TECHNICAL REPORT ON AN
MINERAL RESOURCE ESTIMATE

GETTY ZINC - LEAD DEPOSIT
GAYS RIVER AREA
HALIFAX COUNTY, NOVA SCOTIA, CANADA
NTS 11E03B

PREPARED FOR
SELWYN RESOURCES LIMITED

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Summary

This report on the estimation of mineral resources for the Getty zinc-lead deposit, located in central Nova Scotia, Canada, was prepared by Mercator Geological Services Limited (**Mercator**) on behalf of Selwyn Resources Ltd. (**Selwyn**). It updates earlier resource estimates for the deposit prepared by Mercator for Acadian Mining Inc. (**Acadian**) in 2008. The current and previous estimates were prepared in accordance with disclosure requirements set out under National Instrument 43-101 and are considered compliant with Canadian Institute of Mining, Metallurgy and Petroleum Standards for Mineral Resources and Reserves *Definitions and Guidelines (CIM Standards)*. Current terms of reference were established through discussions between Selwyn and Mercator in February 2011, and it was determined that Mercator would validate the previous resource estimate completed in 2008 and update with respect to current and forecasted metal prices. No new work has been completed on the property since the 2008 resource estimate and the body of this report is substantially the same as the SEDAR filed report completed for Acadian in 2008.

The Getty property consists of 62 contiguous mineral claims, approximately 992 ha, held under Mineral Exploration Licence 06959 currently held by ScoZinc Limited (**ScoZinc**), a subsidiary of Acadian.

In mid-February 2011, Selwyn entered into a formal acquisition agreement to purchase all assets of ScoZinc from Acadian, including Licences 06959. The assets include the Scotia Mine, the Getty deposit and 12,256 hectares of mineral claims covering much of the prospective geology in the Shubenacadie and Musquodoboit sedimentary sub-basins. The acquisition is expected to close in early May 2011.

The purchase price is $10M less any funds paid to the Nova Scotia government related to unpaid mineral taxes on former mine production or any funds needed to top up the reclamation and closure bonds for the Scotia Mine property. Upon completion of the Acquisition, Selwyn will own a 100% interest in the mine-mill complex and an extensive mineral claims package owned by ScoZinc, subject to a mineral royalty to the government of Nova Scotia, and other royalties on certain mineral interests held by ScoZinc. The mineral claims hosting the Getty deposit, as well as certain peripheral mineral claims, are subject to a 1% royalty to Globex Resources Ltd. One half of this royalty can be purchased at any time for a purchase price of $300,000.

The estimation of mineral resources of the Getty deposit is based on 138 drill holes completed by Acadian in 2007 and 2008 and 184 historic drill holes completed during the 1970's by prior operators. Getty Northeast Mines Limited drilled 181 of these historic

drill holes and the remaining 3 drill holes were completed by Imperial Oil Limited. It should be noted that Mercator managed the 2007 and 2008 drilling programs for Acadian and that Quality Control and Quality Assurance protocols included the systematic insertion of independent analytical standards and blanks plus duplicate sample analyses and independent check sample analyses.

The resource estimate is based on a three dimensional block model developed using Gemcom Surpac® Version 6.0.3 software and validated results for 322 diamond drill holes. The model is coordinated to the local grid for the adjacent Scotia Mine and blocks are 2.5 meters x 2.5 meters x 2.5 meters with no sub-blocking. Inverse distance squared (ID2) interpolation methodology utilized 1 meter down-hole assay composites of lead and zinc values within a wire-framed deposit solid containing 26 orientation sub-domains. Grade interpolation was carried out using domain-specific search ellipsoid orientations. Major, semi-major and minor axis ranges for the ellipsoids were 75 meters, 75 meters and 37.5 meters respectively. Included sample range for grade interpolation was from 1 to 12, with no more than 4 samples from a single drill hole. Specific gravity (SG) values for model blocks were calculated from block metal grades using the formula SG = 1 / (Pb% / (86.6 * 7.6) + Zn% / (67.0 * 4.0) + (1 – Pb % / 86.6 – Zn % / 67.0) / 2.82). Zinc Equivalent % (Zn Eq.%) equals Zn % + (Pb % * 1.18) and is based on mill recoveries of 89.3% for zinc and 89.5% for lead, $US1.10/lb Zn and $US1.15/lb Pb metal pricing and smelter returns of 85% for Zn and 95% for Pb. The resource estimate is stated at a 2% Zn Eq. cutoff value that reflects the open pit development potential of this deposit.

Table 1: Mineral Resource Estimate for Getty Deposit- March 2011.

Getty Deposit - Resource Statement - Zn Eq. % * Cut-off					
Resource Category	**Zn Eq. % Cut-off**	**Tonnes (Rounded)**	**Zinc %**	**Lead %**	**Zinc Eq %***
Measured	1.50	1,930,000	1.81	1.26	3.30
Indicated	1.50	3,790,000	1.62	1.21	3.05
Indicated + Measured	***1.50***	***5,720,000***	***1.68***	***1.23***	***3.13***
Inferred	***1.50***	***1,350,000***	***1.52***	***1.31***	***3.06***
Measured	***2.00**	**1,550,000**	**1.97**	**1.45**	**3.68**
Indicated	***2.00**	**2,810,000**	**1.82**	**1.44**	**3.51**
Indicated + Measured	****2.00***	***4,360,000***	***1.87***	***1.44***	***3.57***
Inferred	****2.00***	***960,000***	***1.73***	***1.59***	***3.60***
Measured	2.50	1,180,000	2.14	1.68	4.12
Indicated	2.50	1,950,000	2.06	1.70	4.07
Indicated +	***2.50***	***3,130,000***	***2.09***	***1.69***	***4.09***

