | 555.01 | 41.00 | -90 | 0 | NO | Acadian |
| S1025-07 | 6651.11 | 6897.88 | 541.49 | 62.00 | -90 | 0 | NO | Acadian |
| S1043-07 | 6773.05 | 6958.01 | 536.65 | 68.00 | -90 | 0 | NO | Acadian |
| S1059-08 | 6512.286 | 6997.462 | 553.103 | 71.00 | -90 | 0 | NO | Acadian |
| | | | | | 1 | | | |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR018 | 56.65 | 57.65 | 1 | 0.28 | 3.53 | 3.81 |
| GGR018 | 57.65 | 58.65 | 1 | 0.18 | 4.21 | 4.39 |
| GGR018 | 58.65 | 59.65 | 1 | 2.45 | 7.63 | 10.08 |
| GGR019 | 25 | 26 | 1 | 0.01 | 0.69 | 0.70 |
| GGR019 | 26 | 27 | 1 | 0.02 | 0.76 | 0.78 |
| GGR019 | 27 | 28 | 1 | 0.03 | 0.84 | 0.87 |
| GGR019 | 28 | 29 | 1 | 0.01 | 0.55 | 0.56 |
| GGR019 | 29 | 30 | 1 | 0.01 | 0.50 | 0.51 |
| GGR019 | 30 | 31 | 1 | 0.02 | 0.46 | 0.48 |
| GGR019 | 31 | 32 | 1 | 0.04 | 0.16 | 0.20 |
| GGR019 | 32 | 33 | 1 | 0.03 | 0.13 | 0.16 |
| GGR019 | 33 | 34 | 1 | 0.01 | 0.13 | 0.14 |
| GGR019 | 34 | 35 | 1 | 0.01 | 0.14 | 0.15 |
| GGR019 | 35 | 36 | 1 | 0.02 | 0.12 | 0.14 |
| GGR019 | 36 | 37 | 1 | 0.05 | 0.08 | 0.13 |
| GGR019 | 37 | 38 | 1 | 0.03 | 0.37 | 0.39 |
| GGR019 | 38 | 39 | 1 | 0.02 | 0.52 | 0.54 |
| GGR019 | 39 | 40 | 1 | 0.03 | 0.72 | 0.75 |
| GGR019 | 40 | 41 | 1 | 0.01 | 1.01 | 1.02 |
| GGR019 | 41 | 42 | 1 | 0.01 | 0.97 | 0.98 |
| GGR019 | 42 | 43 | 1 | 0.01 | 0.52 | 0.53 |
| GGR019 | 43 | 44 | 1 | 0.19 | 0.44 | 0.64 |
| GGR019 | 44 | 45 | 1 | 0.24 | 0.41 | 0.64 |
| GGR019 | 45 | 46 | 1 | 0.09 | 0.39 | 0.48 |
| GGR019 | 46 | 47 | 1 | 0.24 | 0.48 | 0.71 |
| GGR019 | 47 | 48 | 1 | 0.30 | 0.64 | 0.93 |
| GGR019 | 48 | 49 | 1 | 0.21 | 1.41 | 1.62 |
| GGR019 | 49 | 50 | 1 | 0.11 | 1.93 | 2.04 |
| GGR019 | 50 | 51 | 1 | 0.08 | 2.42 | 2.50 |
| GGR019 | 51 | 52 | 1 | 0.43 | 3.94 | 4.37 |
| GGR019 | 52 | 53 | 1 | 0.69 | 4.99 | 5.68 |
| GGR019 | 53 | 54 | 1 | 0.98 | 5.84 | 6.82 |
| GGR019 | 54 | 55 | 1 | 3.06 | 6.37 | 9.43 |
| GGR019 | 55 | 56 | 1 | 1.70 | 4.87 | 6.57 |
| GGR019 | 56 | 57 | 1 | 0.40 | 3.42 | 3.82 |
| GGR019 | 57 | 58 | 1 | 0.09 | 1.03 | 1.13 |
| GGR019 | 58 | 59 | 1 | 0.09 | 1.01 | 1.10 |
| GGR021 | 27.44 | 28.44 | 1 | 0.01 | 0.76 | 0.77 |
| GGR021 | 28.44 | 29.44 | 1 | 0.01 | 1.04 | 1.05 |
| GGR021 | 29.44 | 30.44 | 1 | 0.01 | 1.35 | 1.36 |
| GGR021 | 30.44 | 31.44 | 1 | 0.01 | 1.33 | 1.34 |
| GGR021 | 31.44 | 32.44 | 1 | 0.01 | 1.54 | 1.55 |
| GGR021 | 32.44 | 33.44 | 1 | 0.01 | 1.81 | 1.82 |
| GGR021 | 33.44 | 34.44 | 1 | 0.04 | 0.83 | 0.87 |
| GGR021 | 34.44 | 35.44 | 1 | 0.07 | 0.83 | 0.90 |
| GGR021 | 35.44 | 36.44 | 1 | 0.13 | 1.01 | 1.14 |
| GGR021 | 36.44 | 37.44 | 1 | 0.21 | 1.46 | 1.67 |
| GGR021 | 37.44 | 38.44 | 1 | 0.15 | 1.76 | 1.92 |
| GGR021 | 38.44 | 39.44 | 1 | 0.02 | 2.22 | 2.24 |
| GGR021 | 39.44 | 40.44 | 1 | 0.30 | 1.50 | 1.80 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|-------|------|-------------|
| GGR021 | 40.44 | 41.44 | 1 | 0.32 | 1.03 | 1.36 |
| GGR021 | 41.44 | 42.44 | 1 | 0.20 | 0.27 | 0.47 |
| GGR021 | 42.44 | 43.44 | 1 | 0.26 | 0.38 | 0.64 |
| GGR021 | 43.44 | 44.44 | 1 | 0.47 | 0.51 | 0.97 |
| GGR021 | 44.44 | 45.44 | 1 | 0.91 | 0.67 | 1.59 |
| GGR021 | 45.44 | 46.44 | 1 | 0.06 | 0.06 | 0.12 |
| GGR021 | 46.44 | 47.44 | 1 | 0.03 | 0.02 | 0.05 |
| GGR021 | 47.44 | 48.44 | 1 | 1.32 | 1.22 | 2.55 |
| GGR021 | 48.44 | 49.44 | 1 | 1.14 | 1.51 | 2.65 |
| GGR021 | 49.44 | 50.44 | 1 | 0.46 | 1.74 | 2.20 |
| GGR022 | 43.29 | 44.29 | 1 | 0.08 | 0.57 | 0.65 |
| GGR022 | 44.29 | 45.29 | 1 | 0.13 | 0.69 | 0.81 |
| GGR022 | 45.29 | 46.29 | 1 | 0.18 | 0.82 | 1.00 |
| GGR022 | 46.29 | 47.29 | 1 | 1.02 | 1.77 | 2.79 |
| GGR022 | 47.29 | 48.29 | 1 | 0.74 | 1.62 | 2.36 |
| GGR022 | 48.29 | 49.29 | 1 | 0.29 | 1.35 | 1.64 |
| GGR022 | 49.29 | 50.29 | 1 | 0.42 | 1.94 | 2.36 |
| GGR022 | 50.29 | 51.29 | 1 | 0.44 | 2.04 | 2.49 |
| GGR022 | 51.29 | 52.29 | 1 | 0.46 | 2.10 | 2.56 |
| GGR022 | 52.29 | 53.29 | 1 | 0.30 | 1.44 | 1.74 |
| GGR022 | 53.29 | 54.29 | 1 | 0.21 | 1.28 | 1.49 |
| GGR022 | 54.29 | 55.29 | 1 | 0.10 | 1.19 | 1.29 |
| GGR022 | 55.29 | 56.29 | 1 | 0.04 | 0.72 | 0.75 |
| GGR022 | 56.29 | 57.29 | 1 | 0.02 | 0.89 | 0.91 |
| GGR022 | 57.29 | 58.29 | 1 | 0.02 | 1.64 | 1.65 |
| GGR022 | 58.29 | 59.29 | 1 | 0.01 | 0.81 | 0.82 |
| GGR022 | 59.29 | 60.29 | 1 | 0.01 | 0.53 | 0.54 |
| GGR022 | 60.29 | 61.29 | 1 | 0.01 | 0.54 | 0.55 |
| GGR024 | 70.12 | 71.12 | 1 | 6.41 | 3.76 | 10.17 |
| GGR024 | 71.12 | 72.12 | 1 | 4.41 | 2.58 | 7.00 |
| GGR025A | 121.21 | 122.21 | 1 | 1.68 | 0.01 | 1.69 |
| GGR025A | 122.21 | 123.21 | 1 | 4.68 | 0.01 | 4.78 |
| GGR025A | 123.21 | 124.21 | 1 | 6.49 | 0.29 | 6.78 |
| GGR025A | 124.21 | 125.21 | 1 | 6.51 | 0.23 | 6.64 |
| GGR025A | 125.21 | 126.21 | 1 | 6.48 | 0.13 | 6.62 |
| GGR025A | 126.21 | 127.21 | 1 | 8.18 | 0.15 | 8.33 |
| GGR025A | 127.21 | 128.21 | 1 | 10.98 | 0.13 | 10.99 |
| GGR025A | 128.21 | 129.21 | 1 | 4.64 | 0.01 | 4.65 |
| GGR025A | 129.21 | 130.21 | 1 | 1.52 | 0.01 | 1.53 |
| GGR026 | 71.34 | 72.34 | 1 | 3.16 | 1.55 | 4.71 |
| GGR026 | 72.34 | 73.34 | 1 | 2.28 | 1.20 | 3.48 |
| GGR026 | 73.34 | 74.34 | 1 | 4.79 | 3.02 | 7.81 |
| GGR026 | 74.34 | 75.34 | 1 | 3.38 | 3.74 | 7.12 |
| GGR026 | 75.34 | 76.34 | 1 | 2.16 | 2.84 | 5.00 |
| GGR026 | 76.34 | 77.34 | 1 | 0.33 | 1.67 | 2.00 |
| GGR026 | 77.34 | 78.34 | 1 | 0.09 | 0.58 | 0.67 |
| GGR026 | 78.34 | 79.34 | | 0.09 | 1.10 | 1.20 |
| | | | 1 | | | |
| GGR026 | 79.34 | 80.34 | 1 | 0.17 | 2.14 | 2.31 |
| GGR026 | 80.34 | 81.34 | 1 | 0.17 | 1.75 | 1.92 |
| GGR026 | 81.34 | 82.34 | 1 | 0.17 | 0.52 | 0.69 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR027 | 31.1 | 32.1 | 1 | 0.01 | 0.57 | 0.58 |
| GGR027 | 32.1 | 33.1 | 1 | 0.03 | 0.52 | 0.56 |
| GGR027 | 33.1 | 34.1 | 1 | 0.06 | 0.47 | 0.53 |
| GGR027 | 34.1 | 35.1 | 1 | 0.31 | 0.86 | 1.17 |
| GGR027 | 35.1 | 36.1 | 1 | 0.27 | 0.72 | 0.99 |
| GGR027 | 36.1 | 37.1 | 1 | 0.20 | 0.51 | 0.71 |
| GGR027 | 37.1 | 38.1 | 1 | 0.61 | 0.83 | 1.45 |
| GGR027 | 38.1 | 39.1 | 1 | 0.61 | 0.89 | 1.51 |
| GGR027 | 39.1 | 40.1 | 1 | 0.39 | 0.82 | 1.21 |
| GGR027 | 40.1 | 41.1 | 1 | 0.23 | 0.77 | 1.00 |
| GGR027 | 41.1 | 42.1 | 1 | 3.71 | 1.82 | 5.53 |
| GGR027 | 42.1 | 43.1 | 1 | 4.19 | 1.56 | 5.75 |
| GGR027 | 43.1 | 44.1 | 1 | 1.48 | 0.80 | 2.28 |
| GGR027 | 44.1 | 45.1 | 1 | 0.67 | 0.77 | 1.44 |
| GGR027 | 45.1 | 46.1 | 1 | 0.25 | 0.49 | 0.75 |
| GGR027 | 46.1 | 47.1 | 1 | 0.05 | 0.31 | 0.35 |
| GGR027 | 47.1 | 48.1 | 1 | 0.13 | 0.08 | 0.21 |
| GGR032 | 91.8 | 92.8 | 1 | 0.26 | 0.60 | 0.87 |
| GGR032 | 92.8 | 93.8 | 1 | 0.95 | 0.10 | 1.05 |
| GGR032 | 93.8 | 94.8 | 1 | 2.38 | 0.02 | 2.40 |
| GGR035A | 87.5 | 88.5 | 1 | 0.21 | 1.54 | 1.75 |
| GGR035A | 88.5 | 89.5 | 1 | 0.12 | 1.42 | 1.53 |
| GGR035A | 89.5 | 90.5 | 1 | 0.02 | 0.70 | 0.72 |
| GGR036 | 39.94 | 40.94 | 1 | 1.27 | 0.65 | 1.92 |
| GGR036 | 40.94 | 41.94 | 1 | 0.54 | 0.25 | 0.80 |
| GGR036 | 41.94 | 42.94 | 1 | 1.26 | 0.53 | 1.79 |
| GGR036 | 42.94 | 43.94 | 1 | 2.61 | 1.04 | 3.65 |
| GGR036 | 43.94 | 44.94 | 1 | 0.63 | 0.75 | 1.38 |
| GGR036 | 44.94 | 45.94 | 1 | 0.51 | 0.49 | 0.99 |
| GGR036 | 45.94 | 46.94 | 1 | 0.41 | 0.27 | 0.67 |
| GGR036 | 46.94 | 47.94 | 1 | 0.71 | 0.59 | 1.30 |
| GGR036 | 47.94 | 48.94 | 1 | 0.53 | 0.44 | 0.97 |
| GGR036 | 48.94 | 49.94 | 1 | 0.32 | 0.27 | 0.59 |
| GGR037 | 39.94 | 40.94 | 1 | 0.73 | 2.35 | 3.08 |
| GGR037 | 40.94 | 41.94 | 1 | 2.15 | 2.41 | 4.56 |
| GGR037 | 41.94 | 42.94 | 1 | 7.28 | 2.00 | 9.27 |
| GGR037 | 42.94 | 43.94 | 1 | 3.83 | 1.37 | 5.20 |
| GGR037 | 43.94 | 44.94 | 1 | 2.64 | 3.21 | 5.85 |
| GGR037 | 44.94 | 45.94 | 1 | 2.39 | 2.72 | 5.11 |
| GGR037 | 45.94 | 46.94 | 1 | 1.83 | 2.72 | 4.15 |
| GGR037 | 46.94 | 47.94 | 1 | 4.89 | 2.84 | 7.73 |
| GGR037 | 47.94 | 48.94 | 1 | 1.43 | 1.58 | 3.01 |
| GGR037 | 48.94 | 49.94 | 1 | 0.71 | 0.87 | 1.58 |
| GGR037 | 49.94 | 50.94 | 1 | 0.71 | 0.70 | 1.22 |
| GGR037 | 50.94 | 51.94 | 1 | 0.48 | 0.76 | 1.14 |
| GGR037 | 51.94 | 52.94 | 1 | 0.46 | 1.05 | 1.44 |
| | | | | | | |
| GGR037 | 52.94 | 53.94 | 1 | 2.38 | 1.35 | 3.74 |
| GGR037 | 53.94 | 54.94 | 1 | 3.61 | 1.45 | 5.07 |
| GGR037 | 54.94 | 55.94 | 1 | 0.82 | 0.88 | 1.70 |
| GGR037 | 55.94 | 56.94 | 1 | 1.08 | 1.06 | 2.14 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---|---|---|-----------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| GGR037 | 56.94 | 57.94 | 1 | 0.98 | 1.03 | 2.01 |
| GGR037 | 57.94 | 58.94 | 1 | 0.37 | 0.75 | 1.12 |
| GGR037 | 58.94 | 59.94 | 1 | 0.41 | 0.58 | 0.98 |
| GGR037 | 59.94 | 60.94 | 1 | 0.42 | 0.50 | 0.92 |
| GGR038 | 46.65 | 47.65 | 1 | 0.03 | 0.66 | 0.69 |
| GGR038 | 47.65 | 48.65 | 1 | 0.03 | 0.66 | 0.69 |
| GGR038 | 48.65 | 49.65 | 1 | 0.05 | 0.67 | 0.72 |
| GGR038 | 49.65 | 50.65 | 1 | 0.29 | 0.74 | 1.03 |
| GGR038 | 50.65 | 51.65 | 1 | 0.08 | 0.71 | 0.78 |
| GGR038 | 51.65 | 52.65 | 1 | 0.06 | 0.64 | 0.70 |
| GGR038 | 52.65 | 53.65 | 1 | 0.09 | 0.53 | 0.62 |
| GGR038 | 53.65 | 54.65 | 1 | 0.22 | 0.38 | 0.60 |
| GGR038 | 54.65 | 55.65 | 1 | 0.07 | 0.15 | 0.22 |
| GGR038 | 55.65 | 56.65 | 1 | 0.12 | 0.59 | 0.70 |
| GGR038 | 56.65 | 57.65 | 1 | 0.40 | 2.07 | 2.47 |
| GGR038 | 57.65 | 58.65 | 1 | 0.21 | 1.34 | 1.55 |
| GGR038 | 58.65 | 59.65 | 1 | 0.12 | 0.86 | 0.98 |
| GGR038 | 59.65 | 60.65 | 1 | 0.04 | 0.08 | 0.12 |
| GGR038 | 60.65 | 61.65 | 1 | 0.20 | 0.84 | 1.04 |
| GGR038 | 61.65 | 62.65 | 1 | 0.25 | 1.18 | 1.43 |
| GGR038 | 62.65 | 63.65 | 1 | 0.21 | 1.14 | 1.35 |
| GGR038 | 63.65 | 64.65 | 1 | 0.07 | 0.32 | 0.39 |
| GGR038 | 64.65 | 65.65 | 1 | 0.19 | 1.10 | 1.29 |
| GGR038 | 65.65 | 66.65 | 1 | 1.44 | 2.73 | 4.17 |
| GGR038 | 66.65 | 67.65 | 1 | 4.62 | 4.00 | 8.62 |
| GGR038 | 67.65 | 68.65 | 1 | 1.79 | 1.91 | 3.70 |
| GGR038 | 68.65 | 69.65 | 1 | 0.28 | 0.69 | 0.97 |
| GGR038 | 69.65 | 70.65 | 1 | 0.10 | 0.23 | 0.33 |
| GGR038 | 70.65 | 71.65 | 1 | 0.11 | 0.25 | 0.36 |
| GGR038 | 71.65 | 72.65 | 1 | 0.12 | 0.34 | 0.46 |
| GGR038 | 72.65 | 73.65 | 1 | 0.15 | 0.72 | 0.87 |
| GGR038 | 73.65 | 74.65 | 1 | 0.06 | 0.39 | 0.45 |
| GGR038 | 74.65 | 75.65 | 1 | 0.03 | 0.35 | 0.38 |
| GGR038 | 75.65 | 76.65 | 1 | 0.03 | 0.51 | 0.54 |
| GGR038 | 76.65 | 77.65 | 1 | 0.03 | 0.81 | 0.84 |
| GGR038 | 77.65 | 78.65 | 1 | 0.02 | 0.83 | 0.85 |
| GGR038 | 78.65 | 79.65 | 1 | 0.01 | 0.71 | 0.72 |
| GGR038 | 79.65 | 80.65 | 1 | 0.01 | 0.61 | 0.62 |
| GGR038 | 80.65 | 81.65 | 1 | 0.01 | 0.60 | 0.61 |
| GGR038 | 81.65 | 82.65 | 1 | 0.01 | 0.00 | 0.02 |
| GGR038 | 82.65 | 83.65 | 1 | 0.01 | 0.39 | 0.66 |
| GGR039A | 58.54 | 59.54 | 1 | 5.82 | 2.28 | 8.10 |
| GGR039A | 59.54 | 60.54 | 1 | 4.21 | 1.99 | 6.20 |
| GGR039A | 60.54 | 61.54 | 1 | 1.72 | 1.42 | 3.14 |
| GGR039A | 61.54 | 62.54 | 1 | 1.36 | 1.43 | 2.79 |
| | | 63.54 | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| GGR039A GGR039A GGR039A GGR039A GGR039A | 62.54 63.54 64.54 65.54 66.54 | 63.54 64.54 65.54 66.54 67.54 | 1 1 1 1 1 | 0.76 1.25 1.74 1.99 1.21 | 1.06 0.63 1.99 2.69 0.41 | 1.82 1.88 3.72 4.68 1.62 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR039A | 67.54 | 68.54 | 1 | 0.91 | 0.89 | 1.80 |
| GGR039A | 68.54 | 69.54 | 1 | 0.66 | 1.28 | 1.94 |
| GGR039A | 69.54 | 70.54 | 1 | 0.44 | 1.17 | 1.61 |
| GGR039A | 70.54 | 71.54 | 1 | 0.39 | 1.29 | 1.68 |
| GGR039A | 71.54 | 72.54 | 1 | 0.34 | 1.41 | 1.75 |
| GGR039A | 72.54 | 73.54 | 1 | 0.73 | 0.39 | 1.12 |
| GGR039A | 73.54 | 74.54 | 1 | 0.57 | 0.62 | 1.19 |
| GGR039A | 74.54 | 75.54 | 1 | 1.27 | 0.40 | 1.67 |
| GGR039A | 75.54 | 76.54 | 1 | 0.36 | 0.21 | 0.57 |
| GGR039A | 76.54 | 77.54 | 1 | 0.79 | 0.41 | 1.20 |
| GGR039A | 77.54 | 78.54 | 1 | 2.03 | 1.19 | 3.22 |
| GGR039A | 78.54 | 79.54 | 1 | 2.15 | 0.51 | 2.67 |
| GGR039A | 79.54 | 80.54 | 1 | 1.70 | 0.31 | 2.01 |
| GGR039A | 80.54 | 81.54 | 1 | 0.87 | 0.12 | 0.99 |
| GGR039A | 81.54 | 82.54 | 1 | 0.40 | 0.10 | 0.50 |
| GGR039A | 82.54 | 83.54 | 1 | 0.28 | 0.09 | 0.36 |
| GGR039A | 83.54 | 84.54 | 1 | 0.22 | 0.06 | 0.28 |
| GGR039A | 84.54 | 85.54 | 1 | 0.46 | 0.45 | 0.91 |
| GGR039A | 85.54 | 86.54 | 1 | 0.64 | 0.55 | 1.20 |
| GGR039A | 86.54 | 87.54 | 1 | 0.96 | 0.54 | 1.50 |
| GGR039A | 87.54 | 88.54 | 1 | 1.50 | 0.95 | 2.45 |
| GGR039A | 88.54 | 89.54 | 1 | 1.60 | 1.11 | 2.71 |
| GGR039A | 89.54 | 90.54 | 1 | 1.25 | 1.20 | 2.45 |
| GGR039A | 90.54 | 91.54 | 1 | 1.51 | 1.24 | 2.75 |
| GGR039A | 91.54 | 92.54 | 1 | 1.88 | 1.52 | 3.40 |
| GGR039A | 92.54 | 93.54 | 1 | 3.19 | 2.88 | 6.07 |
| GGR039A | 93.54 | 94.54 | 1 | 2.45 | 1.94 | 4.39 |
| GGR039A | 94.54 | 95.54 | 1 | 1.90 | 0.45 | 2.35 |
| GGR039A | 95.54 | 96.54 | 1 | 1.03 | 0.31 | 1.34 |
| GGR039A | 96.54 | 97.54 | 1 | 0.43 | 0.22 | 0.65 |
| GGR039A | 97.54 | 98.54 | 1 | 1.79 | 0.02 | 1.81 |
| GGR040 | 71.55 | 72.55 | 1 | 0.99 | 0.50 | 1.49 |
| GGR040 | 72.55 | 73.55 | 1 | 0.85 | 0.33 | 1.18 |
| GGR040 | 73.55 | 74.55 | 1 | 1.18 | 0.53 | 1.71 |
| GGR040 | 74.55 | 75.55 | 1 | 0.82 | 0.69 | 1.51 |
| GGR040 | 75.55 | 76.55 | 1 | 0.08 | 0.75 | 0.83 |
| GGR040 | 76.55 | 77.55 | 1 | 0.06 | 0.70 | 0.76 |
| GGR040 | 77.55 | 78.55 | 1 | 0.32 | 0.56 | 0.88 |
| GGR040 | 78.55 | 79.55 | 1 | 0.57 | 0.44 | 1.01 |
| GGR079 | 27.37 | 28.37 | 1 | 1.19 | 0.04 | 1.23 |
| GGR079 | 28.37 | 29.37 | 1 | 0.37 | 0.63 | 1.01 |
| GGR079 | 29.37 | 30.37 | 1 | 0.20 | 0.44 | 0.64 |
| GGR079 | 30.37 | 31.37 | 1 | 1.26 | 0.93 | 2.19 |
| GGR079 | 31.37 | 32.37 | 1 | 2.09 | 1.51 | 3.60 |
| GGR079 | 32.37 | 33.37 | 1 | 1.32 | 1.03 | 2.35 |
| GGR081 | 28.32 | 29.32 | 1 | 2.42 | 0.07 | 2.49 |
| GGR081 | 29.32 | 30.32 | 1 | 0.91 | 0.07 | 1.08 |
| GGR081 | 30.32 | 31.32 | 1 | 1.76 | 0.17 | 2.18 |
| GGR081 | 31.32 | 32.32 | 1 | 1.93 | 0.42 | 2.45 |
| GGR081 | 32.32 | 33.32 | 1 | 2.21 | 0.90 | 3.11 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|-------|------|-------------|
| GGR081 | 33.32 | 34.32 | 1 | 1.25 | 0.62 | 1.87 |
| GGR081 | 34.32 | 35.32 | 1 | 0.94 | 0.57 | 1.51 |
| GGR081 | 35.32 | 36.32 | 1 | 0.77 | 0.66 | 1.43 |
| GGR081 | 36.32 | 37.32 | 1 | 0.53 | 0.73 | 1.27 |
| GGR081 | 37.32 | 38.32 | 1 | 0.37 | 0.62 | 0.99 |
| GGR081 | 38.32 | 39.32 | 1 | 0.08 | 0.12 | 0.20 |
| GGR081 | 39.32 | 40.32 | 1 | 0.29 | 0.18 | 0.47 |
| GGR081 | 40.32 | 41.32 | 1 | 0.38 | 0.21 | 0.59 |
| GGR093 | 35.39 | 36.39 | 1 | 0.10 | 0.50 | 0.60 |
| GGR093 | 36.39 | 37.39 | 1 | 0.16 | 0.70 | 0.86 |
| GGR093 | 37.39 | 38.39 | 1 | 0.18 | 0.74 | 0.92 |
| GGR093 | 38.39 | 39.39 | 1 | 0.23 | 0.70 | 0.93 |
| GGR093 | 39.39 | 40.39 | 1 | 0.21 | 0.73 | 0.94 |
| GGR093 | 40.39 | 41.39 | 1 | 0.17 | 1.22 | 1.39 |
| GGR093 | 41.39 | 42.39 | 1 | 0.46 | 3.90 | 4.36 |
| GGR093 | 42.39 | 43.39 | 1 | 1.23 | 1.93 | 3.16 |
| GGR094 | 26.82 | 27.82 | 1 | 0.03 | 0.83 | 0.86 |
| GGR094 | 27.82 | 28.82 | 1 | 0.11 | 0.83 | 0.94 |
| GGR094 | 28.82 | 29.82 | 1 | 0.20 | 0.83 | 1.03 |
| GGR094 | 29.82 | 30.82 | 1 | 0.13 | 1.03 | 1.16 |
| GGR094 | 30.82 | 31.82 | 1 | 0.09 | 0.87 | 0.96 |
| GGR094 | 31.82 | 32.82 | 1 | 0.04 | 0.65 | 0.69 |
| GGR094 | 32.82 | 33.82 | 1 | 0.01 | 0.68 | 0.69 |
| GGR094 | 33.82 | 34.82 | 1 | 0.01 | 0.39 | 0.40 |
| GGR094 | 34.82 | 35.82 | 1 | 0.13 | 2.09 | 2.21 |
| GGR094 | 35.82 | 36.82 | 1 | 0.19 | 3.09 | 3.28 |
| GGR094 | 36.82 | 37.82 | 1 | 0.08 | 1.18 | 1.26 |
| GGR094 | 37.82 | 38.82 | 1 | 0.06 | 0.76 | 0.82 |
| GGR096 | 18.11 | 19.11 | 1 | 0.53 | 2.32 | 2.85 |
| GGR096 | 19.11 | 20.11 | 1 | 0.23 | 1.08 | 1.31 |
| GGR096 | 20.11 | 21.11 | 1 | 0.21 | 1.06 | 1.26 |
| GGR096 | 21.11 | 22.11 | 1 | 0.11 | 2.58 | 2.69 |
| GGR096 | 22.11 | 23.11 | 1 | 0.02 | 0.48 | 0.50 |
| GGR096 | 23.11 | 24.11 | 1 | 0.07 | 0.40 | 0.47 |
| GGR096 | 24.11 | 25.11 | 1 | 0.09 | 0.36 | 0.45 |
| GGR096 | 25.11 | 26.11 | 1 | 0.04 | 0.76 | 0.80 |
| GGR096 | 26.11 | 27.11 | 1 | 0.07 | 0.73 | 0.80 |
| GGR096 | 27.11 | 28.11 | 1 | 0.14 | 0.57 | 0.71 |
| GGR096 | 28.11 | 29.11 | 1 | 0.14 | 0.75 | 0.89 |
| GGR096 | 29.11 | 30.11 | 1 | 0.15 | 0.76 | 0.91 |
| GGR096 | 30.11 | 31.11 | 1 | 0.55 | 1.05 | 1.60 |
| GGR096 | 31.11 | 32.11 | 1 | 0.72 | 1.49 | 2.21 |
| GGR096 | 32.11 | 33.11 | 1 | 1.45 | 1.55 | 2.99 |
| GGR096 | 33.11 | 34.11 | 1 | 2.59 | 2.37 | 4.96 |
| GGR096 | 34.11 | 35.11 | 1 | 2.16 | 2.46 | 4.62 |
| GGR096 | 35.11 | 36.11 | 1 | 6.21 | 4.31 | 10.51 |
| GGR096 | 36.11 | 37.11 | 1 | 6.72 | 4.55 | 11.26 |
| GGR096 | 37.11 | 38.11 | 1 | 3.66 | 3.10 | 6.76 |
| GGR096 | 38.11 | 39.11 | 1 | 4.14 | 1.31 | 5.45 |
| | 100.11 | 100.11 | | 17.17 | 1.01 | IUITU |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR096 | 40.11 | 41.11 | 1 | 2.40 | 0.92 | 3.32 |
| GGR096 | 41.11 | 42.11 | 1 | 0.27 | 0.28 | 0.55 |
| GGR096 | 42.11 | 43.11 | 1 | 0.35 | 0.21 | 0.56 |
| GGR096 | 43.11 | 44.11 | 1 | 0.50 | 0.15 | 0.65 |
| GGR096 | 44.11 | 45.11 | 1 | 1.00 | 0.28 | 1.28 |
| GGR096 | 45.11 | 46.11 | 1 | 1.05 | 0.29 | 1.34 |
| GGR102 | 94.31 | 95.31 | 1 | 0.02 | 0.03 | 0.05 |
| GGR102 | 95.31 | 96.31 | 1 | 0.02 | 0.03 | 0.05 |
| GGR102 | 97.31 | 98.31 | 1 | 0.09 | 0.03 | 0.13 |
| GGR102 | 98.31 | 99.31 | 1 | 3.28 | 3.96 | 7.24 |
| GGR103 | 78.03 | 79.03 | 1 | 2.46 | 1.91 | 4.37 |
| GGR103 | 79.03 | 80.03 | 1 | 0.60 | 0.73 | 1.33 |
| GGR103 | 80.03 | 81.03 | 1 | 0.07 | 0.02 | 0.09 |
| GGR103 | 81.03 | 82.03 | 1 | 0.02 | 0.34 | 0.36 |
| GGR103 | 82.03 | 83.03 | 1 | 0.01 | 0.42 | 0.43 |
| GGR113A | 71.69 | 72.69 | 1 | 0.11 | 0.67 | 0.78 |
| GGR113A | 72.69 | 73.69 | 1 | 0.06 | 0.45 | 0.52 |
| GGR113A | 73.69 | 74.69 | 1 | 0.01 | 0.22 | 0.23 |
| GGR113A | 74.69 | 75.69 | 1 | 0.03 | 0.70 | 0.73 |
| GGR113A | 75.69 | 76.69 | 1 | 0.37 | 0.58 | 0.96 |
| GGR113A | 76.69 | 77.69 | 1 | 0.81 | 0.40 | 1.21 |
| GGR113A | 77.69 | 78.69 | 1 | 0.63 | 0.51 | 1.14 |
| GGR113A | 78.69 | 79.69 | 1 | 1.34 | 1.28 | 2.62 |
| GGR113A | 79.69 | 80.69 | 1 | 2.37 | 2.17 | 4.54 |
| GGR113A | 80.69 | 81.69 | 1 | 0.60 | 0.94 | 1.54 |
| GGR116 | 65.53 | 66.53 | 1 | 1.43 | 0.52 | 1.95 |
| GGR116 | 66.53 | 67.53 | 1 | 2.92 | 1.20 | 4.12 |
| GGR116 | 67.53 | 68.53 | 1 | 3.49 | 1.98 | 5.47 |
| GGR116 | 68.53 | 69.53 | 1 | 0.15 | 0.33 | 0.48 |
| GGR116 | 69.53 | 70.53 | 1 | 0.20 | 0.33 | 0.53 |
| GGR116 | 70.53 | 71.53 | 1 | 0.37 | 0.37 | 0.74 |
| GGR116 | 71.53 | 72.53 | 1 | 0.13 | 0.48 | 0.61 |
| GGR116 | 72.53 | 73.53 | 1 | 0.12 | 0.35 | 0.46 |
| GGR116 | 73.53 | 74.53 | 1 | 0.14 | 0.11 | 0.25 |
| GGR116 | 74.53 | 75.53 | 1 | 0.35 | 0.39 | 0.74 |
| GGR116 | 75.53 | 76.53 | 1 | 0.56 | 0.69 | 1.25 |
| GGR116 | 76.53 | 77.53 | 1 | 2.00 | 0.89 | 2.89 |
| GGR116 | 77.53 | 78.53 | 1 | 1.52 | 0.63 | 2.15 |
| GGR116 | 78.53 | 79.53 | 1 | 0.84 | 0.29 | 1.13 |
| GGR116 | 79.53 | 80.53 | 1 | 0.15 | 0.17 | 0.33 |
| GGR116 | 80.53 | 81.53 | 1 | 0.19 | 0.24 | 0.44 |
| GGR124 | 122.71 | 123.71 | 1 | 3.94 | 0.01 | 3.95 |
| GGR124 | 123.71 | 124.71 | 1 | 4.09 | 0.02 | 4.11 |
| GGR124 | 124.71 | 125.71 | 1 | 0.55 | 0.01 | 0.56 |
| GGR125 | 44.2 | 45.2 | 1 | 0.41 | 1.60 | 2.01 |
| GGR125 | 45.2 | 46.2 | 1 | 0.27 | 1.44 | 1.71 |
| GGR125 | 46.2 | 47.2 | 1 | 0.38 | 1.13 | 1.51 |
| GGR125 | 47.2 | 48.2 | 1 | 0.37 | 0.47 | 0.83 |
| GGR125 | 48.2 | 49.2 | 1 | 0.34 | 1.68 | 2.02 |
| GGR125 | 49.2 | 50.2 | 1 | 0.33 | 3.37 | 3.70 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR125 | 50.2 | 51.2 | 1 | 0.47 | 2.67 | 3.14 |
| GGR125 | 51.2 | 52.2 | 1 | 0.12 | 2.58 | 2.71 |
| GGR125 | 52.2 | 53.2 | 1 | 0.70 | 2.99 | 3.69 |
| GGR125 | 53.2 | 54.2 | 1 | 4.41 | 1.69 | 6.10 |
| GGR125 | 54.2 | 55.2 | 1 | 1.13 | 1.75 | 2.88 |
| GGR125 | 55.2 | 56.2 | 1 | 1.11 | 2.71 | 3.83 |
| GGR125 | 56.2 | 57.2 | 1 | 0.32 | 0.57 | 0.89 |
| GGR125 | 57.2 | 58.2 | 1 | 1.19 | 0.79 | 1.98 |
| GGR125 | 58.2 | 59.2 | 1 | 0.83 | 1.08 | 1.92 |
| GGR125 | 59.2 | 60.2 | 1 | 0.63 | 1.20 | 1.83 |
| GGR125 | 60.2 | 61.2 | 1 | 1.78 | 1.24 | 3.02 |
| GGR125 | 61.2 | 62.2 | 1 | 1.58 | 1.06 | 2.64 |
| GGR125 | 62.2 | 63.2 | 1 | 1.15 | 0.93 | 2.09 |
| GGR125 | 63.2 | 64.2 | 1 | 1.37 | 0.57 | 1.95 |
| GGR126 | 44.1 | 45.1 | 1 | 0.43 | 1.75 | 2.19 |
| GGR126 | 45.1 | 46.1 | 1 | 0.85 | 1.92 | 2.77 |
| GGR126 | 46.1 | 47.1 | 1 | 0.05 | 0.72 | 0.77 |
| GGR126 | 47.1 | 48.1 | 1 | 0.43 | 1.62 | 2.05 |
| GGR126 | 48.1 | 49.1 | 1 | 0.20 | 0.96 | 1.16 |
| GGR126 | 49.1 | 50.1 | 1 | 0.28 | 1.39 | 1.67 |
| GGR126 | 50.1 | 51.1 | 1 | 0.10 | 1.54 | 1.65 |
| GGR126 | 51.1 | 52.1 | 1 | 0.05 | 1.22 | 1.27 |
| GGR126 | 52.1 | 53.1 | 1 | 0.02 | 0.30 | 0.32 |
| GGR126 | 53.1 | 54.1 | 1 | 0.01 | 0.34 | 0.35 |
| GGR126 | 54.1 | 55.1 | 1 | 0.02 | 0.48 | 0.50 |
| GGR126 | 55.1 | 56.1 | 1 | 0.07 | 0.89 | 0.96 |
| GGR126 | 56.1 | 57.1 | 1 | 0.11 | 0.69 | 0.80 |
| GGR126 | 57.1 | 58.1 | 1 | 0.12 | 0.55 | 0.67 |
| GGR126 | 58.1 | 59.1 | 1 | 0.07 | 0.28 | 0.35 |
| GGR126 | 59.1 | 60.1 | 1 | 0.07 | 0.57 | 0.64 |
| GGR126 | 60.1 | 61.1 | 1 | 0.07 | 0.72 | 0.79 |
| GGR129 | 80.07 | 81.07 | 1 | 3.33 | 4.36 | 7.69 |
| GGR129 | 81.07 | 82.07 | 1 | 4.10 | 3.97 | 8.08 |
| GGR129 | 82.07 | 83.07 | 1 | 2.96 | 2.52 | 5.47 |
| GGR129 | 83.07 | 84.07 | 1 | 0.78 | 1.77 | 2.55 |
| GGR129 | 84.07 | 85.07 | 1 | 0.66 | 1.34 | 2.01 |
| GGR129 | 85.07 | 86.07 | 1 | 0.07 | 0.57 | 0.64 |
| GGR129 | 86.07 | 87.07 | 1 | 0.05 | 1.43 | 1.48 |
| GGR129 | 87.07 | 88.07 | 1 | 0.05 | 1.43 | 1.48 |
| GGR130 | 39.62 | 40.62 | 1 | 0.09 | 0.63 | 0.72 |
| GGR130 | 40.62 | 41.62 | 1 | 0.15 | 0.52 | 0.67 |
| GGR130 | 41.62 | 42.62 | 1 | 0.48 | 0.55 | 1.04 |
| GGR130 | 42.62 | 43.62 | 1 | 1.79 | 1.42 | 3.22 |
| GGR130 | 43.62 | 44.62 | 1 | 1.63 | 1.54 | 3.17 |
| GGR130 | 44.62 | 45.62 | 1 | 1.23 | 1.54 | 2.78 |
| GGR130 | 45.62 | 46.62 | 1 | 1.37 | 1.45 | 2.82 |
| GGR130 | 46.62 | 47.62 | 1 | 1.29 | 1.42 | 2.71 |
| GGR130 | 47.62 | 48.62 | 1 | 2.29 | 2.33 | 4.62 |
| GGR130 | 48.62 | 49.62 | 1 | 5.31 | 4.28 | 9.59 |
| GGR130 | 49.62 | 50.62 | 1 | 4.19 | 4.67 | 8.87 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|------------------|-------------|-------------|------------|--------------|--------------|--------------|
| GGR130 | 50.62 | 51.62 | 1 | 1.47 | 3.52 | 4.99 |
| GGR130 | 51.62 | 52.62 | 1 | 1.66 | 1.66 | 3.32 |
| GGR130 | 52.62 | 53.62 | 1 | 0.57 | 0.58 | 1.14 |
| GGR130 | 53.62 | 54.62 | 1 | 0.04 | 0.60 | 0.64 |
| GGR130 | 54.62 | 55.62 | 1 | 0.01 | 0.77 | 0.78 |
| GGR130 | 55.62 | 56.62 | 1 | 0.02 | 0.58 | 0.60 |
| GGR130 | 56.62 | 57.62 | 1 | 0.02 | 0.42 | 0.44 |
| GGR130 | 57.62 | 58.62 | 1 | 0.27 | 0.64 | 0.91 |
| GGR130 | 58.62 | 59.62 | 1 | 0.28 | 0.56 | 0.84 |
| GGR130 | 59.62 | 60.62 | 1 | 0.29 | 0.47 | 0.76 |
| GGR133 | 30.18 | 31.18 | 1 | 0.01 | 0.79 | 0.80 |
| GGR133 | 31.18 | 32.18 | 1 | 0.01 | 0.65 | 0.66 |
| GGR133 | 32.18 | 33.18 | 1 | 0.01 | 0.50 | 0.51 |
| GGR133 | 33.18 | 34.18 | 1 | 0.01 | 0.29 | 0.30 |
| GGR133 | 34.18 | 35.18 | 1 | 0.01 | 1.14 | 1.15 |
| GGR133 | 35.18 | 36.18 | 1 | 0.01 | 2.33 | 2.34 |
| GGR133 | 36.18 | 37.18 | 1 | 0.01 | 2.70 | 2.71 |
| GGR133 | 37.18 | 38.18 | 1 | 0.01 | 3.03 | 3.04 |
| GGR133 | 38.18 | 39.18 | 1 | 0.03 | 3.18 | 3.21 |
| GGR133 | 39.18 | 40.18 | 1 | 0.04 | 1.55 | 1.59 |
| GGR133 | 40.18 | 41.18 | 1 | 0.06 | 1.01 | 1.07 |
| GGR133 | 41.18 | 42.18 | 1 | 0.02 | 1.01 | 1.03 |
| GGR133 | 42.18 | 43.18 | 1 | 0.01 | 1.03 | 1.04 |
| GGR133 | 43.18 | 44.18 | 1 | 0.01 | 1.09 | 1.10 |
| GGR133 | 44.18 | 45.18 | 1 | 0.02 | 0.88 | 0.90 |
| GGR133 | 45.18 | 46.18 | 1 | 0.02 | 0.92 | 0.94 |
| GGR133 | 46.18 | 47.18 | 1 | 0.03 | 1.65 | 1.68 |
| GGR133 | 47.18 | 48.18 | 1 | 0.02 | 0.95 | 0.97 |
| GGR133 | 48.18 | 49.18 | 1 | 0.01 | 0.84 | 0.85 |
| GGR133 | 49.18 | 50.18 | 1 | 0.01 | 1.08 | 1.09 |
| GGR133 | 50.18 | 51.18 | 1 | 0.01 | 1.33 | 1.34 |
| GGR133 | 51.18 | 52.18 | 1 | 0.01 | 1.02 | 1.03 |
| GGR133 | 52.18 | 53.18 | 1 | 0.01 | 0.41 | 0.42 |
| GGR133 | 53.18 | 54.18 | 1 | 0.01 | 0.40 | 0.41 |
| GGR133 | 54.18 | 55.18 | 1 | 0.01 | 0.40 | 0.41 |
| GGR133 | 55.18 | 56.18 | 1 | 0.01 | 0.41 | 0.42 |
| GGR135 | 26 | 27 | 1 | 2.50 | 0.53 | 3.03 |
| GGR135 | 27 | 28 | 1 | 4.20 | 0.99 | 5.19 |
| GGR135 | 28 | 29 | 1 | 1.62 | 0.50 | 2.12 |
| GGR135 | 29 | 30 | 1 | 0.72 | 0.35 | 1.06 |
| GGR135 | 30 | 31 | 1 | 0.72 | 0.32 | 0.78 |
| GGR135 | 31 | 32 | 1 | 0.70 | 0.34 | 1.04 |
| GGR135 | 32 | 33 | 1 | 0.43 | 0.51 | 0.94 |
| GGR135 | 33 | 34 | 1 | 0.43 | 0.51 | 0.94 |
| GGR135 | 34 | 35 | 1 | 0.43 | 0.51 | 0.94 |
| GGR135 | 35 | 36 | 1 | 0.79 | 0.75 | 1.54 |
| GGR135 | 36 | 37 | 1 | 0.60 | 0.75 | 1.26 |
| GGR135 | 37 | 38 | 1 | 0.50 | 0.58 | 1.08 |
| | | | | | | |
| | | | | | | |
| GGR135 GGR136 | 38 22.86 | 39 23.86 | 1 | 2.59 0.51 | 1.29 0.37 | 3.88 0.88 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR136 | 23.86 | 24.86 | 1 | 0.44 | 0.34 | 0.77 |
| GGR136 | 24.86 | 25.86 | 1 | 0.55 | 0.33 | 0.88 |
| GGR136 | 25.86 | 26.86 | 1 | 0.97 | 0.35 | 1.32 |
| GGR136 | 26.86 | 27.86 | 1 | 1.66 | 0.69 | 2.35 |
| GGR136 | 27.86 | 28.86 | 1 | 1.74 | 0.71 | 2.45 |
| GGR136 | 28.86 | 29.86 | 1 | 1.08 | 0.31 | 1.39 |
| GGR157 | 42.06 | 43.06 | 1 | 0.48 | 0.33 | 0.81 |
| GGR157 | 43.06 | 44.06 | 1 | 1.47 | 3.91 | 5.38 |
| GGR157 | 44.06 | 45.06 | 1 | 1.53 | 7.12 | 8.64 |
| GGR157 | 45.06 | 46.06 | 1 | 0.07 | 0.53 | 0.60 |
| GGR157 | 46.06 | 47.06 | 1 | 0.09 | 0.68 | 0.77 |
| GGR157 | 47.06 | 48.06 | 1 | 0.63 | 3.95 | 4.59 |
| GGR157 | 48.06 | 49.06 | 1 | 0.01 | 0.57 | 0.58 |
| GGR157 | 49.06 | 50.06 | 1 | 0.01 | 0.52 | 0.53 |
| GGR158 | 21.52 | 22.52 | 1 | 0.01 | 1.80 | 1.81 |
| GGR158 | 22.52 | 23.52 | 1 | 0.01 | 1.15 | 1.16 |
| GGR158 | 23.52 | 24.52 | 1 | 0.01 | 0.86 | 0.87 |
| GGR158 | 24.52 | 25.52 | 1 | 0.01 | 1.12 | 1.13 |
| GGR158 | 25.52 | 26.52 | 1 | 0.01 | 1.22 | 1.23 |
| GGR158 | 26.52 | 27.52 | 1 | 0.01 | 1.27 | 1.28 |
| GGR158 | 27.52 | 28.52 | 1 | 0.01 | 1.12 | 1.13 |
| GGR158 | 28.52 | 29.52 | 1 | 0.33 | 6.44 | 6.77 |
| GGR158 | 29.52 | 30.52 | 1 | 0.01 | 0.50 | 0.51 |
| GGR158 | 30.52 | 31.52 | 1 | 0.23 | 0.83 | 1.06 |
| GGR158 | 31.52 | 32.52 | 1 | 0.80 | 1.67 | 2.47 |
| GGR158 | 32.52 | 33.52 | 1 | 1.15 | 2.11 | 3.25 |
| GGR158 | 33.52 | 34.52 | 1 | 1.03 | 1.96 | 2.99 |
| GGR158 | 34.52 | 35.52 | 1 | 0.26 | 0.97 | 1.23 |
| GGR158 | 35.52 | 36.52 | 1 | 0.20 | 0.91 | 1.11 |
| GGR158 | 36.52 | 37.52 | 1 | 0.16 | 0.91 | 1.07 |
| GGR158 | 37.52 | 38.52 | 1 | 0.12 | 1.01 | 1.13 |
| GGR166 | 23.1 | 24.1 | 1 | 1.00 | 0.51 | 1.51 |
| GGR166 | 24.1 | 25.1 | 1 | 1.18 | 2.00 | 3.18 |
| GGR166 | 25.1 | 26.1 | 1 | 1.26 | 0.67 | 1.93 |
| GGR166 | 26.1 | 27.1 | 1 | 0.62 | 0.12 | 0.74 |
| GGR166 | 27.1 | 28.1 | 1 | 0.70 | 0.12 | 0.88 |
| GGR166 | 28.1 | 29.1 | 1 | 0.75 | 0.17 | 0.92 |
| GGR166 | 29.1 | 30.1 | 1 | 0.77 | 0.16 | 0.93 |
| GGR167 | 25.45 | 26.45 | 1 | 0.77 | 0.02 | 0.95 |
| GGR167 | 26.45 | 27.45 | 1 | 1.12 | 0.02 | 1.16 |
| GGR167 | 27.45 | 28.45 | 1 | 3.55 | 0.44 | 3.99 |
| GGR167 | 28.45 | 29.45 | 1 | 4.66 | 0.59 | 5.25 |
| GGR167 | 29.45 | 30.45 | 1 | 3.52 | 0.51 | 4.03 |
| GGR167 | 30.45 | 31.45 | 1 | 2.64 | 0.85 | 3.49 |
| GGR167 | 31.45 | 32.45 | 1 | 3.10 | 0.92 | 4.02 |
| GGR167 | 32.45 | 33.45 | 1 | 2.22 | 0.67 | 2.89 |
| GGR167 | 33.45 | 34.45 | 1 | 2.01 | 0.80 | 2.82 |
| GGR167 | 34.45 | 35.45 | 1 | 1.81 | 0.72 | 2.52 |
| GGR167 | 35.45 | 36.45 | 1 | 1.56 | 0.72 | 2.15 |
| GGR167 | 36.45 | 37.45 | 1 | 0.89 | 0.66 | 1.55 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|------------------|----------|--------|------------|-------|------|-------------|
| GGR167 | 37.45 | 38.45 | 1 7 | 0.53 | 0.67 | 1.20 |
| GGR167 | 38.45 | 39.45 | 1 | 0.05 | 0.68 | 0.73 |
| GGR169 | 46.63 | 47.63 | 1 | 10.30 | 0.07 | 10.37 |
| GGR169 | 47.63 | 48.63 | 1 | 6.78 | 0.07 | 6.85 |
| GGR169 | 48.63 | 49.63 | 1 | 2.82 | 0.07 | 2.89 |
| GGR169 | 49.63 | 50.63 | 1 | 2.37 | 0.19 | 2.57 |
| GGR169 | 50.63 | 51.63 | 1 | 2.28 | 0.17 | 2.46 |
| GGR169 | 51.63 | 52.63 | 1 | 2.19 | 0.14 | 2.33 |
| GGR169 | 52.63 | 53.63 | 1 | 2.11 | 0.18 | 2.29 |
| GGR169 | 53.63 | 54.63 | 1 | 2.20 | 0.15 | 2.35 |
| GGR169 | 54.63 | 55.63 | 1 | 2.35 | 0.11 | 2.46 |
| GGR169 | 55.63 | 56.63 | 1 | 5.82 | 1.86 | 7.68 |
| GGR169 | 56.63 | 57.63 | 1 | 6.43 | 2.17 | 8.60 |
| GGR169 | 59.63 | 60.63 | 1 | 0.27 | 1.69 | 1.96 |
| GGR170 | 17.53 | 18.53 | 1 | 0.10 | 0.84 | 0.94 |
| GGR170 | 18.53 | 19.53 | 1 | 0.02 | 0.54 | 0.56 |
| GGR170 | 19.53 | 20.53 | 1 | 0.02 | 0.43 | 0.45 |
| GGR170 | 20.53 | 21.53 | 1 | 0.34 | 0.68 | 1.02 |
| GGR170 | 21.53 | 22.53 | 1 | 0.24 | 0.66 | 0.90 |
| GGR170 | 22.53 | 23.53 | 1 | 0.06 | 0.29 | 0.35 |
| GGR170 | 23.53 | 24.53 | 1 | 0.11 | 0.28 | 0.39 |
| GGR170 | 24.53 | 25.53 | 1 | 0.26 | 0.39 | 0.65 |
| GGR170 | 25.53 | 26.53 | 1 | 0.44 | 0.45 | 0.88 |
| GGR170 | 26.53 | 27.53 | 1 | 0.46 | 0.43 | 0.89 |
| GGR170 | 27.53 | 28.53 | 1 | 0.25 | 0.25 | 0.50 |
| GGR172 | 26.82 | 27.82 | 1 | 0.16 | 0.35 | 0.51 |
| GGR172 | 27.82 | 28.82 | 1 | 1.08 | 0.97 | 2.05 |
| GGR172 | 28.82 | 29.82 | 1 | 1.18 | 1.32 | 2.50 |
| GGR172 | 29.82 | 30.82 | 1 | 2.11 | 1.92 | 4.03 |
| GGR172 | 30.82 | 31.82 | 1 | 1.48 | 1.33 | 2.81 |
| GGR172 | 31.82 | 32.82 | 1 | 5.96 | 1.39 | 7.35 |
| GGR172 | 32.82 | 33.82 | 1 | 2.31 | 2.03 | 4.34 |
| GGR173 | 32.61 | 33.61 | 1 | 0.96 | 0.60 | 1.56 |
| GGR173 | 33.61 | 34.61 | 1 | 0.97 | 0.56 | 1.53 |
| GGR173 | 34.61 | 35.61 | 1 | 0.98 | 0.51 | 1.49 |
| GGR173 | 35.61 | 36.61 | 1 | 1.51 | 1.17 | 2.68 |
| GGR173 | 36.61 | 37.61 | 1 | 1.44 | 1.04 | 2.48 |
| GGR173 | 37.61 | 38.61 | 1 | 1.31 | 0.81 | 2.12 |
| GGR173 | 38.61 | 39.61 | 1 | 0.49 | 0.41 | 0.90 |
| GGR173 | 39.61 | 40.61 | 1 | 0.49 | 0.41 | 0.60 |
| GGR173 | 40.61 | 41.61 | 1 | 0.32 | 0.29 | 0.35 |
| GGR173 | 41.61 | 42.61 | 1 | 0.16 | 0.17 | 0.49 |
| GGR173 | 42.61 | 43.61 | 1 | 0.17 | 0.38 | 0.55 |
| GGR173 | 43.61 | 44.61 | 1 | 0.20 | 0.42 | 0.62 |
| GGR176 | 65.44 | 66.44 | 1 | 1.05 | 1.36 | 2.41 |
| GGR176 | 66.44 | 67.44 | 1 | 1.25 | 0.73 | 1.97 |
| GGR176 | 67.44 | 68.44 | 1 | 0.93 | 0.73 | 1.70 |
| GGR176 | 68.44 | 69.44 | | 0.93 | 0.77 | 1.40 |
| GGR176 GGR176 | | | 1 | 2.54 | | 4.31 |
| | 69.44 | 70.44 | 1 | | 1.77 | |
| GGR176 | 70.44 | 71.44 | 1 | 0.11 | 0.95 | 1.06 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|-------|------|-------------|
| GGR176 | 71.44 | 72.44 | 1 | 0.36 | 0.86 | 1.22 |
| GGR176 | 72.44 | 73.44 | 1 | 0.53 | 0.81 | 1.34 |
| GGR176 | 73.44 | 74.44 | 1 | 0.77 | 0.84 | 1.61 |
| GGR176 | 74.44 | 75.44 | 1 | 0.38 | 0.42 | 0.80 |
| GGR176 | 75.44 | 76.44 | 1 | 0.10 | 0.16 | 0.25 |
| GGR176 | 76.44 | 77.44 | 1 | 0.03 | 0.77 | 0.80 |
| GGR176 | 77.44 | 78.44 | 1 | 0.03 | 1.80 | 1.83 |
| GGR176 | 78.44 | 79.44 | 1 | 0.06 | 1.17 | 1.23 |
| GGR176 | 79.44 | 80.44 | 1 | 0.07 | 1.36 | 1.43 |
| GGR176 | 80.44 | 81.44 | 1 | 0.07 | 1.62 | 1.70 |
| GGR176 | 81.44 | 82.44 | 1 | 0.15 | 1.70 | 1.85 |
| GGR176 | 82.44 | 83.44 | 1 | 0.13 | 2.24 | 2.36 |
| GGR176 | 83.44 | 84.44 | 1 | 0.11 | 2.69 | 2.80 |
| GGR176 | 84.44 | 85.44 | 1 | 0.14 | 0.69 | 0.83 |
| GGR176 | 85.44 | 86.44 | 1 | 0.14 | 0.69 | 0.83 |
| GGR177 | 47.55 | 48.55 | 1 | 0.07 | 1.18 | 1.25 |
| GGR177 | 48.55 | 49.55 | 1 | 0.07 | 1.03 | 1.10 |
| GGR177 | 49.55 | 50.55 | 1 | 0.05 | 0.30 | 0.35 |
| GGR177 | 50.55 | 51.55 | 1 | 1.13 | 1.67 | 2.80 |
| GGR177 | 51.55 | 52.55 | 1 | 1.00 | 2.29 | 3.30 |
| GGR177 | 52.55 | 53.55 | 1 | 17.94 | 4.83 | 22.77 |
| GGR177 | 53.55 | 54.55 | 1 | 1.54 | 1.45 | 2.99 |
| GGR177 | 54.55 | 55.55 | 1 | 1.22 | 1.52 | 2.73 |
| GGR177 | 55.55 | 56.55 | 1 | 1.15 | 1.60 | 2.75 |
| GGR177 | 56.55 | 57.55 | 1 | 1.56 | 1.88 | 3.44 |
| GGR177 | 57.55 | 58.55 | 1 | 1.22 | 1.25 | 2.47 |
| GGR177 | 58.55 | 59.55 | 1 | 0.97 | 0.92 | 1.89 |
| GGR177 | 59.55 | 60.55 | 1 | 0.46 | 1.08 | 1.54 |
| GGR177 | 60.55 | 61.55 | 1 | 0.37 | 0.75 | 1.12 |
| GGR177 | 61.55 | 62.55 | 1 | 0.30 | 0.70 | 0.80 |
| GGR177 | 62.55 | 63.55 | 1 | 0.30 | 0.30 | 0.60 |
| GGR177 | 63.55 | 64.55 | 1 | 0.47 | 0.71 | 1.18 |
| GGR177 | 64.55 | 65.55 | 1 | 0.63 | 1.07 | 1.69 |
| GGR177 | 65.55 | 66.55 | 1 | 1.86 | 1.55 | 3.41 |
| GGR177 | 66.55 | 67.55 | 1 | 6.03 | 1.88 | 7.91 |
| GGR177 | 67.55 | 68.55 | 1 | 2.58 | 1.30 | 3.88 |
| GGR177 | 68.55 | 69.55 | 1 | 0.84 | 1.42 | 2.26 |
| GGR177 | 69.55 | 70.55 | 1 | 0.04 | 0.89 | 1.11 |
| GGR177 | 70.55 | 71.55 | 1 | 0.21 | 0.03 | 0.33 |
| GGR177 | 71.55 | 71.55 | 1 | 0.20 | 0.13 | 0.25 |
| GGR177 | 72.55 | 73.55 | 1 | 0.13 | 0.09 | 0.24 |
| GGR177 | 73.55 | 74.55 | 1 | 0.11 | 0.12 | 0.23 |
| GGR177 | 74.55 | 75.55 | 1 | 0.06 | 0.17 | 0.36 |
| GGR177 | 75.55 | 76.55 | 1 | 0.10 | 0.20 | 0.48 |
| GGR177 | 76.55 | 77.55 | 1 | 0.21 | 0.27 | 0.48 |
| GGR177 | 77.55 | 78.55 | 1 | 0.20 | 1.29 | 1.39 |
| GGR177 | 78.55 | 79.55 | | 0.10 | 1.29 | 1.28 |
| | | | 1 | | | |
| GGR177 | 79.55 | 80.55 | 1 | 0.08 | 0.59 | 0.67 |
| GGR177 | 80.55 | 81.55 | 1 | 0.12 | 0.73 | 0.85 |
| GGR177 | 81.55 | 82.55 | 1 | 0.12 | 0.78 | 0.90 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR177 | 82.55 | 83.55 | 1 | 0.13 | 0.91 | 1.04 |
| GGR177 | 83.55 | 84.55 | 1 | 0.19 | 0.85 | 1.04 |
| GGR177 | 84.55 | 85.55 | 1 | 0.16 | 0.45 | 0.61 |
| GGR178 | 41.45 | 42.45 | 1 | 0.02 | 1.08 | 1.10 |
| GGR178 | 42.45 | 43.45 | 1 | 0.03 | 0.73 | 0.76 |
| GGR178 | 43.45 | 44.45 | 1 | 1.41 | 1.31 | 2.72 |
| GGR178 | 44.45 | 45.45 | 1 | 3.40 | 2.18 | 5.58 |
| GGR178 | 45.45 | 46.45 | 1 | 1.60 | 1.55 | 3.14 |
| GGR178 | 46.45 | 47.45 | 1 | 1.16 | 1.69 | 2.85 |
| GGR178 | 47.45 | 48.45 | 1 | 0.82 | 2.10 | 2.92 |
| GGR178 | 48.45 | 49.45 | 1 | 1.61 | 1.71 | 3.32 |
| GGR178 | 49.45 | 50.45 | 1 | 1.70 | 1.41 | 3.11 |
| GGR178 | 50.45 | 51.45 | 1 | 1.55 | 0.92 | 2.47 |
| GGR178 | 51.45 | 52.45 | 1 | 1.63 | 1.92 | 3.54 |
| GGR178 | 52.45 | 53.45 | 1 | 1.55 | 2.06 | 3.61 |
| GGR178 | 53.45 | 54.45 | 1 | 1.28 | 1.72 | 3.00 |
| GGR178 | 54.45 | 55.45 | 1 | 1.73 | 1.15 | 2.88 |
| GGR178 | 55.45 | 56.45 | 1 | 1.78 | 0.94 | 2.72 |
| GGR178 | 56.45 | 57.45 | 1 | 1.36 | 0.91 | 2.27 |
| GGR178 | 57.45 | 58.45 | 1 | 0.77 | 0.59 | 1.35 |
| GGR179 | 40.75 | 41.75 | 1 | 0.30 | 0.88 | 1.18 |
| GGR179 | 41.75 | 42.75 | 1 | 0.51 | 1.66 | 2.18 |
| GGR179 | 42.75 | 43.75 | 1 | 0.75 | 2.55 | 3.30 |
| GGR179 | 43.75 | 44.75 | 1 | 1.51 | 1.93 | 3.44 |
| GGR179 | 44.75 | 45.75 | 1 | 2.78 | 2.48 | 5.27 |
| GGR179 | 45.75 | 46.75 | 1 | 0.73 | 1.74 | 2.46 |
| GGR179 | 46.75 | 47.75 | 1 | 1.55 | 2.20 | 3.75 |
| GGR179 | 47.75 | 48.75 | 1 | 2.29 | 1.80 | 4.08 |
| GGR179 | 48.75 | 49.75 | 1 | 1.72 | 1.52 | 3.24 |
| GGR179 | 49.75 | 50.75 | 1 | 0.62 | 1.13 | 1.75 |
| GGR179 | 50.75 | 51.75 | 1 | 1.65 | 2.35 | 4.00 |
| GGR179 | 51.75 | 52.75 | 1 | 1.60 | 2.04 | 3.64 |
| GGR179 | 52.75 | 53.75 | 1 | 1.10 | 0.91 | 2.01 |
| GGR179 | 53.75 | 54.75 | 1 | 0.85 | 0.56 | 1.41 |
| GGR179 | 54.75 | 55.75 | 1 | 0.75 | 0.63 | 1.38 |
| GGR179 | 55.75 | 56.75 | 1 | 0.65 | 1.03 | 1.68 |
| GGR179 | 56.75 | 57.75 | 1 | 0.52 | 1.29 | 1.82 |
| GGR179 | 57.75 | 58.75 | 1 | 0.46 | 1.18 | 1.64 |
| GGR179 | 58.75 | 59.75 | 1 | 0.41 | 0.51 | 0.92 |
| GGR181 | 35.97 | 36.97 | 1 | 0.22 | 0.72 | 0.94 |
| GGR181 | 36.97 | 37.97 | 1 | 0.12 | 0.60 | 0.72 |
| GGR181 | 37.97 | 38.97 | 1 | 0.02 | 0.47 | 0.49 |
| GGR181 | 38.97 | 39.97 | 1 | 0.93 | 0.65 | 1.58 |
| GGR181 | 39.97 | 40.97 | 1 | 0.64 | 0.66 | 1.30 |
| GGR181 | 40.97 | 41.97 | 1 | 0.20 | 0.67 | 0.87 |
| GGR181 | 41.97 | 42.97 | 1 | 0.42 | 0.92 | 1.33 |
| GGR181 | 42.97 | 43.97 | 1 | 0.53 | 0.73 | 1.26 |
| GGR181 | 43.97 | 44.97 | 1 | 0.68 | 0.73 | 1.07 |
| GGR181 | 44.97 | 45.97 | 1 | 0.77 | 0.39 | 1.16 |
| GGR181 | 45.97 | 46.97 | 1 | 0.77 | 0.39 | 0.84 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR181 | 46.97 | 47.97 | 1 | 0.03 | 0.18 | 0.21 |
| GGR181 | 47.97 | 48.97 | 1 | 0.25 | 0.31 | 0.56 |
| GGR181 | 48.97 | 49.97 | 1 | 0.51 | 0.35 | 0.86 |
| GGR181 | 49.97 | 50.97 | 1 | 1.01 | 0.39 | 1.40 |
| GGR181 | 50.97 | 51.97 | 1 | 1.03 | 0.53 | 1.57 |
| GGR181 | 51.97 | 52.97 | 1 | 1.03 | 0.61 | 1.64 |
| GGR181 | 52.97 | 53.97 | 1 | 0.99 | 0.70 | 1.69 |
| GGR181 | 53.97 | 54.97 | 1 | 0.62 | 0.33 | 0.95 |
| GGR181 | 54.97 | 55.97 | 1 | 0.51 | 0.19 | 0.70 |
| GGR181 | 55.97 | 56.97 | 1 | 0.67 | 0.19 | 0.86 |
| GGR182 | 40.36 | 41.36 | 1 | 0.01 | 0.61 | 0.62 |
| GGR182 | 41.36 | 42.36 | 1 | 0.01 | 0.33 | 0.34 |
| GGR182 | 42.36 | 43.36 | 1 | 0.01 | 0.55 | 0.56 |
| GGR182 | 43.36 | 44.36 | 1 | 0.02 | 0.81 | 0.83 |
| GGR182 | 44.36 | 45.36 | 1 | 0.16 | 1.98 | 2.14 |
| GGR182 | 45.36 | 46.36 | 1 | 0.58 | 3.00 | 3.59 |
| GGR182 | 46.36 | 47.36 | 1 | 0.96 | 2.44 | 3.40 |
| GGR182 | 47.36 | 48.36 | 1 | 0.36 | 1.48 | 1.84 |
| GGR182 | 48.36 | 49.36 | 1 | 1.93 | 5.29 | 7.23 |
| GGR182 | 49.36 | 50.36 | 1 | 6.29 | 5.90 | 12.19 |
| GGR182 | 50.36 | 51.36 | 1 | 0.65 | 0.69 | 1.33 |
| GGR182 | 51.36 | 52.36 | 1 | 0.09 | 0.24 | 0.33 |
| GGR182 | 52.36 | 53.36 | 1 | 0.10 | 0.26 | 0.36 |
| GGR182 | 53.36 | 54.36 | 1 | 0.23 | 0.20 | 0.43 |
| GGR182 | 54.36 | 55.36 | 1 | 0.22 | 0.23 | 0.46 |
| GGR182 | 55.36 | 56.36 | 1 | 0.17 | 0.32 | 0.49 |
| GGR182 | 56.36 | 57.36 | 1 | 0.15 | 0.29 | 0.44 |
| GGR182 | 57.36 | 58.36 | 1 | 0.17 | 0.33 | 0.50 |
| GGR182 | 58.36 | 59.36 | 1 | 0.22 | 0.43 | 0.65 |
| GGR182 | 59.36 | 60.36 | 1 | 0.42 | 0.57 | 0.99 |
| GGR182 | 60.36 | 61.36 | 1 | 0.50 | 0.60 | 1.10 |
| GGR182 | 61.36 | 62.36 | 1 | 0.56 | 0.55 | 1.11 |
| GGR183 | 40.23 | 41.23 | 1 | 6.29 | 4.68 | 10.97 |
| GGR183 | 41.23 | 42.23 | 1 | 0.67 | 3.53 | 4.20 |
| GGR183 | 42.23 | 43.23 | 1 | 0.24 | 2.79 | 3.03 |
| GGR183 | 43.23 | 44.23 | 1 | 1.80 | 2.96 | 4.76 |
| GGR183 | 44.23 | 45.23 | 1 | 6.05 | 2.57 | 8.62 |
| GGR183 | 45.23 | 46.23 | 1 | 6.55 | 4.14 | 10.69 |
| GGR183 | 46.23 | 47.23 | 1 | 0.85 | 2.31 | 3.16 |
| GGR183 | 47.23 | 48.23 | 1 | 3.49 | 3.93 | 7.42 |
| GGR183 | 48.23 | 49.23 | 1 | 1.78 | 3.26 | 5.04 |
| GGR183 | 49.23 | 50.23 | 1 | 0.54 | 2.46 | 3.00 |
| GGR183 | 50.23 | 51.23 | 1 | 0.45 | 2.55 | 3.00 |
| GGR183 | 51.23 | 52.23 | 1 | 2.52 | 3.99 | 6.51 |
| GGR183 | 52.23 | 53.23 | 1 | 0.74 | 0.81 | 1.55 |
| GGR183 | 53.23 | 54.23 | 1 | 1.72 | 1.53 | 3.25 |
| GGR183 | 54.23 | 55.23 | 1 | 2.22 | 1.86 | 4.08 |
| GGR183 | 55.23 | 56.23 | 1 | 0.91 | 0.46 | 1.37 |
| GGR183 | 56.23 | 57.23 | 1 | 1.29 | 1.26 | 2.55 |
| GGR183 | 57.23 | 58.23 | 1 | 1.49 | 1.56 | 3.05 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR183 | 58.23 | 59.23 | 1 | 1.84 | 1.65 | 3.49 |
| GGR183 | 59.23 | 60.23 | 1 | 2.13 | 1.61 | 3.74 |
| GGR183 | 60.23 | 61.23 | 1 | 1.77 | 0.56 | 2.33 |
| GGR183 | 61.23 | 62.23 | 1 | 1.45 | 0.37 | 1.82 |
| GGR183 | 62.23 | 63.23 | 1 | 0.98 | 0.27 | 1.25 |
| GGR191 | 29.87 | 30.87 | 1 | 0.01 | 0.61 | 0.62 |
| GGR191 | 30.87 | 31.87 | 1 | 0.01 | 1.02 | 1.03 |
| GGR191 | 31.87 | 32.87 | 1 | 0.01 | 1.46 | 1.47 |
| GGR191 | 32.87 | 33.87 | 1 | 0.07 | 1.12 | 1.19 |
| GGR191 | 33.87 | 34.87 | 1 | 0.07 | 1.28 | 1.36 |
| GGR191 | 34.87 | 35.87 | 1 | 0.08 | 1.53 | 1.61 |
| GGR191 | 35.87 | 36.87 | 1 | 0.08 | 1.11 | 1.19 |
| GGR191 | 36.87 | 37.87 | 1 | 0.09 | 1.13 | 1.22 |
| GGR191 | 37.87 | 38.87 | 1 | 0.10 | 1.24 | 1.34 |
| GGR191 | 38.87 | 39.87 | 1 | 0.15 | 2.03 | 2.18 |
| GGR191 | 39.87 | 40.87 | 1 | 1.75 | 4.38 | 6.14 |
| GGR191 | 40.87 | 41.87 | 1 | 0.21 | 1.02 | 1.23 |
| GGR191 | 41.87 | 42.87 | 1 | 0.11 | 0.85 | 0.96 |
| GGR191 | 42.87 | 43.87 | 1 | 0.01 | 0.67 | 0.68 |
| GGR191 | 43.87 | 44.87 | 1 | 0.11 | 0.62 | 0.73 |
| GGR191 | 44.87 | 45.87 | 1 | 0.11 | 0.74 | 0.86 |
| GGR191 | 45.87 | 46.87 | 1 | 0.12 | 0.89 | 1.01 |
| GGR191 | 46.87 | 47.87 | 1 | 0.12 | 0.84 | 1.02 |
| GGR191 | 47.87 | 48.87 | 1 | 0.11 | 0.61 | 0.72 |
| GGR191 | 48.87 | 49.87 | 1 | 0.01 | 0.27 | 0.28 |
| GGR191 | 49.87 | 50.87 | 1 | 0.01 | 0.38 | 0.39 |
| GGR191 | 50.87 | 51.87 | 1 | 0.01 | 0.40 | 0.41 |
| GGR191 | 51.87 | 52.87 | 1 | 0.01 | 0.41 | 0.42 |
| GGR192 | 29.5 | 30.5 | 1 | 0.01 | 1.24 | 1.25 |
| GGR192 | 30.5 | 31.5 | 1 | 0.01 | 2.49 | 2.50 |
| GGR192 | 31.5 | 32.5 | 1 | 0.01 | 3.99 | 4.00 |
| GGR192 | 32.5 | 33.5 | 1 | 0.52 | 2.66 | 3.18 |
| GGR192 | 33.5 | 34.5 | 1 | 2.30 | 5.25 | 7.55 |
| GGR192 | 34.5 | 35.5 | 1 | 0.87 | 4.10 | 4.98 |
| GGR192 | 35.5 | 36.5 | 1 | 0.19 | 3.03 | 3.22 |
| GGR192 | 36.5 | 37.5 | 1 | 0.13 | 2.11 | 2.24 |
| GGR192 | 37.5 | 38.5 | 1 | 0.31 | 2.26 | 2.57 |
| GGR192 | 38.5 | 39.5 | 1 | 0.35 | 1.92 | 2.27 |
| GGR192 | 39.5 | 40.5 | 1 | 0.36 | 1.56 | 1.92 |
| GGR192 | 40.5 | 41.5 | 1 | 0.35 | 2.43 | 2.78 |
| GGR192 | 41.5 | 42.5 | 1 | 1.45 | 5.02 | 6.48 |
| GGR192 | 42.5 | 43.5 | 1 | 0.64 | 3.22 | 3.86 |
| GGR192 | 43.5 | 44.5 | 1 | 0.13 | 1.81 | 1.94 |
| GGR192 | 44.5 | 45.5 | 1 | 0.15 | 0.83 | 0.98 |
| GGR192 | 45.5 | 46.5 | 1 | 0.32 | 1.52 | 1.84 |
| GGR192 | 46.5 | 47.5 | 1 | 0.41 | 1.88 | 2.29 |
| GGR192 | 47.5 | 48.5 | 1 | 0.16 | 0.50 | 0.67 |
| GGR192 | 48.5 | 49.5 | 1 | 0.16 | 0.59 | 0.75 |
| GGR192 | 49.5 | 50.5 | 1 | 0.10 | 0.80 | 0.73 |
| GGR192 | 50.5 | 51.5 | 1 | 0.14 | 0.75 | 0.76 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR192 | 51.5 | 52.5 | 1 | 0.01 | 0.92 | 0.93 |
| GGR192 | 52.5 | 53.5 | 1 | 0.01 | 1.01 | 1.02 |
| GGR192 | 53.5 | 54.5 | 1 | 0.01 | 1.08 | 1.09 |
| GGR192 | 54.5 | 55.5 | 1 | 0.01 | 0.89 | 0.90 |
| GGR192 | 55.5 | 56.5 | 1 | 0.01 | 1.17 | 1.18 |
| GGR192 | 56.5 | 57.5 | 1 | 0.01 | 1.80 | 1.81 |
| GGR192 | 57.5 | 58.5 | 1 | 0.01 | 2.08 | 2.09 |
| GGR192 | 58.5 | 59.5 | 1 | 0.01 | 1.65 | 1.66 |
| GGR192 | 59.5 | 60.5 | 1 | 0.01 | 1.00 | 1.01 |
| GGR192 | 60.5 | 61.5 | 1 | 0.01 | 0.24 | 0.25 |
| GGR192 | 61.5 | 62.5 | 1 | 0.02 | 0.51 | 0.53 |
| GGR192 | 62.5 | 63.5 | 1 | 0.03 | 0.77 | 0.80 |
| GGR193 | 38.1 | 39.1 | 1 | 2.24 | 1.34 | 3.58 |
| GGR193 | 39.1 | 40.1 | 1 | 3.11 | 2.98 | 6.09 |
| GGR193 | 40.1 | 41.1 | 1 | 1.80 | 2.35 | 4.15 |
| GGR193 | 41.1 | 42.1 | 1 | 0.40 | 0.59 | 1.00 |
| GGR193 | 42.1 | 43.1 | 1 | 0.40 | 0.62 | 1.03 |
| GGR193 | 43.1 | 44.1 | 1 | 0.50 | 0.79 | 1.29 |
| GGR193 | 44.1 | 45.1 | 1 | 1.81 | 0.54 | 2.35 |
| GGR193 | 45.1 | 46.1 | 1 | 1.96 | 0.51 | 2.47 |
| GGR193 | 46.1 | 47.1 | 1 | 1.96 | 0.51 | 2.47 |
| GGR193 | 47.1 | 48.1 | 1 | 1.96 | 0.51 | 2.47 |
| GGR193 | 48.1 | 49.1 | 1 | 0.83 | 0.41 | 1.24 |
| GGR193 | 49.1 | 50.1 | 1 | 0.73 | 1.60 | 2.33 |
| GGR193 | 50.1 | 51.1 | 1 | 2.17 | 3.94 | 6.11 |
| GGR193 | 51.1 | 52.1 | 1 | 1.29 | 2.65 | 3.93 |
| GGR193 | 52.1 | 53.1 | 1 | 2.17 | 3.29 | 5.47 |
| GGR193 | 53.1 | 54.1 | 1 | 2.83 | 3.69 | 6.52 |
| GGR193 | 54.1 | 55.1 | 1 | 1.86 | 1.50 | 3.36 |
| GGR193 | 55.1 | 56.1 | 1 | 3.82 | 3.73 | 7.54 |
| GGR193 | 56.1 | 57.1 | 1 | 2.42 | 4.16 | 6.58 |
| GGR193 | 57.1 | 58.1 | 1 | 0.58 | 1.25 | 1.83 |
| GGR193 | 58.1 | 59.1 | 1 | 0.17 | 0.64 | 0.81 |
| GGR193 | 59.1 | 60.1 | 1 | 0.19 | 0.63 | 0.82 |
| GGR193 | 60.1 | 61.1 | 1 | 0.31 | 0.93 | 1.24 |
| GGR193 | 61.1 | 62.1 | 1 | 0.99 | 1.30 | 2.29 |
| GGR193 | 62.1 | 63.1 | 1 | 1.01 | 1.13 | 2.14 |
| GGR193 | 63.1 | 64.1 | 1 | 0.22 | 0.72 | 0.94 |
| GGR193 | 64.1 | 65.1 | 1 | 0.05 | 0.61 | 0.66 |
| GGR193 | 65.1 | 66.1 | 1 | 0.09 | 0.49 | 0.58 |
| GGR193 | 66.1 | 67.1 | 1 | 0.09 | 0.49 | 0.58 |
| GGR206 | 30.54 | 31.54 | 1 | 0.01 | 1.28 | 1.29 |
| GGR206 | 31.54 | 32.54 | 1 | 0.01 | 2.08 | 2.09 |
| GGR206 | 32.54 | 33.54 | 1 | 0.01 | 0.30 | 0.31 |
| GGR206 | 33.54 | 34.54 | 1 | 0.05 | 1.86 | 1.91 |
| GGR206 | 34.54 | 35.54 | 1 | 0.05 | 2.25 | 2.30 |
| GGR206 | 35.54 | 36.54 | 1 | 0.05 | 2.65 | 2.70 |
| GGR206 | 36.54 | 37.54 | 1 | 0.05 | 1.18 | 1.23 |
| GGR206 | 37.54 | 38.54 | 1 | 0.03 | 1.16 | 1.24 |
| GGR206 | 38.54 | 39.54 | 1 | 0.08 | 1.53 | 1.71 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|-------|------|-------------|
| GGR206 | 39.54 | 40.54 | 1 | 0.43 | 1.30 | 1.73 |
| GGR206 | 40.54 | 41.54 | 1 | 0.50 | 1.10 | 1.60 |
| GGR206 | 41.54 | 42.54 | 1 | 0.22 | 0.58 | 0.80 |
| GGR206 | 42.54 | 43.54 | 1 | 0.09 | 0.46 | 0.55 |
| GGR206 | 43.54 | 44.54 | 1 | 0.04 | 0.44 | 0.48 |
| GGR206 | 44.54 | 45.54 | 1 | 0.12 | 0.57 | 0.69 |
| GGR206 | 45.54 | 46.54 | 1 | 0.13 | 0.87 | 0.99 |
| GGR206 | 46.54 | 47.54 | 1 | 0.13 | 0.77 | 0.90 |
| GGR206 | 47.54 | 48.54 | 1 | 0.13 | 0.18 | 0.31 |
| GGR206 | 48.54 | 49.54 | 1 | 1.05 | 1.45 | 2.50 |
| GGR206 | 49.54 | 50.54 | 1 | 0.84 | 0.60 | 1.44 |
| GGR206 | 50.54 | 51.54 | 1 | 0.63 | 0.20 | 0.83 |
| GGR206 | 51.54 | 52.54 | 1 | 0.24 | 0.25 | 0.49 |
| GGR206 | 52.54 | 53.54 | 1 | 0.22 | 0.37 | 0.59 |
| GGR206 | 53.54 | 54.54 | 1 | 0.61 | 0.80 | 1.41 |
| GGR206 | 54.54 | 55.54 | 1 | 0.44 | 1.63 | 2.07 |
| GGR206 | 55.54 | 56.54 | 1 | 0.41 | 1.87 | 2.28 |
| GGR206 | 56.54 | 57.54 | 1 | 0.41 | 2.03 | 2.44 |
| GGR206 | 57.54 | 58.54 | 1 | 0.53 | 1.16 | 1.69 |
| GGR206 | 58.54 | 59.54 | 1 | 0.82 | 0.89 | 1.72 |
| GGR206 | 59.54 | 60.54 | 1 | 1.55 | 0.84 | 2.39 |
| GGR206 | 60.54 | 61.54 | 1 | 1.03 | 0.14 | 1.17 |
| GGR206 | 61.54 | 62.54 | 1 | 1.16 | 1.15 | 2.30 |
| GGR206 | 62.54 | 63.54 | 1 | 0.29 | 1.06 | 1.35 |
| GGR206 | 63.54 | 64.54 | 1 | 0.16 | 1.02 | 1.18 |
| GGR206 | 64.54 | 65.54 | 1 | 0.10 | 1.00 | 1.10 |
| GGR208 | 98.37 | 99.37 | 1 | 18.54 | 9.12 | 27.66 |
| GGR208 | 99.37 | 100.37 | 1 | 3.74 | 1.51 | 5.25 |
| GGR208 | 100.37 | 101.37 | 1 | 4.50 | 2.14 | 6.63 |
| GGR208 | 101.37 | 102.37 | 1 | 0.59 | 0.45 | 1.04 |
| GGR208 | 102.37 | 103.37 | 1 | 2.86 | 1.92 | 4.78 |
| GGR208 | 103.37 | 104.37 | 1 | 6.30 | 3.53 | 9.83 |
| GGR208 | 104.37 | 105.37 | 1 | 2.10 | 0.65 | 2.75 |
| GGR209 | 109.73 | 110.73 | 1 | 0.28 | 0.33 | 0.61 |
| GGR209 | 110.73 | 111.73 | 1 | 4.13 | 2.73 | 6.86 |
| GGR209 | 111.73 | 112.73 | 1 | 0.93 | 1.77 | 2.70 |
| GGR209 | 112.73 | 113.73 | 1 | 1.65 | 2.55 | 4.19 |
| GGR209 | 113.73 | 114.73 | 1 | 5.55 | 4.94 | 10.49 |
| GGR209 | 114.73 | 115.73 | 1 | 1.75 | 0.46 | 2.21 |
| GGR209 | 115.73 | 116.73 | 1 | 0.80 | 0.40 | 1.00 |
| GGR209 | 116.73 | 117.73 | 1 | 0.04 | 0.20 | 0.05 |
| GGR209 | 117.73 | 118.73 | 1 | 0.69 | 0.01 | 0.70 |
| GGR209 | 118.73 | 119.73 | 1 | 0.82 | 0.01 | 0.83 |
| GGR211 | 22.83 | 23.83 | 1 | 0.01 | 0.52 | 0.53 |
| GGR211 | 23.83 | 24.83 | 1 | 0.01 | 0.64 | 0.65 |
| GGR211 | 24.83 | 25.83 | 1 | 0.01 | 0.76 | 0.77 |
| GGR211 | 25.83 | 26.83 | 1 | 0.01 | 1.90 | 2.08 |
| GGR211 | 26.83 | 27.83 | 1 | 0.18 | 2.49 | 2.82 |
| GGR211 | 27.83 | 28.83 | 1 | 0.53 | 3.20 | 3.71 |
| GGR211 | 28.83 | 29.83 | 1 | 1.05 | 1.59 | 2.64 |

| From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|----------|---|---|---|---|--|
| 29.83 | 30.83 | 1 | 2.20 | 1.71 | 3.90 |
| 30.83 | 31.83 | 1 | 0.76 | 2.59 | 3.35 |
| 31.83 | 32.83 | 1 | 1.26 | 2.26 | 3.51 |
| 32.83 | 33.83 | 1 | 1.74 | 1.98 | 3.73 |
| 33.83 | 34.83 | 1 | 1.75 | 1.94 | 3.69 |
| 34.83 | 35.83 | 1 | 1.59 | 2.03 | 3.61 |
| 35.83 | 36.83 | 1 | | 1.83 | 3.04 |
| 36.83 | | 1 | | | 1.37 |
| 37.83 | | 1 | | | 1.71 |
| | | 1 | | | 1.85 |
| | | 1 | | | 1.93 |
| 40.83 | 41.83 | 1 | 0.27 | | 1.32 |
| | | | | | 1.11 |
| | | 1 | | | 1.54 |
| | | 1 | | | 2.05 |
| | | | | | 2.47 |
| 45.83 | 46.83 | 1 | 0.09 | 3.39 | 3.48 |
| 46.83 | 47.83 | 1 | | | 1.95 |
| | | | | | 0.90 |
| | | | | | 1.01 |
| | | | | | 1.58 |
| | | | | | 2.16 |
| | | | | | 12.14 |
| | | | | | 7.67 |
| | | | | | 3.01 |
| | | | | | 2.09 |
| | | | | | 2.06 |
| | | | | | 0.63 |
| | | | _ | | 0.88 |
| | | | _ | | 0.52 |
| | | | _ | | 0.61 |
| | | | | | 1.09 |
| | | | | | 0.82 |
| | | | | | 0.67 |
| | | 1 | | | 0.45 |
| | | | | | 0.34 |
| | | 1 | | | 0.34 |
| | | 1 | | | 0.53 |
| | | | | | 0.40 |
| | | | | | 0.36 |
| | | | | | 0.53 |
| | | | | | 0.60 |
| | | | | | 0.72 |
| | | | | | 1.41 |
| | | | | | 5.26 |
| | | | | | 7.96 |
| | | | | | 2.96 |
| | | | | | 2.18 |
| | | | | | 1.46 |
| | | | | | 0.97 |
| | 32.83 33.83 34.83 35.83 36.83 37.83 38.83 39.83 40.83 41.83 42.83 43.83 44.83 | 32.83 33.83 33.83 34.83 34.83 35.83 36.83 37.83 37.83 38.83 39.83 40.83 40.83 41.83 42.83 43.83 43.83 44.83 44.83 45.83 45.83 46.83 47.83 48.83 49.83 50.83 50.83 51.83 52.83 53.83 54.83 55.83 55.83 56.83 32.25 33.25 34.25 34.25 34.25 35.25 36.25 37.25 37.25 38.25 39.25 40.25 40.25 42.25 42.25 43.25 45.25 46.25 46.25 47.25 47.25 48.25 49.25 50.25 50.25 50.25 50.25 53.25 | 32.83 33.83 1 33.83 34.83 1 34.83 35.83 1 35.83 36.83 1 37.83 38.83 1 38.83 39.83 1 39.83 40.83 1 40.83 41.83 1 41.83 42.83 1 42.83 43.83 1 44.83 45.83 1 45.83 46.83 1 46.83 47.83 1 47.83 48.83 1 49.83 50.83 1 50.83 51.83 1 51.83 52.83 1 52.83 53.83 1 55.83 56.83 1 55.83 56.83 1 33.25 34.25 1 34.25 35.25 1 36.25 37.25 1 37.25 38.25 1 39.25 40.25 1 40.25 41.25 1 <t< td=""><td>32.83 33.83 1 1.74 33.83 34.83 1 1.75 34.83 35.83 1 1.59 35.83 36.83 1 1.20 36.83 37.83 1 0.19 37.83 38.83 1 0.57 38.83 39.83 1 0.70 39.83 40.83 1 0.68 40.83 41.83 1 0.27 41.83 42.83 1 0.10 42.83 43.83 1 0.19 43.83 44.83 1 0.22 44.83 45.83 1 0.29 45.83 46.83 1 0.09 46.83 47.83 1 0.09 46.83 47.83 1 0.09 47.83 48.83 1 0.09 48.83 49.83 1 0.09 48.83 50.83 1 0.06 50.83 51.83 1 0.06 55.83 53.83 1</td><td>32.83 33.83 1 1.74 1.98 33.83 34.83 1 1.75 1.94 34.83 35.83 1 1.59 2.03 35.83 36.83 1 1.20 1.83 36.83 37.83 1 0.19 1.18 37.83 38.83 1 0.57 1.14 38.83 39.83 1 0.70 1.15 39.83 40.83 1 0.68 1.25 40.83 41.83 1 0.10 1.01 41.83 42.83 1 0.10 1.01 42.83 43.83 1 0.19 1.35 43.83 44.83 1 0.26 1.79 44.83 45.83 1 0.28 2.20 45.83 46.83 1 0.09 3.39 46.83 47.83 1 0.09 1.86 47.83 48.83 1 0.09 0.81 <!--</td--></td></t<> | 32.83 33.83 1 1.74 33.83 34.83 1 1.75 34.83 35.83 1 1.59 35.83 36.83 1 1.20 36.83 37.83 1 0.19 37.83 38.83 1 0.57 38.83 39.83 1 0.70 39.83 40.83 1 0.68 40.83 41.83 1 0.27 41.83 42.83 1 0.10 42.83 43.83 1 0.19 43.83 44.83 1 0.22 44.83 45.83 1 0.29 45.83 46.83 1 0.09 46.83 47.83 1 0.09 46.83 47.83 1 0.09 47.83 48.83 1 0.09 48.83 49.83 1 0.09 48.83 50.83 1 0.06 50.83 51.83 1 0.06 55.83 53.83 1 | 32.83 33.83 1 1.74 1.98 33.83 34.83 1 1.75 1.94 34.83 35.83 1 1.59 2.03 35.83 36.83 1 1.20 1.83 36.83 37.83 1 0.19 1.18 37.83 38.83 1 0.57 1.14 38.83 39.83 1 0.70 1.15 39.83 40.83 1 0.68 1.25 40.83 41.83 1 0.10 1.01 41.83 42.83 1 0.10 1.01 42.83 43.83 1 0.19 1.35 43.83 44.83 1 0.26 1.79 44.83 45.83 1 0.28 2.20 45.83 46.83 1 0.09 3.39 46.83 47.83 1 0.09 1.86 47.83 48.83 1 0.09 0.81 </td |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|------------------|----------|--------|------------|-------|------|-------------|
| GGR214 | 62.72 | 63.72 | 1 | 0.31 | 1.03 | 1.34 |
| GGR214 | 63.72 | 64.72 | 1 | 0.07 | 1.69 | 1.76 |
| GGR214 | 64.72 | 65.72 | 1 | 0.11 | 2.23 | 2.34 |
| GGR214 | 65.72 | 66.72 | 1 | 0.18 | 1.70 | 1.88 |
| GGR214 | 66.72 | 67.72 | 1 | 0.27 | 0.95 | 1.22 |
| GGR215 | 65.47 | 66.47 | 1 | 12.97 | 4.08 | 17.05 |
| GGR215 | 66.47 | 67.47 | 1 | 0.71 | 1.90 | 2.61 |
| GGR215 | 67.47 | 68.47 | 1 | 2.11 | 0.91 | 3.02 |
| GGR216 | 58.83 | 59.83 | 1 | 3.92 | 0.01 | 3.93 |
| GGR216 | 59.83 | 60.83 | 1 | 0.96 | 0.01 | 0.97 |
| GGR216 | 60.83 | 61.83 | 1 | 0.12 | 0.01 | 0.13 |
| GGR217 | 96.62 | 97.62 | 1 | 0.05 | 3.53 | 3.57 |
| GGR217 | 97.62 | 98.62 | 1 | 0.07 | 5.93 | 6.00 |
| GGR217 | 98.62 | 99.62 | 1 | 0.11 | 3.85 | 3.96 |
| GGR217 | 99.62 | 100.62 | 1 | 0.69 | 1.67 | 2.37 |
| GGR217 | 100.62 | 101.62 | 1 | 1.08 | 2.30 | 3.38 |
| GGR217 | 101.62 | 102.62 | 1 | 0.47 | 1.31 | 1.78 |
| GGR217 | 102.62 | 103.62 | 1 | 0.46 | 0.64 | 1.10 |
| GGR217 | 103.62 | 104.62 | 1 | 0.23 | 0.33 | 0.55 |
| GGR217 | 104.62 | 105.62 | 1 | 0.30 | 0.57 | 0.87 |
| GGR217 | 105.62 | 106.62 | 1 | 0.52 | 1.13 | 1.65 |
| GGR217 | 106.62 | 107.62 | 1 | 0.31 | 0.74 | 1.04 |
| GGR217 | 107.62 | 108.62 | 1 | 0.23 | 0.59 | 0.82 |
| GGR217 | 108.62 | 109.62 | 1 | 0.64 | 1.17 | 1.81 |
| GGR217 | 109.62 | 110.62 | 1 | 2.79 | 2.68 | 5.47 |
| GGR217 | 110.62 | 111.62 | 1 | 4.89 | 3.87 | 8.76 |
| GGR217 | 111.62 | 112.62 | 1 | 3.94 | 2.70 | 6.64 |
| GGR217 | 112.62 | 113.62 | 1 | 2.47 | 1.08 | 3.55 |
| GGR217 | 113.62 | 114.62 | 1 | 2.47 | 1.08 | 3.55 |
| GGR217 | 114.62 | 115.62 | 1 | 2.27 | 0.81 | 3.08 |
| GGR217 | 115.62 | 116.62 | 1 | 2.12 | 0.79 | 2.91 |
| GGR217 | 116.62 | 117.62 | 1 | 2.27 | 1.17 | 3.44 |
| GGR217 | 117.62 | 118.62 | 1 | 2.45 | 2.36 | 4.81 |
| GGR217 | 118.62 | 119.62 | 1 | 0.62 | 0.50 | 1.12 |
| GGR217 | 119.62 | 120.62 | 1 | 2.52 | 0.89 | 3.40 |
| GGR217 | 120.62 | 121.62 | 1 | 4.43 | 1.29 | 5.72 |
| GGR219 | 22.56 | 23.56 | 1 | 0.01 | 1.07 | 1.08 |
| GGR219 | 23.56 | 24.56 | 1 | 0.03 | 1.57 | 1.59 |
| GGR219 | 24.56 | 25.56 | 1 | 0.02 | 1.64 | 1.67 |
| GGR219 | 25.56 | 26.56 | 1 | 0.01 | 1.47 | 1.48 |
| GGR219 | 26.56 | 27.56 | 1 | 0.11 | 1.98 | 2.09 |
| GGR219 | 27.56 | 28.56 | 1 | 0.12 | 2.06 | 2.18 |
| GGR219 | 28.56 | 29.56 | 1 | 0.06 | 1.66 | 1.72 |
| GGR219 | 29.56 | 30.56 | 1 | 0.09 | 1.60 | 1.69 |
| GGR219 | 30.56 | 31.56 | 1 | 0.11 | 1.51 | 1.62 |
| GGR219 | 31.56 | 32.56 | 1 | 0.12 | 1.20 | 1.32 |
| GGR219 | 32.56 | 33.56 | 1 | 0.12 | 1.00 | 1.14 |
| GGR219 | 33.56 | 34.56 | 1 | 0.15 | 0.81 | 0.97 |
| GGR219 GGR219 | 34.56 | 35.56 | 1 | 0.10 | 0.32 | 0.42 |
| GGR219 GGR219 | 35.56 | 36.56 | 1 | 0.10 | 0.32 | 0.33 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|------------------|----------|--------|------------|------|------|-------------|
| GGR219 | 36.56 | 37.56 | 1 | 0.10 | 0.21 | 0.31 |
| GGR219 | 37.56 | 38.56 | 1 | 0.11 | 0.67 | 0.78 |
| GGR219 | 38.56 | 39.56 | 1 | 0.12 | 0.47 | 0.58 |
| GGR219 | 39.56 | 40.56 | 1 | 0.12 | 0.30 | 0.42 |
| GGR219 | 40.56 | 41.56 | 1 | 0.03 | 0.20 | 0.23 |
| GGR219 | 41.56 | 42.56 | 1 | 0.02 | 0.25 | 0.27 |
| GGR219 | 42.56 | 43.56 | 1 | 0.01 | 0.29 | 0.30 |
| GGR219 | 43.56 | 44.56 | 1 | 0.01 | 0.13 | 0.14 |
| GGR219 | 44.56 | 45.56 | 1 | 0.01 | 0.26 | 0.27 |
| GGR219 | 45.56 | 46.56 | 1 | 0.01 | 0.42 | 0.43 |
| GGR219 | 46.56 | 47.56 | 1 | 0.01 | 0.41 | 0.42 |
| GGR219 | 47.56 | 48.56 | 1 | 0.01 | 0.41 | 0.42 |
| GGR220 | 36.21 | 37.21 | 1 | 0.01 | 3.43 | 3.44 |
| GGR220 | 37.21 | 38.21 | 1 | 0.03 | 1.41 | 1.45 |
| GGR220 | 38.21 | 39.21 | 1 | 0.14 | 0.74 | 0.88 |
| GGR220 | 39.21 | 40.21 | 1 | 0.54 | 1.20 | 1.74 |
| GGR220 | 40.21 | 41.21 | 1 | 0.44 | 0.89 | 1.33 |
| GGR220 | 41.21 | 42.21 | 1 | 0.43 | 0.83 | 1.26 |
| GGR220 | 42.21 | 43.21 | 1 | 0.54 | 1.05 | 1.59 |
| GGR220 | 43.21 | 44.21 | 1 | 0.33 | 0.87 | 1.20 |
| GGR220 | 44.21 | 45.21 | 1 | 0.34 | 1.52 | 1.86 |
| GGR220 | 45.21 | 46.21 | 1 | 0.81 | 2.38 | 3.19 |
| GGR220 | 46.21 | 47.21 | 1 | 0.77 | 1.34 | 2.11 |
| GGR220 | 47.21 | 48.21 | 1 | 0.31 | 0.68 | 0.99 |
| GGR220 | 48.21 | 49.21 | 1 | 0.07 | 0.11 | 0.18 |
| GGR220 | 49.21 | 50.21 | 1 | 0.09 | 0.68 | 0.77 |
| GGR220 | 50.21 | 51.21 | 1 | 1.04 | 2.63 | 3.68 |
| GGR220 | 51.21 | 52.21 | 1 | 0.49 | 2.96 | 3.45 |
| GGR220 | 52.21 | 53.21 | 1 | 0.12 | 2.15 | 2.27 |
| GGR220 | 53.21 | 54.21 | 1 | 0.05 | 1.47 | 1.53 |
| GGR220 | 54.21 | 55.21 | 1 | 0.01 | 1.07 | 1.08 |
| GGR220 | 55.21 | 56.21 | 1 | 0.08 | 0.91 | 0.99 |
| GGR220 | 56.21 | 57.21 | 1 | 0.06 | 1.01 | 1.07 |
| GGR220 | 57.21 | 58.21 | 1 | 0.03 | 2.23 | 2.26 |
| GGR220 | 58.21 | 59.21 | 1 | 0.30 | 1.54 | 1.84 |
| GGR220 | 59.21 | 60.21 | 1 | 0.13 | 1.54 | 1.66 |
| GGR220 | 60.21 | 61.21 | 1 | 0.05 | 0.49 | 0.54 |
| GGR220 | 61.21 | 62.21 | 1 | 0.03 | 0.40 | 0.42 |
| GGR220 | 62.21 | 63.21 | 1 | 0.01 | 0.39 | 0.40 |
| GGR220 | 63.21 | 64.21 | 1 | 0.01 | 0.84 | 0.85 |
| GGR220 | 64.21 | 65.21 | 1 | 0.01 | 0.81 | 0.82 |
| GGR220 | 65.21 | 66.21 | 1 | 0.01 | 0.70 | 0.71 |
| GGR221 | 27.58 | 28.58 | 1 | 0.01 | 0.56 | 0.57 |
| GGR221 | 28.58 | 29.58 | 1 | 0.01 | 0.55 | 0.56 |
| GGR221 | 29.58 | 30.58 | 1 | 0.12 | 1.19 | 1.31 |
| GGR221 | 30.58 | 31.58 | 1 | 0.12 | 1.34 | 1.50 |
| GGR221 | 31.58 | 32.58 | 1 | 0.13 | 0.29 | 0.33 |
| GGR221 GGR221 | 32.58 | 33.58 | 1 | 0.04 | 0.29 | 0.57 |
| GGR221 GGR221 | 33.58 | 34.58 | 1 | 0.05 | 0.51 | 0.58 |
| GGR221 GGR221 | 34.58 | 35.58 | 1 | 0.03 | 0.32 | 0.30 |
| GGNZZI | 34.30 | JJJ.JO | I | 0.04 | 0.20 | ს.ას |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR221 | 35.58 | 36.58 | 1 | 0.02 | 0.28 | 0.30 |
| GGR221 | 36.58 | 37.58 | 1 | 0.01 | 0.28 | 0.29 |
| GGR221 | 37.58 | 38.58 | 1 | 0.01 | 0.19 | 0.20 |
| GGR221 | 38.58 | 39.58 | 1 | 0.04 | 0.38 | 0.42 |
| GGR221 | 39.58 | 40.58 | 1 | 0.06 | 0.57 | 0.64 |
| GGR221 | 40.58 | 41.58 | 1 | 0.18 | 1.86 | 2.04 |
| GGR221 | 41.58 | 42.58 | 1 | 0.17 | 1.87 | 2.05 |
| GGR221 | 42.58 | 43.58 | 1 | 0.14 | 1.94 | 2.08 |
| GGR221 | 43.58 | 44.58 | 1 | 0.13 | 1.71 | 1.84 |
| GGR221 | 44.58 | 45.58 | 1 | 0.09 | 1.05 | 1.14 |
| GGR221 | 45.58 | 46.58 | 1 | 0.06 | 0.80 | 0.87 |
| GGR221 | 46.58 | 47.58 | 1 | 0.03 | 0.34 | 0.37 |
| GGR221 | 47.58 | 48.58 | 1 | 0.09 | 0.41 | 0.50 |
| GGR221 | 48.58 | 49.58 | 1 | 0.12 | 0.47 | 0.59 |
| GGR221 | 49.58 | 50.58 | 1 | 0.01 | 0.58 | 0.59 |
| GGR221 | 50.58 | 51.58 | 1 | 0.01 | 0.32 | 0.33 |
| GGR221 | 51.58 | 52.58 | 1 | 0.01 | 0.08 | 0.09 |
| GGR221 | 52.58 | 53.58 | 1 | 0.01 | 0.04 | 0.05 |
| GGR221 | 53.58 | 54.58 | 1 | 0.01 | 0.18 | 0.19 |
| GGR221 | 54.58 | 55.58 | 1 | 0.01 | 0.34 | 0.35 |
| GGR221 | 55.58 | 56.58 | 1 | 0.01 | 0.16 | 0.17 |
| GGR221 | 56.58 | 57.58 | 1 | 0.01 | 0.09 | 0.10 |
| GGR221 | 57.58 | 58.58 | 1 | 0.01 | 0.04 | 0.05 |
| GGR221 | 58.58 | 59.58 | 1 | 0.01 | 0.22 | 0.23 |
| GGR221 | 59.58 | 60.58 | 1 | 0.01 | 0.28 | 0.29 |
| GGR221 | 60.58 | 61.58 | 1 | 0.03 | 1.84 | 1.87 |
| GGR221 | 61.58 | 62.58 | 1 | 0.01 | 0.63 | 0.64 |
| GGR222 | 26.82 | 27.82 | 1 | 1.85 | 0.18 | 2.03 |
| GGR222 | 27.82 | 28.82 | 1 | 1.02 | 0.22 | 1.23 |
| GGR222 | 28.82 | 29.82 | 1 | 1.23 | 0.68 | 1.91 |
| GGR222 | 29.82 | 30.82 | 1 | 1.47 | 0.93 | 2.40 |
| GGR222 | 30.82 | 31.82 | 1 | 1.45 | 1.00 | 2.45 |
| GGR222 | 31.82 | 32.82 | 1 | 1.63 | 0.72 | 2.35 |
| GGR222 | 32.82 | 33.82 | 1 | 0.96 | 0.18 | 1.14 |
| GGR222 | 33.82 | 34.82 | 1 | 0.63 | 0.12 | 0.75 |
| GGR222 | 34.82 | 35.82 | 1 | 0.23 | 0.05 | 0.28 |
| GGR230 | 28.35 | 29.35 | 1 | 0.01 | 0.90 | 0.91 |
| GGR230 | 29.35 | 30.35 | 1 | 0.07 | 0.56 | 0.63 |
| GGR230 | 30.35 | 31.35 | 1 | 0.09 | 0.50 | 0.58 |
| GGR230 | 31.35 | 32.35 | 1 | 0.10 | 0.45 | 0.55 |
| GGR230 | 32.35 | 33.35 | 1 | 1.74 | 0.29 | 2.04 |
| GGR230 | 33.35 | 34.35 | 1 | 2.52 | 0.23 | 2.65 |
| GGR230 | 34.35 | 35.35 | 1 | 1.79 | 0.32 | 2.10 |
| GGR230 | 35.35 | 36.35 | 1 | 0.95 | 0.42 | 1.37 |
| GGR230 | 36.35 | 37.35 | 1 | 0.75 | 0.42 | 1.04 |
| GGR230 | 37.35 | 38.35 | 1 | 0.85 | 0.55 | 1.40 |
| GGR230 | 38.35 | 39.35 | 1 | 0.99 | 1.05 | 2.04 |
| GGR230 | 39.35 | 40.35 | 1 | 0.48 | 0.69 | 1.17 |
| GGR230 | 40.35 | 41.35 | 1 | 0.40 | 0.60 | 0.94 |
| GGR231 | 36.58 | 37.58 | 1 | 1.08 | 0.00 | 1.33 |
| 0011201 | 50.50 | 07.00 | 1 | 1.00 | 0.20 | 1.00 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR231 | 37.58 | 38.58 | 1 | 0.45 | 0.06 | 0.51 |
| GGR231 | 38.58 | 39.58 | 1 | 0.40 | 0.04 | 0.44 |
| GGR231 | 39.58 | 40.58 | 1 | 1.39 | 0.09 | 1.48 |
| GGR231 | 40.58 | 41.58 | 1 | 1.50 | 0.10 | 1.60 |
| GGR231 | 41.58 | 42.58 | 1 | 2.39 | 1.93 | 4.31 |
| GGR231 | 42.58 | 43.58 | 1 | 1.11 | 0.89 | 2.00 |
| GGR231 | 43.58 | 44.58 | 1 | 0.73 | 0.12 | 0.85 |
| GGR231 | 44.58 | 45.58 | 1 | 1.39 | 0.24 | 1.63 |
| GGR231 | 45.58 | 46.58 | 1 | 0.61 | 0.80 | 1.41 |
| GGR231 | 46.58 | 47.58 | 1 | 0.25 | 0.07 | 0.32 |
| GGR231 | 47.58 | 48.58 | 1 | 0.40 | 0.08 | 0.48 |
| GGR231 | 48.58 | 49.58 | 1 | 0.41 | 0.09 | 0.50 |
| GGR231 | 49.58 | 50.58 | 1 | 0.41 | 0.10 | 0.51 |
| GGR231 | 50.58 | 51.58 | 1 | 0.55 | 0.96 | 1.50 |
| GGR231 | 51.58 | 52.58 | 1 | 0.61 | 1.36 | 1.97 |
| GGR231 | 52.58 | 53.58 | 1 | 0.26 | 1.05 | 1.31 |
| GGR231 | 53.58 | 54.58 | 1 | 0.19 | 0.97 | 1.17 |
| GGR231 | 54.58 | 55.58 | 1 | 0.43 | 2.07 | 2.50 |
| GGR231 | 55.58 | 56.58 | 1 | 0.10 | 0.59 | 0.69 |
| GGR231 | 56.58 | 57.58 | 1 | 0.05 | 0.24 | 0.29 |
| GGR231 | 57.58 | 58.58 | 1 | 0.05 | 0.05 | 0.10 |
| GGR231 | 58.58 | 59.58 | 1 | 0.09 | 0.31 | 0.40 |
| GGR231 | 59.58 | 60.58 | 1 | 0.16 | 0.57 | 0.73 |
| GGR231 | 60.58 | 61.58 | 1 | 0.26 | 0.81 | 1.08 |
| GGR231 | 61.58 | 62.58 | 1 | 0.80 | 0.97 | 1.76 |
| GGR231 | 62.58 | 63.58 | 1 | 0.24 | 0.64 | 0.88 |
| GGR231 | 63.58 | 64.58 | 1 | 0.09 | 0.49 | 0.58 |
| S526 | 45.16 | 46.16 | 1 | 2.80 | 0.68 | 3.48 |
| S526 | 46.16 | 47.16 | 1 | 0.85 | 0.20 | 1.06 |
| S526 | 47.16 | 48.16 | 1 | 1.07 | 1.28 | 2.35 |
| S526 | 48.16 | 49.16 | 1 | 0.89 | 2.66 | 3.55 |
| S526 | 49.16 | 50.16 | 1 | 0.52 | 4.01 | 4.53 |
| S526 | 50.16 | 51.16 | 1 | 0.48 | 4.15 | 4.64 |
| S526 | 51.16 | 52.16 | 1 | 0.45 | 4.29 | 4.74 |
| S526 | 52.16 | 53.16 | 1 | 0.69 | 2.49 | 3.18 |
| S526 | 53.16 | 54.16 | 1 | 1.02 | 4.16 | 5.18 |
| S526 | 54.16 | 55.16 | 1 | 1.59 | 5.44 | 7.03 |
| S526 | 55.16 | 56.16 | 1 | 1.98 | 6.07 | 8.05 |
| S526 | 56.16 | 57.16 | 1 | 2.05 | 5.63 | 7.68 |
| S526 | 57.16 | 58.16 | 1 | 1.18 | 3.99 | 5.17 |
| S526 | 58.16 | 59.16 | 1 | 0.31 | 2.35 | 2.66 |
| S526 | 59.16 | 60.16 | 1 | 0.03 | 1.82 | 1.85 |
| S526 | 60.16 | 61.16 | 1 | 0.01 | 1.38 | 1.39 |
| S526 | 61.16 | 62.16 | 1 | 0.00 | 0.85 | 0.85 |
| S527 | 20.17 | 21.17 | 1 | 0.09 | 3.53 | 3.62 |
| S527 | 21.17 | 22.17 | 1 | 0.47 | 3.05 | 3.52 |
| S527 | 22.17 | 23.17 | 1 | 0.16 | 1.62 | 1.78 |
| S527 | 23.17 | 24.17 | 1 | 0.10 | 1.47 | 1.58 |
| S527 | 24.17 | 25.17 | 1 | 0.11 | 2.80 | 2.91 |
| S527 | 25.17 | 26.17 | 1 | 0.07 | 2.11 | 2.18 |

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|------------------|----------|--------|------------|------|------|-------------|
| S527 | 26.17 | 27.17 | 1 | 0.02 | 1.03 | 1.05 |
| S527 | 27.17 | 28.17 | 1 | 0.01 | 0.64 | 0.65 |
| S527 | 28.17 | 29.17 | 1 | 0.14 | 0.54 | 0.68 |
| S527 | 29.17 | 30.17 | 1 | 0.10 | 0.80 | 0.91 |
| S527 | 30.17 | 31.17 | 1 | 0.04 | 1.23 | 1.28 |
| S527 | 31.17 | 32.17 | 1 | 0.03 | 1.26 | 1.30 |
| S527 | 32.17 | 33.17 | 1 | 0.06 | 0.62 | 0.68 |
| S527 | 33.17 | 34.17 | 1 | 0.18 | 1.65 | 1.83 |
| S527 | 34.17 | 35.17 | 1 | 0.19 | 1.67 | 1.86 |
| S527 | 35.17 | 36.17 | 1 | 6.27 | 4.74 | 11.01 |
| S527 | 36.17 | 37.17 | 1 | 0.56 | 3.79 | 4.35 |
| S527 | 37.17 | 38.17 | 1 | 0.01 | 2.83 | 2.85 |
| S527 | 38.17 | 39.17 | 1 | 0.00 | 1.89 | 1.89 |
| S527 | 39.17 | 40.17 | 1 | 0.02 | 2.05 | 2.07 |
| S527 | 40.17 | 41.17 | 1 | 0.02 | 1.79 | 1.81 |
| S527 | 41.17 | 42.17 | 1 | 0.00 | 0.81 | 0.81 |
| S527 | 42.17 | 43.17 | 1 | 0.00 | 0.66 | 0.66 |
| S527 | 43.17 | 44.17 | 1 | 0.00 | 0.53 | 0.53 |
| S527 | 44.17 | 45.17 | 1 | 0.00 | 2.53 | 2.53 |
| S527 | 45.17 | 46.17 | 1 | 0.00 | 2.21 | 2.21 |
| S527 | 46.17 | 47.17 | 1 | 0.00 | 1.22 | 1.22 |
| S527 | 47.17 | 48.17 | 1 | 0.00 | 0.21 | 0.21 |
| S527 | 48.17 | 49.17 | 1 | 0.00 | 0.36 | 0.36 |
| GGR018 | 59.65 | 60.65 | 1 | 3.00 | 8.42 | 11.42 |
| GGR022 | 61.29 | 62.29 | 1 | 0.01 | 0.54 | 0.55 |
| GGR024 | 72.12 | 73.12 | 1 | 0.17 | 0.08 | 0.25 |
| GGR025A | 120.21 | 121.21 | 1 | 2.83 | 0.01 | 2.84 |
| GGR026 | 82.34 | 83.34 | 1 | 0.17 | 0.52 | 0.69 |
| GGR027 | 48.1 | 49.1 | 1 | 0.62 | 0.13 | 0.75 |
| GGR032 | 94.8 | 95.8 | 1 | 1.40 | 0.01 | 1.41 |
| GGR036 | 49.94 | 50.94 | 1 | 0.32 | 0.01 | 0.59 |
| GGR039A | 98.54 | 99.54 | 1 | 1.35 | 0.02 | 1.37 |
| GGR040 | 79.55 | 80.55 | 1 | 0.57 | 0.44 | 1.01 |
| GGR079 | 33.37 | 34.37 | 1 | 1.27 | 1.00 | 2.27 |
| GGR102 | 99.31 | 100.31 | 1 | 0.10 | 0.03 | 0.14 |
| GGR125 | 64.2 | 65.2 | 1 | 1.47 | 0.53 | 2.00 |
| GGR130 | 60.62 | 61.62 | 1 | 0.29 | 0.33 | 0.76 |
| GGR133 | 56.18 | 57.18 | 1 | 0.29 | 0.41 | 0.70 |
| GGR169 | 58.63 | 59.63 | 1 | 0.01 | 0.41 | 0.42 |
| GGR169 | 60.63 | 61.63 | 1 | 0.23 | 3.10 | 3.40 |
| GGR170 | 28.53 | 29.53 | 1 | 0.30 | 0.25 | 0.50 |
| GGR170 GGR172 | 33.82 | 34.82 | 1 | 2.31 | 2.03 | 4.34 |
| GGR172 GGR173 | 44.61 | 45.61 | 1 | 0.20 | 0.42 | 0.62 |
| GGR173 | 85.55 | 86.55 | 1 | 0.20 | 0.42 | 0.61 |
| GGR178 | 58.45 | 59.45 | 1 | 0.10 | 0.43 | 0.81 |
| GGR179 | 59.75 | 60.75 | | 0.50 | 0.44 | 0.92 |
| GGR179 GGR181 | 56.97 | 57.97 | 1 | 0.41 | 0.19 | |
| | | | | 0.67 | | 0.86 |
| GGR182 | 62.36 | 63.36 | 1 | | 0.55 | 1.11 |
| GGR183 | 63.23 | 64.23 | 1 | 0.98 | 0.27 | 1.25 |
| GGR191 | 52.87 | 53.87 | 1 | 0.01 | 0.41 | 0.42 |

ACADIAN MINING CORP.

Table A-2: Getty Resource Estimate - December 2007 Listing of 1 Meter Assay Composites

| Hole ID | From (m) | To (m) | Length (m) | Pb % | Zn % | Pb % + Zn % |
|---------|----------|--------|------------|------|------|-------------|
| GGR208 | 105.37 | 106.37 | 1 | 2.10 | 0.65 | 2.75 |
| GGR214 | 67.72 | 68.72 | 1 | 0.27 | 0.95 | 1.22 |
| GGR215 | 68.47 | 69.47 | 1 | 3.45 | 1.48 | 4.93 |
| S527 | 49.17 | 50.17 | 1 | 0.00 | 0.46 | 0.46 |

ACADIAN MINING CORP.

Table A-3: Getty Resource Estimate - December 2007

Nearest Neighbour Drill Hole Intercepts Sorted By - Length (m) x (Zn% +Pb%) Factor

| Hole Id | From (m) | To (m) | Length (m) | Zn (%) | Pb (%) | Zn % + Pb % | Length (m) x (Zn% + Pb%) |
|------------------|----------|--------|----------------|--------|--------|-------------|--------------------------|
| GGR018 | 87.50 | 90.50 | 3.00 | 1.22 | 0.11 | 1.33 | 3.99 |
| GGR019 | 91.80 | 95.06 | 3.26 | 0.22 | 1.21 | 1.43 | 4.66 |
| GGR172 | 58.83 | 61.83 | 3.00 | 0.22 | 1.67 | 1.68 | 5.04 |
| GGR172 GGR231 | 78.03 | 82.78 | 4.75 | 0.70 | 0.67 | 1.37 | 6.51 |
| S527 | 17.53 | 28.86 | 11.33 | 0.70 | 0.07 | 0.68 | 7.70 |
| GGR221 | 94.31 | 99.61 | 5.30 | 0.47 | 0.69 | 1.51 | 8.00 |
| | 122.71 | | | | | 2.87 | |
| GGR022 | | 125.71 | 3.00 | 0.01 | 2.86 | | 8.61 |
| GGR102 | 22.86 | 29.32 | 6.46 | 0.45 | 0.99 | 1.44 | 9.30 |
| GGR124 | 71.55 | 79.76 | 8.21 | 0.56 | 0.61 | 1.17 | 9.61 |
| GGR113A | | 68.03 | 6.31 | 1.32 | 0.25 | 1.57 | 9.91 |
| | 23.10 | 29.90 | 6.80 | 0.56 | 0.90 | 1.46 | 9.93 |
| GGR025A | | 33.53 | 6.16 | 0.77 | 1.08 | 1.85 | 11.40 |
| GGR039A | | 43.13 | 7.74 | 1.28 | 0.31 | 1.59 | 12.31 |
| GGR182 | 71.69 | 81.20 | 9.51 | 0.79 | 0.64 | 1.43 | 13.60 |
| GGR230 | 26.82 | 38.53 | 11.71 | 1.11 | 0.09 | 1.20 | 14.05 |
| GGR220 | 39.94 | 50.00 | 10.06 | 0.53 | 0.87 | 1.40 | 14.08 |
| GGR222 | 26.82 | 35.66 | 8.84 | 0.46 | 1.18 | 1.64 | 14.50 |
| GGR177 | 32.61 | 44.81 | 12.20 | 0.55 | 0.72 | 1.27 | 15.49 |
| GGR040 | 28.35 | 41.03 | 12.68 | 0.52 | 0.83 | 1.35 | 17.12 |
| GGR026 | 56.65 | 59.70 | 3.05 | 5.18 | 1.00 | 6.18 | 18.85 |
| GGR116 | 44.10 | 60.96 | 16.86 | 0.94 | 0.18 | 1.12 | 18.88 |
| GGR179 | 28.32 | 41.15 | 12.83 | 0.45 | 1.07 | 1.52 | 19.50 |
| GGR021 | 42.06 | 49.68 | 7.62 | 2.29 | 0.56 | 2.85 | 21.72 |
| GGR037 | 35.97 | 57.30 | 21.33 | 0.49 | 0.56 | 1.05 | 22.40 |
| GGR215 | 26.00 | 38.77 | 12.77 | 0.59 | 1.20 | 1.79 | 22.86 |
| GGR032 | 70.12 | 73.12 | 3.00 | 2.85 | 4.87 | 7.72 | 23.16 |
| GGR158 | 65.53 | 81.47 | 15.94 | 0.56 | 0.91 | 1.47 | 23.43 |
| GGR038 | 65.47 | 68.64 | 3.17 | 2.25 | 5.17 | 7.42 | 23.52 |
| GGR036 | 27.58 | 62.48 | 34.90 | 0.63 | 0.05 | 0.68 | 23.73 |
| GGR094 | 22.56 | 48.25 | 25.69 | 0.86 | 0.07 | 0.93 | 23.89 |
| GGR024 | 26.82 | 34.14 | 7.32 | 1.36 | 2.05 | 3.41 | 24.96 |
| GGR093 | 31.10 | 48.45 | 17.35 | 0.74 | 0.77 | 1.51 | 26.20 |
| | 43.29 | 61.59 | 18.30 | 1.21 | 0.24 | 1.45 | 26.54 |
| GGR079 | 29.87 | 53.04 | 23.17 | 1.06 | 0.15 | 1.21 | 28.04 |
| S526 | 80.07 | 87.48 | 7.41 | 2.23 | 1.62 | 3.85 | 28.53 |
| GGR209 | 109.73 | 119.48 | 9.75 | 1.33 | 1.68 | 3.01 | 29.35 |
| GGR130 | 27.44 | 49.85 | 22.41 | 1.06 | 0.26 | 1.32 | 29.58 |
| GGR183 | 21.52 | 38.16 | 16.64 | 1.53 | 0.26 | 1.79 | 29.79 |
| GGR103 | 32.25 | 54.25 | 22.00 | 1.11 | 0.28 | 1.39 | 30.58 |
| GGR170 | 30.18 | 56.39 | 26.21 | 1.17 | 0.02 | 1.19 | 31.19 |
| GGR170 | 36.58 | 64.31 | 27.73 | 0.57 | 0.58 | 1.15 | 31.89 |
| | 65.44 | 85.95 | | 1.17 | 0.46 | 1.63 | 33.43 |
| GGR211 GGR167 | | | 20.51 13.75 | | | | |
| | 25.45 | 39.20 | | 0.58 | 2.08 | 2.66 | 36.58 |
| GGR206 | 71.34 | 82.62 | 11.28 | 1.80 | 1.49 | 3.29 | 37.11 |
| | 40.36 | 62.64 | 22.28 | 1.22 | 0.63 | 1.85 | 41.22 |
| GGR035A | | 83.51 | 36.86 | 0.82 | 0.32 | 1.14 | 42.02 |
| GGR166 | 36.21 | 66.20 | 29.99 | 1.28 | 0.24 | 1.52 | 45.58 |
| | 41.45 | 58.67 | 17.22 | 1.40 | 1.37 | 2.77 | 47.70 |
| GGR136 | 40.75 | 60.05 | 19.30 | 1.48 | 1.08 | 2.56 | 49.41 |

ACADIAN MINING CORP.

Table A-3: Getty Resource Estimate - December 2007

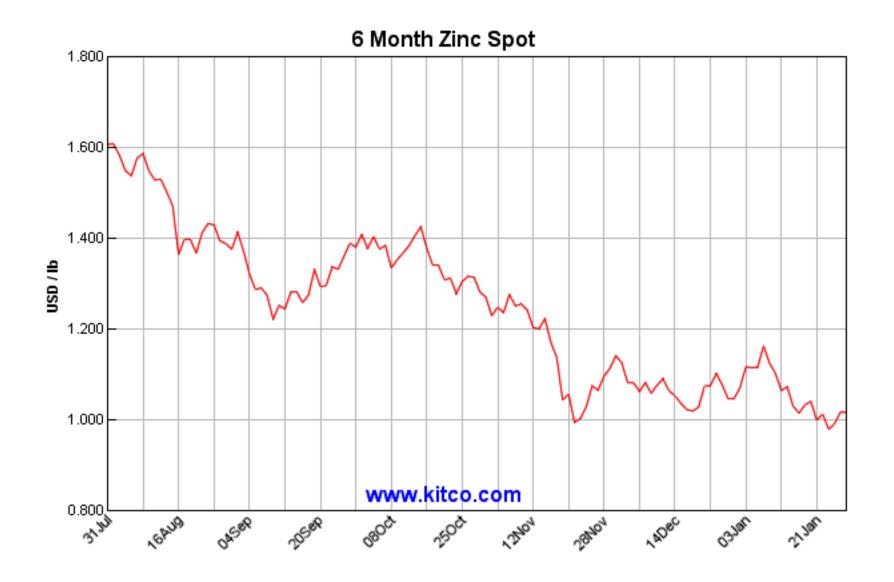
Nearest Neighbour Drill Hole Intercepts Sorted By - Length (m) x (Zn% +Pb%) Factor

| | | _ , , | | 7 (0() | DI (0() | 7 0/ - DI 0/ | |
|---------|----------|--------|------------|--------|---------|--------------|--------------------------|
| Hole Id | From (m) | | Length (m) | Zn (%) | Pb (%) | Zn % + Pb % | Length (m) x (Zn% + Pb%) |
| GGR157 | 30.54 | 65.23 | 34.69 | 1.06 | 0.37 | 1.43 | 49.61 |
| GGR219 | 46.63 | 60.78 | 14.15 | 0.47 | 3.10 | 3.57 | 50.52 |
| GGR214 | 44.20 | 64.31 | 20.11 | 1.57 | 0.95 | 2.52 | 50.68 |
| GGR126 | 120.21 | 130.18 | 9.97 | 0.09 | 5.15 | 5.24 | 52.24 |
| GGR169 | 39.62 | 60.66 | 21.04 | 1.43 | 1.16 | 2.59 | 54.49 |
| GGR181 | 25.00 | 58.54 | 33.54 | 1.42 | 0.28 | 1.70 | 57.02 |
| GGR081 | 20.17 | 49.24 | 29.07 | 1.71 | 0.30 | 2.01 | 58.43 |
| GGR208 | 98.37 | 105.70 | 7.33 | 2.67 | 5.36 | 8.03 | 58.86 |
| GGR213 | 45.16 | 61.62 | 16.46 | 3.10 | 0.97 | 4.07 | 66.99 |
| GGR176 | 39.94 | 60.76 | 20.82 | 1.52 | 1.89 | 3.41 | 71.00 |
| GGR191 | 29.50 | 63.40 | 33.90 | 1.86 | 0.27 | 2.13 | 72.21 |
| GGR217 | 18.11 | 45.72 | 27.61 | 1.35 | 1.40 | 2.75 | 75.93 |
| GGR216 | 96.62 | 121.34 | 24.72 | 1.72 | 1.50 | 3.22 | 79.60 |
| GGR135 | 38.10 | 66.60 | 28.50 | 1.53 | 1.33 | 2.86 | 81.51 |
| GGR096 | 47.55 | 85.65 | 38.10 | 1.04 | 1.16 | 2.20 | 83.82 |
| GGR125 | 58.54 | 98.60 | 40.06 | 0.92 | 1.33 | 2.25 | 90.14 |
| GGR133 | 22.83 | 56.60 | 33.77 | 2.17 | 0.52 | 2.69 | 90.84 |
| GGR129 | 40.23 | 63.40 | 23.17 | 2.21 | 2.07 | 4.28 | 99.17 |

Table A-4: Getty Resource Estimate - 2007 Lithocode Summary

| Lithocode | Primary Rock Description | Primary Modifier | Description | Secondary Modifier | Description |
|-----------|--------------------------|------------------|---------------|--------------------|--------------|
| ОВ | Overburden | GYP | gypsiiferous | LM | Limestone |
| LM | Limestone | MA | massive | DOL | Dolostone |
| DOL | Dolostone | FOL | foliated | GYP | Gypsum |
| GYP | Gypsum | FS | fossiliferous | ANH | Anhydrite |
| ANH | Anhydrite | IMP | impure | G | Greywacke |
| G | Greywacke | BIOT | bioturbated | A | Argillite |
| Α | Argillite | LAM | laminated | VD | Void/Cavity |
| VD | Void/Cavity | ТВ | thin bedded | SS | Sandstone |
| SS | Sandstone | | | SLT | Siltstone |
| SLT | Siltstone | | | MST | Mudstone |
| MST | Mudstone | | | CGL | Conglomerate |
| CGL | Conglomerate | | | | |
| BX | Breccia | | | | |







<u>Sample Preparation Package</u> – PREP-31 Standard Sample Preparation: Dry, Crush, Split and Pulverize

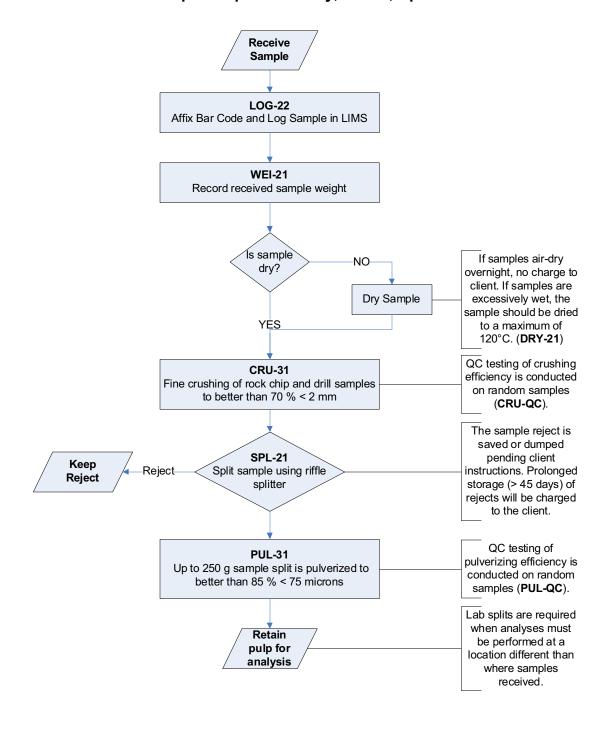
Sample preparation is the most critical step in the entire laboratory operation. The purpose of preparation is to produce a homogeneous analytical subsample that is fully representative of the material submitted to the laboratory.

The sample is logged in the tracking system, weighed, dried and finely crushed to better than 70 % passing a 2 mm (Tyler 9 mesh, US Std. No.10) screen. A split of up to 250 g is taken and pulverized to better than 85 % passing a 75 micron (Tyler 200 mesh, US Std. No. 200) screen. This method is appropriate for rock chip or drill samples.

| Method Code | Description |
|----------------|---|
| LOG-22 | Sample is logged in tracking system and a bar code label is attached. |
| CRU-31 | Fine crushing of rock chip and drill samples to better than 70 % of the sample passing 2 mm. |
| SPL-21 | Split sample using riffle splitter. |
| PUL-31 | A sample split of up to 250 g is pulverized to better than 85 % of the sample passing 75 microns. |



Flow Chart - Sample Preparation Package – PREP-31 Standard Sample Preparation: Dry, Crush, Split and Pulverize





Ore Grade Analysis by XRF - ME-XRF10

Sample Decomposition: 50% Li₂B₄O₇ – 50% LiBO₂ (WEI-GRA06) **Analytical Method**: X-Ray Fluorescence Spectroscopy (XRF)

A calcined or ignited sample (0.9 g) is added to 9.0g of Lithium Borate Flux (50 % - 50 % $\text{Li}_2\text{B}_4\text{O}_7 - \text{LiBO}_2$), mixed well and fused in an auto fluxer between 1050 - 1100°C. A flat molten glass disc is prepared from the resulting melt. This disc is then analysed by X-ray fluorescence spectrometry.

| Element | Symbol | Units | Lower Limit | Upper Limit |
|-----------|--------|-------|----------------|----------------|
| Barium | Ва | % | 0.01 | 50 |
| Niobium | Nb | % | 0.01 | 10 |
| Antimony | Sb | % | 0.01 | 50 |
| Tin | Sn | % | 0.01 | 60 |
| Tantalum | Та | % | 0.01 | 50 |
| Thorium | Th | % | 0.01 | 15 |
| Uranium | U | % | 0.01 | 15 |
| Tungsten | W | % | 0.01 | 50 |
| Zirconium | Zr | % | 0.01 | 50 |



Elements listed below are available upon request

| Element | Symbol | Units | Lower Limit | Upper Limit |
|-----------|--------------------------------|-------|----------------|----------------|
| Iron | Fe ₂ O ₃ | % | 0.01 | 100 |
| Potassium | K ₂ O | % | 0.01 | 100 |
| Magnesium | MgO | % | 0.01 | 100 |
| Sodium | Na ₂ O | % | 0.01 | 100 |



Assay Procedure – ME-OG62 Ore Grade Elements by Four Acid Digestion Using Conventional ICP-AES Analysis

Sample Decomposition: HNO₃-HClO₄-HF-HCl Digestion (ASY-4A01)

Analytical Method: Inductively Coupled Plasma - Atomic Emission Spectroscopy (ICP - AES)*

Assays for the evaluation of ores and high-grade materials are optimized for accuracy and precision at high concentrations. Ultra high concentration samples (> 15 -20%) may require the use of methods such as titrimetric and gravimetric analysis, in order to achieve maximum accuracy.

A prepared sample is digested with nitric, perchloric, hydrofluoric, and hydrochloric acids, and then evaporated to incipient dryness. Hydrochloric acid and de-ionized water is added for further digestion, and the sample is heated for an additional allotted time. The sample is cooled to room temperature and transferred to a volumetric flask (100 mL). The resulting solution is diluted to volume with de-ionized water, homogenized and the solution is analyzed by inductively coupled plasma - atomic emission spectroscopy or by atomic absorption spectrometry.

*NOTE: ICP-AES is the default finish technique for ME-OG62. However, under some conditions and at the discretion of the laboratory an AA finish may be substituted. The certificate will clearly reflect which instrument finish was used.

| Element | Symbol | Units | Lower Limit | Upper Limit |
|----------|--------|-------|----------------|----------------|
| Silver | Ag | ppm | 1 | 1500 |
| Arsenic | As | % | 0.01 | 30 |
| Bismuth | Bi | % | 0.01 | 30 |
| Cadmium | Cd | % | 0.0001 | 10 |
| Cobalt | Со | % | 0.001 | 20 |
| Chromium | Cr | % | 0.002 | 30 |



| Element | Symbol | Units | Lower Limit | Upper Limit |
|------------|--------|-------|----------------|----------------|
| Copper | Cu | % | 0.01 | 40 |
| Iron | Fe | % | 0.01 | 100 |
| Manganese | Mn | % | 0.01 | 50 |
| Molybdenum | Мо | % | 0.001 | 10 |
| Nickel | Ni | % | 0.01 | 30 |
| Lead | Pb | % | 0.01 | 20 |
| Zinc | Zn | % | 0.01 | 30 |

Eastern Analytical Ltd. Preparation and Analytical Procedures

SAMPLE PREPARATION

ROCK/CORE

Samples are organized and labeled when they enter the lab. They are then placed in drying ovens until they are completely dry.

After drying is complete samples are taken and crushed in a Rhino

Jaw Crusher to approximately 75% -10 mesh material.

The complete sample is rifle split until we are left with approximately 250 - 300 grams of material. The remainder of the sample is bagged and stored as coarse reject.

The 250 - 300 gram split is then pulverized using a ring mill to approximately 98% - 150 mesh material.

SOILS/STREAMS/SILTS

Soils are dried at 90°F. They are then pounded with a rubber mallet in the soil bag. Then the soil is screened through a 80 mesh screen. The -80 fraction is rolled and kept as the sample. The +80 mesh fraction is discarded.

ASSAY PROCEDURE FOR CU/PB/ZN/NI/CO

A 0.200g sample is digested in a beaker with 10ml of nitric acid and 5ml of hydrochloric acid for 45 minutes. Samples are then transferred to 100ml volumetric flasks and then analyzed on the AA. Lower detection limit is 0.01%, no upper detection limit.

ASSAY PROCEDURE FOR AG

A 1000mg sample is digested in a 500ml beaker with 10ml of hydrochloric acid and 10ml of nitric acid with the cover left on for 1 hour. Remove the covers and evaporate to a moist paste. Add 25ml of hydrochloric acid and 25ml of deoinized water, heat gently and swirl to dissolve solids. Cool, transfer to 100ml Volumetric and analyze on the AA.Lower detection limit is 0.01oz/t, no upper detection limit.

PROCEDURE FOR AR-ICP30

Each rack is to contain one blank, two CanMet standards and 37 unknowns, of which two will be duplicates.

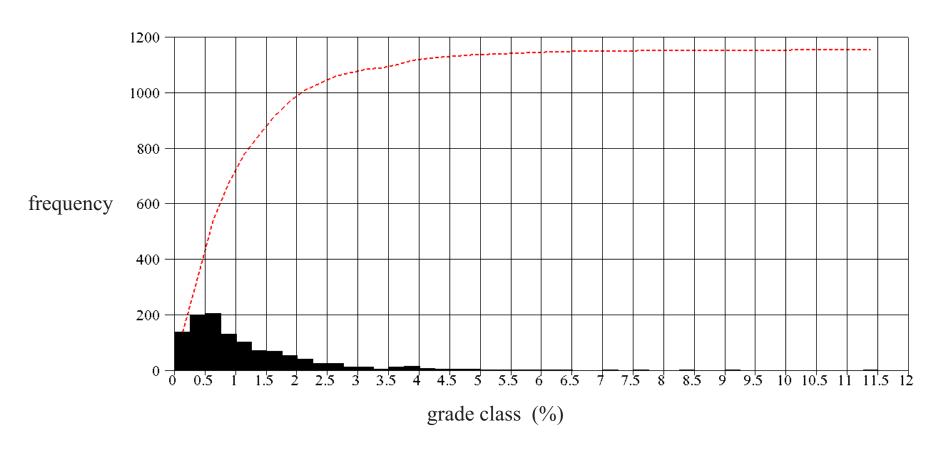
A 0.500 gram sample is digested with 2ml HNO3 in a 95°C water bath for ½ hour, after which 1ml HCL is added and the samples is returned to the water bath for an additional ½ hour. After cooling, samples are diluted to 10ml with deionized water, stirred and let stand for 1 hour to allow precipitate to settle. They are now prepared for ICP analysis.

Updated January 25, 2008

Appendix 3: Resource Estimate Support Documents

Histograms and Cumulative Frequency Plots

Cumulative Frequency of Zn Grade in 1 m Composites



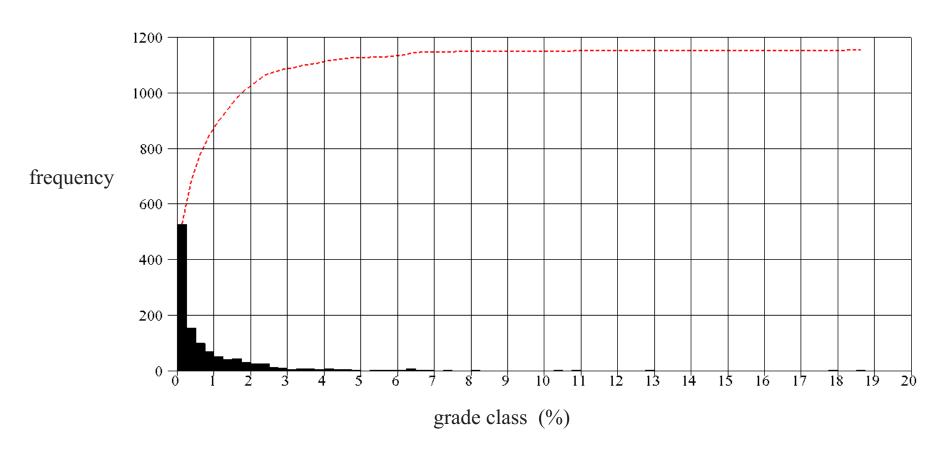
Zn Composite Grade (n=1154)

Probability Plot of Zn Grade in 1 m Composites



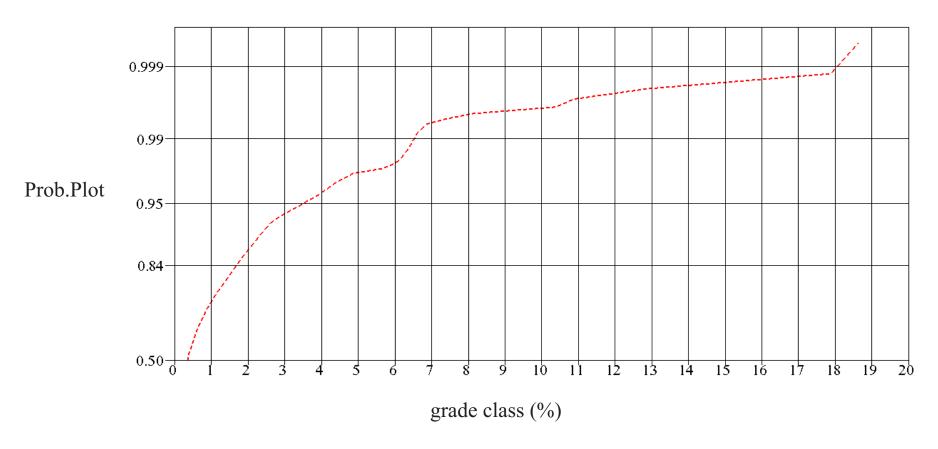
Zn Composite Grade (n=1154)

Cumulative Frequency of Pb Grade in 1 m Composites



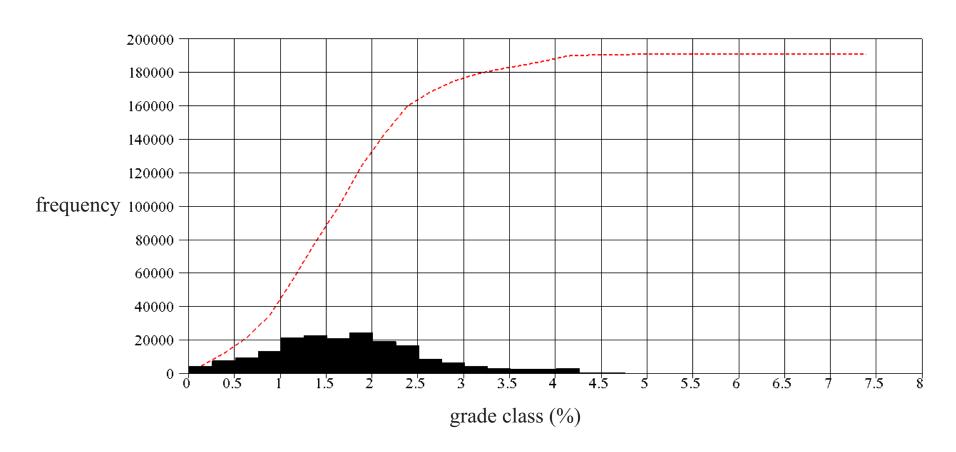
Pb Composite Grade (n=1154)

Probability Plot of Pb Grade in 1 m Composites



Pb Composite Grade (n=1154)

Cumulative Frequency of Zn Block Grades 2% Zn + Pb Minimum Threshold



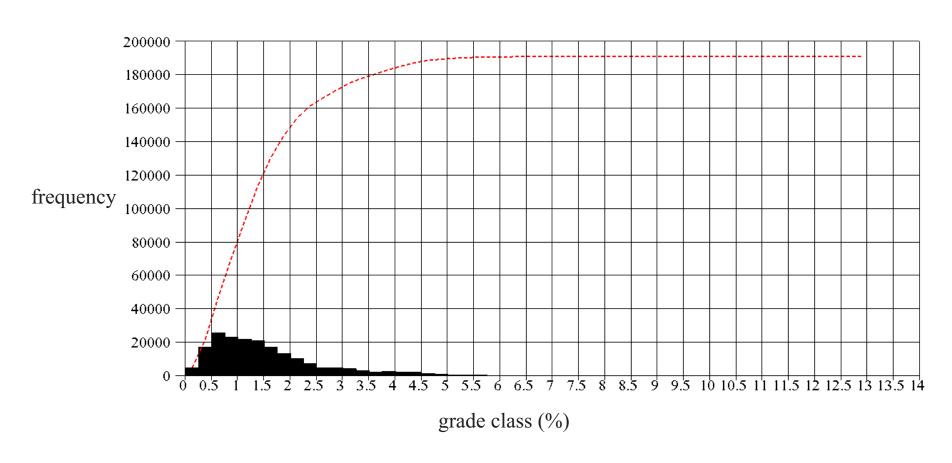
Zn Block Grade (n=190826)

Probability Plot of Zn Block Grades 2% Zn + Pb Minimum Threshold



Zn Block Grade (n=190826)

Cumulative Frequency of Pb Block Grades 2% Zn + Pb Minimum Threshold



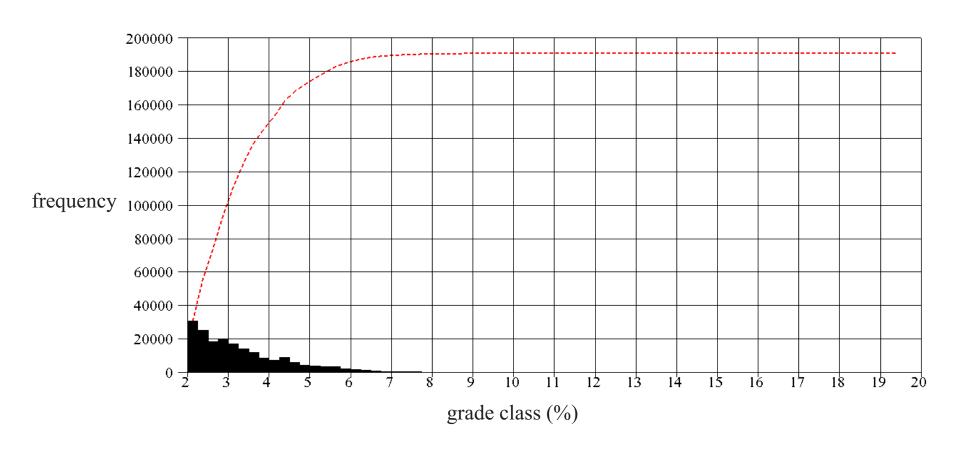
Pb Block Grade (n=190826)

Probability Plot of Pb Block Grades 2% Zn + Pb Minimum Threshold



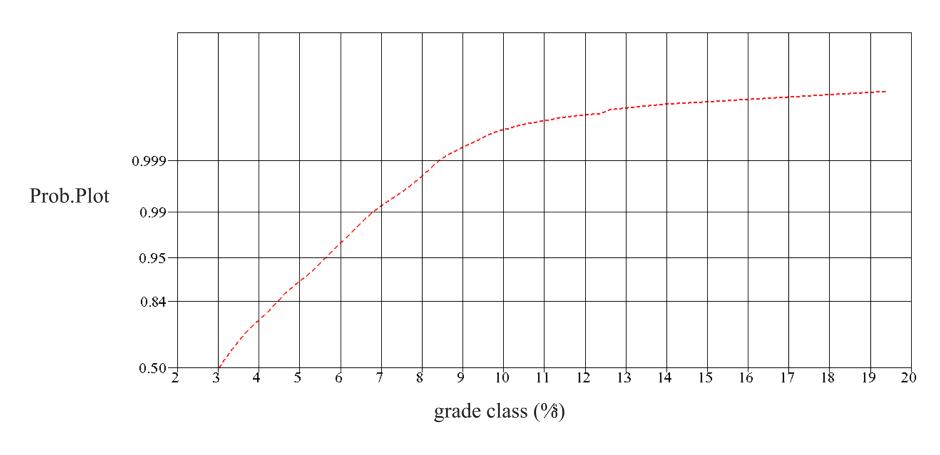
Pb Block Grade (n=190826)

Cumulative Frequency of Zn Equivalent Block Grades 2% Zn + Pb Minimum Threshold



Zn Equivalent Block Grade (n=190826)

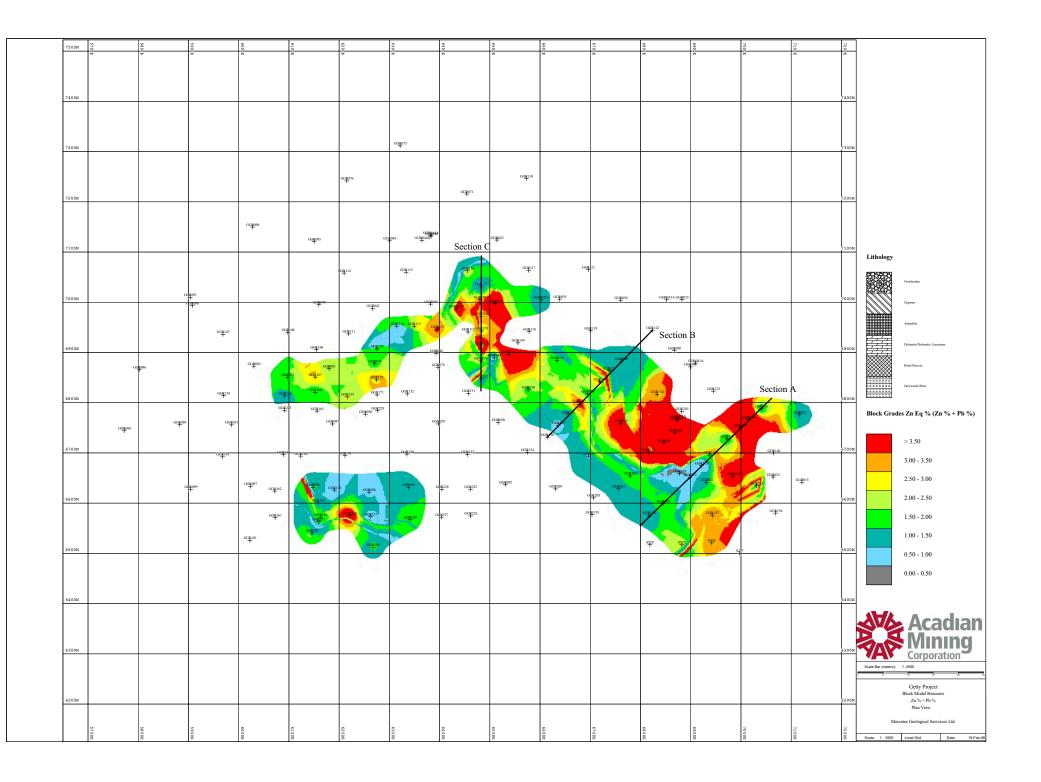
Probability Plot of Zn Equivalent Block Grades 2% Zn + Pb Minimum Threshold

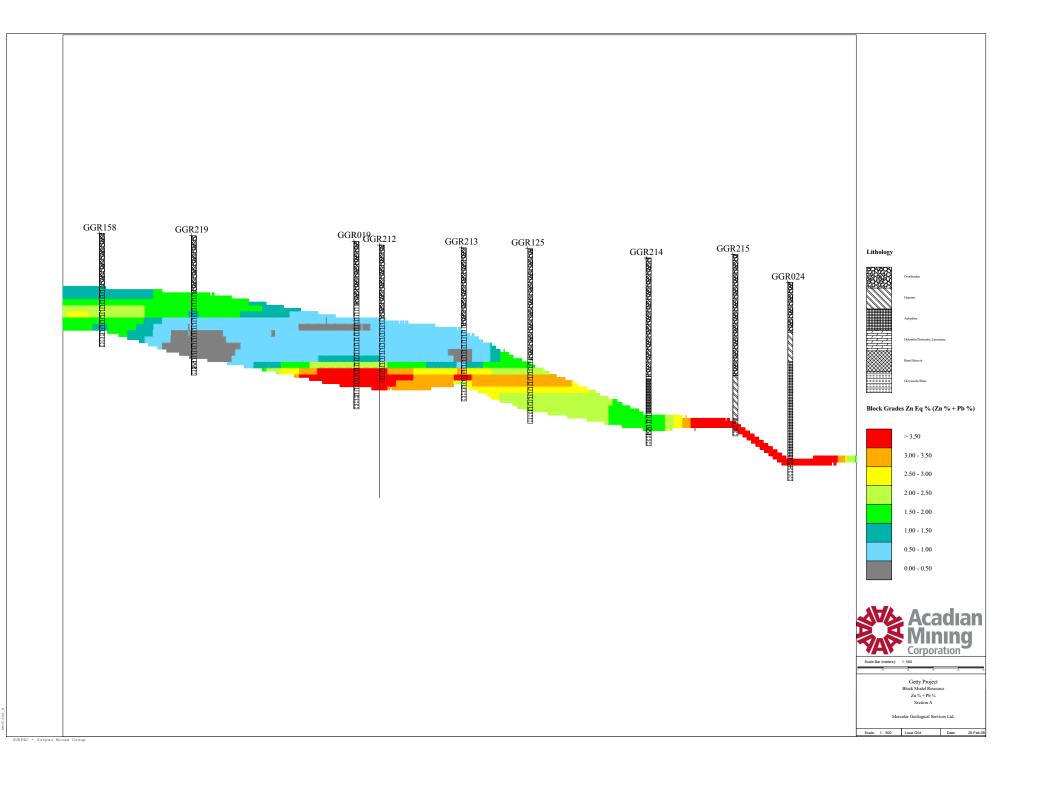


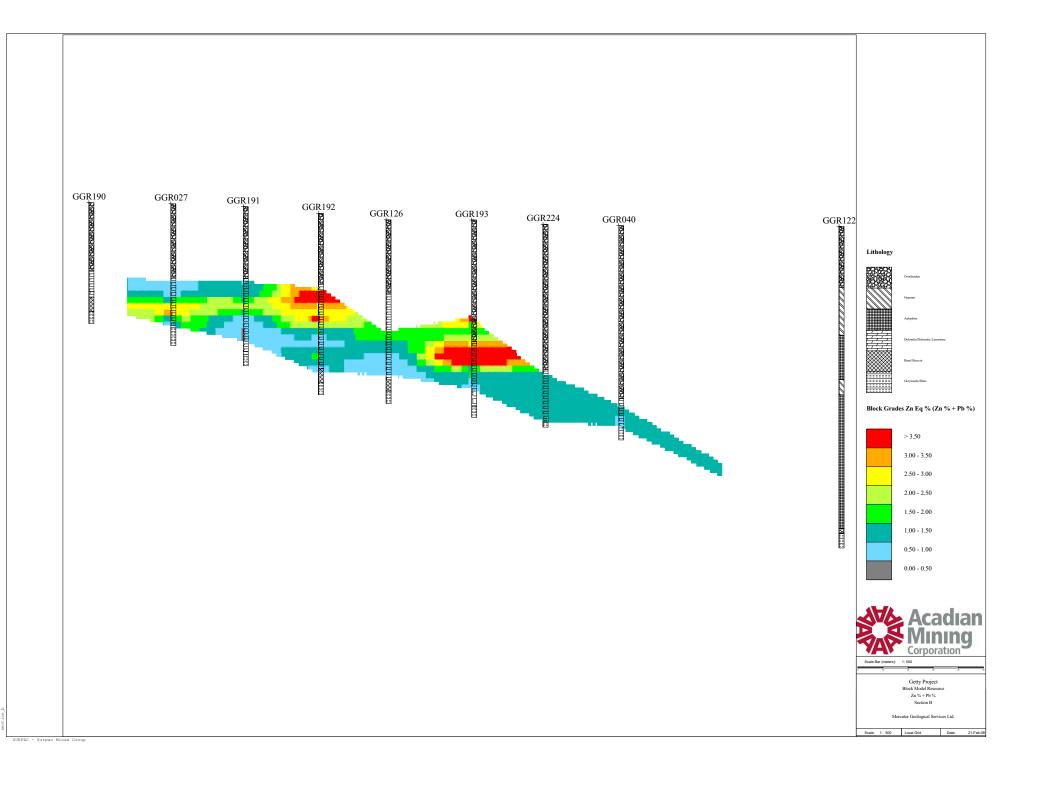
Zn Equivalent Block Grade (n=190826)

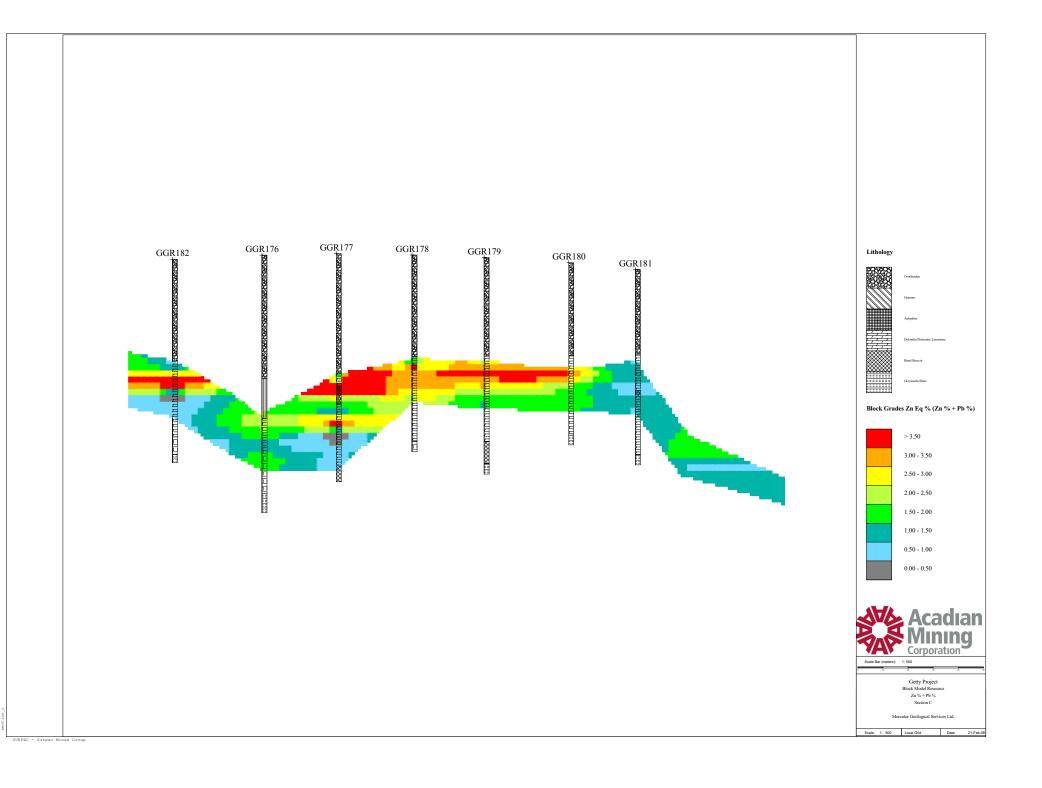
Appendix 4: Resource Estimate Plans and Sections

Block Model Cross Sections and Level Plans
Drill Hole Location Plan









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| 73 | 300N | | | | | | | | | | | | | | | | 7300N | | |
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| 72 | 200N | | | | | | | | | | | | | | | | 7200N | | |
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| | | | | | | GGR095 | GG | GGR0448 R045 GGR044B | 1 | GGR043 | | | | | | | | | |
| 71 | 100N | | | | | | | | | | | | | | | | 7100N | Lithology | |
| | | | | | | | GGR114 | GGR115 | GGR116 | GGR117 | GG | R121 | | | | | | 1595/595) | |
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| 70 | 000N | | | GGR088 | | -GGR078 | GGR042 | GGR039 | GGR09A | GGR037GC | R035A GGR035 | GGR034 | GGR033A GGR033 | | | | 7000N | Oypum | |
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| 69 | 900N | | | | | GGR168 | GGR173 GGR079 | GGR | 046 | ARGS GGR183 | GGR036 | GGR040 | GGR090 | ATRIANI A | | | 6900N | Dolomite Dolomitic Limotone Basal Rececia | |
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| | | | | GGR138 | GGR | GGR166 | GGR172 GGR135 GGR171 | GGR132 | GGR131 | GGR130 | GG | GGR193 RI ₂ 6 | GGR124 | GGR123 | | | | Greywacke Slate | |
| 68 | 800N | | | Concern | GGR | | GGR229 | | | | GGR192. | | GGR210 | | GGR216 | | 6800N | | |
| | | | GGR089 | GGRO | 81 | GGR08 | 7 | GG | R029 | GGR028 | GGR027 | GGR026 | SGR825A | GG | GGR024 | GGR032 | | Block Grades Zn Eq % (Zn % | + Pb % |
| | | GGR080 | | | | | | | | | GGR190 | | GGR209 GGR208 | GGR214 | | | | > 3.50 | |
| 67 | 700N | | | GGR145 | | 42—GGR164 | *GGR141 | GGR139 | GGR137 | GGR134 | | R133 | GGR129 | - GGR125- | GGR140 | | 6700N | 3.00 - 3.50 | |
| | | | | | | | | | | | | GGR206 | GGR019 GG | GGR213 | GGR023 | | | | |
| | | | G | KR099 | GGR097 GGR162 | GGR096 GGR1 | 70 GGR094 | GGR093 | GR228 GGR225 | GGR092 | GGR020 | GGR021 | 7 | GGR022 | GGR211 | GGR015 | | 2.50 - 3.00 | |
| 66 | 600N | | | | | GGR230 | | _ | | | | GGR205 | GGR219 | | GGR156 | | 6600N | 2.00 - 2.50 | |
| | | | | | GGR161 | GGR163 GGR231 | GGR169 (GR221 | GGR220 | GR227 GGR226 | | | | GGR158 | GGR157 | GGRIS6 | | | 1.50 - 2.00 | |
| | | | | | GGR101 | GGR 102 | | | | | | | S528 S527 | S526 | | | | 1.00 - 1.50 | |
| 65 | 500N | | | | | | GGR103 | | | | | | | S2 | 77 | | 6500N | 0.50 - 1.00 | |
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| 62 | 200N | | | | 1 | | | | | | | | | | | | 6200N | Block Model Resource Zn % + Pb % Level 510 El | |
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| 7 | 300N | | | | | | | GGR075 | | | | | | | | | 7300N | |
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| 7 | 200N | | | | | | | | GGR071 | | | | | | | | 7200N | |
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| 7 | 100N | | | | | GGR095 | GG | G GBR≜4 4 R045 GGR044B | | GGR043 | | | | | | | 7100N | |
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| | | | | | | | GGR114 | GGR115 | GGR116 | GGR117 | GC | R121 | | | | | | Overbunden |
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| | | | , | GGR088 | | -GGR078 | GGR042 | GGR039 | GGR039A GGR179 | GGR037 | | | | | | | | Gypum |
| | | | | GGR147 | GC | R146 | GGR111 | GGR113A GGR113 GGF | R217 GGR112 GGR178 | GGR118 | G | GR119 | GGR122 | | | | | Anhydrite |
| 6 | 900N | | | | | GGR168 | GGR173 | | GGR17 | GGR184 | | | GGR090 | | | | 6900N | Dolomite/Dolomitic Limestone |
| ľ | | | | | GGR082 | (CONS) | GGR079 | GGR | GGR176 | CKIR038 GGR 183 | GGR036 | GGR040 | | GGR041A R041 | | | | Dolomite Delemite Limestere Basal Reccia |
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| _ | 800N | | | GGR138 | GGR | GGR166 | GGR135 GGR171 | GGR132 | GGR131 | GGR130 | | R126 | GGR124 | GGR123 | | | 6000M | Greywacke/Slate |
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| | | GGR080 | GGR089 | GGR0 | 31 | GGR08 | 1 | | | GGR028 | GGR027 | GGR026 | GGR025A GGR209 | | 2215 | | | |
| 6 | 700N | | | | | | | | | | | | GGR208 GGR129 | GGR214 | GGR140 | | 6700N | > 3.50 |
| ľ | | | | GGR145 | | 42—GGR164 | -GGR141 | | | | GC | R133 | | GGR125- | GGR140 | | | 3.00 - 3.50 |
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| 6 | 600N | | G | KR099 | GGR162 | GGR096 GGR1 | 70 GGR094 | GGR093 | GR228 GGR225 | | GGR020 | GGR021 | (a.) | | | | 6600N | 2.60 - 2.50 |
| | | | | | GGR161 | GGR163 GGR231 | GGR159 GGR221 | (CR220) G | GR227 GGR226 | | | | GGR219 GGR158 | GGR157 | GGR156 | | | |
| | | | | | | GGR231 GGR102 | | | | | | | | | | | | 1.50 - 2.00 |
| 6 | 500N | | | | GGR101 | | GGR103 | | | | | | S527 | S526 | 77 | | 6500N | 1.00 - 1.50 |
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| 7 | 500N | 70 | | 900E | 000 | 1002 | 200E | 300E | 400E | 500E | 6005 | 70 E | 800E | 900E | 000E | 100E | 200E | - | |
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| | | | | | | | | | GGR181 | | | | | | | | | | Overburden |
| 2 | 000N | | G | GR091 | | | | | GGR180 | G | GR035A GGR035 | GGR034 | GGR033A GGR033 | | | | 7000N | | |
| ľ | | | | GGR088 | | GGR078 | GGR042 | - GGR039 | GGE039A | -GGR037 | | | | | | | | | Gypsum |
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| | | | | GGR147 | GG | R146 | GGR111 | GGR113A GGR113 GGF | 1217 GGR112 GGR178 | GGR118 | G | GR119 | GGR122 | | | | | | russ/SERE |
| | | | | | | | Comm | | GGR17 | GGR184 | | | | | | | | | Dolomite/Dolomitic Limestone |
| 6 | 900N | | | | | GGR168 | GOR173 | GGR | 046 | GGR038 GGR183 | GGR036 | | GGR090 | | | | 6900N | | |
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| | | | | | | | GGR172 | * | GGR182 | | | CKIR194 | | | | | | | |
| | | | | | | | | | GGR131 | GGR130 | | R126 | GGR124 | GGR123 | | | | | Greywacke/Slate |
| 6 | 800N | | | GGR138 | GGR | | GGR135 | | OGACI I | | GGR192 | | GGR124 | | | | 6800N | | |
| | 1 | | | | GGR | 23 | | | | | GGR191 | | GGR210 | | GGR216 | GGR032 | | Block Grad | les Zn Eq % (Zn % + Pb %) |
| | | | GGR089 | GGR031 | | | | | | | | GGR026 | SGR025A | | GGR024 R215 | | | | |
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| f | | | | GGR145 | -GGR1 | 42—GGR164 | | | | | GC | R133 | | GGR125 | GGR140 | | 1 | | 3.00 - 3.50 |
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| | | | G | KIKU99 | GGR162 | GGRI | 70 GGR094 | | GGR225 | | | GGR021 | | | | | | | |
| 6 | 600N | | | | | GGR230 | | | - | | | | GGR219 | 7 | | | 6600N | | 2.00 - 2.50 |
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| 1 | | 700E | 300E | 300E |)00E | T00E | 200E | 300E | 100E | 500E | 3000 | 700E | 300E | 300E | 3000 | 100E | 2 0 0 E | Scale: 1: 2500 | Local Grid Date: 19-Fet |
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| 75 | 500N | 570 | 580 | 590 | 600 | 610 | 620 | 630 | 640 | 650 | 660 | 670 | 680 | 969 | 700 | 710 | 720 | | |
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| 72 | 200N | | | | | | | | | | | | | | | | 7200N | | |
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| | | | | | | GGR095 | GG | GGBR44 R045 GGR044B | , | GGR043 | | | | | | | | | |
| 7: | 100N | | | | | | | | | | | | | | | | 7100N | Lithology | |
| | | | | | | | GGR114 | GGR115 | GGR116 | GGR117 | GG | R121 | | | | | | remanenal | |
| | | | | | | | | | GGRESS | | | | | | | | | | verbunden |
| 71 | 000N | | G | GGR088 | | GGR078 | GGR042 | | GGR180 | GGR037GG | R035A GGR035 | GGR034 | GGR033A GGR033 | | | | 7000N | | урыш |
| | | | | | | | | | GGR179 | | | | | | | | | | abvárite |
| | | | | GGR147 | GC | ir 146 | GGR111 | GGR113A GGR113 GGI | 2217 GGR112 GGR178 | | G | GR119 | GGR122 | | | | | | тум нь |
| 6 | 900N | | | | | GGR168 | GGR173 | GGR | GGR17 | GGR184 | | | GGR090 | | | | 6900N | D. B. | olomite Dolomitic Limestone |
| | | GG | R086 | | GGR082 | GGR081 | GGR079 | GG | GGR176 | | GGR036 | GGR040 GGR224 | GG | GR041A R041 | | | | | ssal Breccia |
| | | | | | | | GGR172 | | GGR182 | | | GGR193 | | | | | | | reywacke/Slate |
| 61 | 800N | | | GGR138 | | | | | | | GGI | RI 26 | GGR124 | GGR123 | | | 6800N | | |
| | | | | | | | | | | | | | GGR210 SGR825A | | GGR216 GGR024 | GGR032 | | Block Grades | Zn Eq % (Zn % + Pb % |
| | | GGR080 | GGR089 | GGI | 8031 | | | | | | | Groze | GGR209 | GGR214 | R215 | | | _ | |
| 6" | 700N | | | | CCR | 42 | | | | | | | GGR208 GGR129 | GGR125 | GGR140 | | 6700N | > | 3.50 |
| | | | | GGR145 | | | | | | | GG | RI33 | | GGR213 | | | | 3. | 00 - 3.50 |
| | | | | | GGR097 | GGR0% | | | | | | GGi <mark>ctos</mark> | GGI | GGR022 GGR01 | GGR023 | GGR015 | | 2 | 50 - 3.00 |
| 61 | 600N | | | JK18099 | GGR162 | GGR230 | 70 | | | | | | | | | | 6600N | 2 | 10 - 2.50 |
| | | | | | GGR161 | GGR163 GGR231 | GGR169 GGR221 | GGR220 | | | | | | GGR157 | GGR156 | | | | 50 - 2.00 |
| | | | | | | GGR102 | | | | | | | | | | | | | |
| 6 | 500N | | | | GGR101 | | GGR103 | | | | | | | S526 | | | 6500N | ., | 10 - 1.50 |
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| 63 | 200N | | | | | | | | | | | | | | | | 6200N | | Zn % + Pb % Level 480 El |
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| | | | | | | | GGR111 | GGRH3A GGF | 2 <mark>17 GGR112</mark> | GGR118 | | GR119 | GGR122 | | | | | Anhydrite |
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| 6 | 900N | | | | | | | GGR | 046 | GGR038 | GGR036 | GGR040 | GGR990 | | | | 900N | Dolomic Dolomic Limestene Band Breccia |
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| | | | | GGR138 | | | | | | | | | GGR124 | GGR123 | | | | Creywacke/Slate |
| 6 | 800N | | | | | | | | | | | | GGR210 | | GGR216 | GGR032 | 800N | ck Grades Zn Eq % (Zn % + Pb %) |
| | | GGR080 | GGR089 | GGR03 | 1 | | | | | | | GGR026 | GGR025A GGR209 | | GGR024 | | Bioc | ik Oraucs Zii Eq /0 (Zii /0 + 1 b /0) |
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| 6 | 700N | | | GGR145 | | 42 | | | | | | | GÖRTA | | GGR140 | | 700N | 3.00 - 3.50 |
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| 7 | 7500N | 570 | 5 80 | 590 | 600 | 610 | 620 | 630 | 640 | 550 | 660 | 670 | 680 | 369 | 701 | 710 | 720 | | |
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| 7 | 7100N | | | | | GGR095 | GG | GGBB444 GR045 GGR044B | | GGR043 | | | | | | | 7100N | | |
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| | | | | GGR147 | | | GGR111 | GGR113A GGR | GGR112 | | G | GR119 | GGR122 | | | | | Anhydrite | |
| 6 | 5900N | | | | | | | | | | | | GGR090 | | | | 6900N | Dolomite/Dol | lomitic Limestone |
| | | GG | R086 | | | | | | GGR176 | | | | | | | | | Dolomite Del | |
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| 6 | 5800N | | | GGR138 | | | | | | | | | GGR124 | GGR123 | / 0 | | 6800N | | an. |
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| | | GGR080 | GGR089 | GGR031 | | | | | | | | GGR026 | GGR209 | | 🌓 | | | | |
| 6 | 5700N | | | GGR145 | | | | | | | | | GGR208 GGR129 | | · | | 6700N | > 3.50 | |
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| 6 | 5500N | | | | | | | | | | | | | s | 77 | | 6500N | 0.50 - 1.00 | |
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| | | 5700E | 5800E | 5900E | 5000E | 61 00E | 62 00E | 63 00E | 64 00E | 6500E | 6600E | 6700E | 68 00E | 6900E | 7000E | 7100E | 72 00E | Scale: 1: 2500 Local Grid | |

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| | | | | GGR147 | | | CORTT | | | | | | GGR090 | | | | | Dolomite/Dolomitic Limestone |
| | 6900N | | | | | | | | | | | | GGR090 | | | 69 | 0.01 | |
| | | GG | R086 | | | | | | | | | | • | | | | | Basal Beeccia |
| | | | | GGR138 | | | | | | | | | GGR124 | GGR123 | | | | Greywacke/Slate |
| | 6800N | | | | | | | | | | | | GGR210 | | | iGR032 | Block Gr | ades Zn Eq % (Zn % + Pb %) |
| | | GGR080 | GGR089 | GGR031 | | | | | | | | | SGR025A GGR209 | | | _ | | |
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| ľ | 6700N | | | GGR145 | | | | | | | | | | | | 67 | DON | 3.00 - 3.50 |
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| ľ | 6600N | | | | GGR161 | | | | | | | | | | GGR156 | 66 | DUN | |
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| Γ | 7500N | 570 | 580 | 590 | 600 | 610 | 620 | 630 | 640 | 650 | 660 | 670 | 680 | 690 | 700 | 710 | 720 | | |
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