Getty Deposit - Resource Statement - Zn Eq. % * Cut-off					
Resource Category	**Zn Eq. % Cut-off**	**Tonnes (Rounded)**	**Zinc %**	**Lead %**	**Zinc Eq %***
Measured					
Inferred	***2.50***	***680,000***	***1.95***	***1.88***	***4.16***
Measured	3.00	860,000	2.34	1.95	4.64
Indicated	3.00	1,300,000	2.35	2.03	4.74
Indicated + Measured	***2.50***	***2,160,000***	***2.35***	***2.00***	***4.70***
Inferred	***3.00***	***460,000***	***2.21***	***2.23***	***4.85***

Notes: *(1) Zinc Equivalent % (Zn Eq.%) = Zn % + (Pb % x 1.18) and is based on mill recoveries of 89.3% for zinc and 89.5% for lead, $US1.10/lb Zn and $US1.15/lb Pb metal pricing and smelter returns of 85% for Zn and 95% for Pb, (2) * denotes the 2.00% Zn Eq. resource statement cutoff value that reflects open pit development potential*

The following recommendations have been provided with respect to further work on the deposit:

1. A preliminary economic study of the deposit should be completed to establish an initial assessment of future development potential.

2. Infill drilling should be carried out in areas of Inferred resources, particularly those present in the southeast half of the deposit, where generally higher metal grades are present. Infill drill hole spacing of at least 50 meters by 50 meters should be developed in such areas to allow upgrading of Inferred resources to Indicated status.

3 A preliminary metallurgical testing program should be carried out on selected core sample reject materials or on new representative drill core samples from the deposit. Results of this work should identify basic processing attributes and provide input data for more advanced assessments of development potential.

A Phase 1 budget of $55,000 and a Phase 2 budget of $660,000 are suggested to complete recommendations outlined above.

1.0 Introduction and Terms of Reference

This report on the estimation of mineral resources for the Getty zinc-lead deposit, located in central Nova Scotia, Canada, was prepared by Mercator Geological Services Limited (**Mercator**) on behalf of Selwyn Resources Ltd. (**Selwyn**). It updates earlier resource estimates for the deposit prepared by Mercator for Acadian Mining Inc. (**Acadian**). The current and previous estimates were prepared in accordance with disclosure requirements set out under National Instrument 43-101 and are considered compliant with Canadian Institute of Mining, Metallurgy and Petroleum Standards for Mineral Resources and Reserves *Definitions and Guidelines (CIM Standards)*. Current terms of reference were established through discussions between Selwyn and Mercator in February 2011, at which time it was determined that Mercator would validate the previous resource estimate completed in 2008 and update with respect to current and forecasted metal prices. No new work has been completed on the property since the 2008 resource estimate and the body of this report is substantially the same as the SEDAR filed report completed for Acadian in 2008.

Historic exploration reports and previous resource estimates pertaining to the property were first compiled by Mercator from records stored at the Scotia Mine facility and from government assessment record archives. This field of information included drill logs with assay information and drill plans completed by Getty Northeast Mines Limited (Getty) and Imperial Oil Limited (Esso) in the 1970's. Mercator also designed and implemented the 2007-2008 diamond drilling program for the Getty deposit, on Acadian's behalf, results of which served to upgrade the deposit database. Mercator was also responsible for database validation, core logging, sampling and quality control/assurance procedures associated with the 2007-2008 drilling program at Getty.

All authors have met with Selwyn staff with respect to the current Getty resource estimate. Authors Kennedy and Cullen visited the property on numerous occasions during the 2007-2008 drilling program and Kennedy visited the property in April 2011 for the purposes of this report. Author Kennedy provided day to day project supervision for the 2007-2008 Acadian drilling program and Cullen, Harrington and Kennedy were responsible, in consultation with Acadian staff, for review and interpretation of data generated by the drilling program.

2.0 Reliance on Other Experts

No other experts were consulted in the preparation of this report.

This report was prepared by Mercator for Selwyn and the information, conclusions and recommendations contained herein are based upon information available to Mercator at the time of report preparation. This includes data made available by Acadian and Selwyn, and from government and public record sources. Information contained in this report is believed reliable but in part the report is based upon information not within Mercator's control. Mercator has no reason, however, to question the quality or validity of data used in this report. Comments and conclusions presented herein reflect Mercator's best judgment at the time of report preparation and are based upon information available at that time. Mercator is not providing a professional opinion with respect to environmental liabilities, surface rights, titles or issues of land ownership.

This report also expresses opinions regarding exploration and development potential for the project, and recommendations for further analysis. These opinions and recommendations are intended to serve as guidance for future development of the property, but should not be construed as a guarantee of success. Mercator is not a Qualified Person with respect to comments on validity of surface rights titles and other issues of land ownership in the province of Nova Scotia.

3.0 Property Description and Location

3.1 General

The Getty deposit is located at Gays River, Halifax County, approximately 45 kilometres northeast of the provincial capital city of Halifax. The area is directly accessible from paved provincial Highway 277 and is approximately 1700 meters northwest of ScoZinc's mill at the Scotia Mine complex (Figures 1 and 2).

The deposit occurs within Exploration Licence 06959 which was issued to Acadian on October 20th, 2006 as a result of tendering by Nova Scotia Department of Natural Resources ("**NSDNR**") and is currently held by ScoZinc, a subsidiary of Acadian. The Getty property consists of 62 contiguous mineral claims, approximately 992 ha, held under Mineral Exploration Licence 06959 that are further described in Table 2.

In 1990 lands covering the deposit were placed under closure by NSDNR (1990, c. 18, s. 22; 1999 (2nd Sess.), c. 12, s. 6.) and these were subsequently opened for staking on

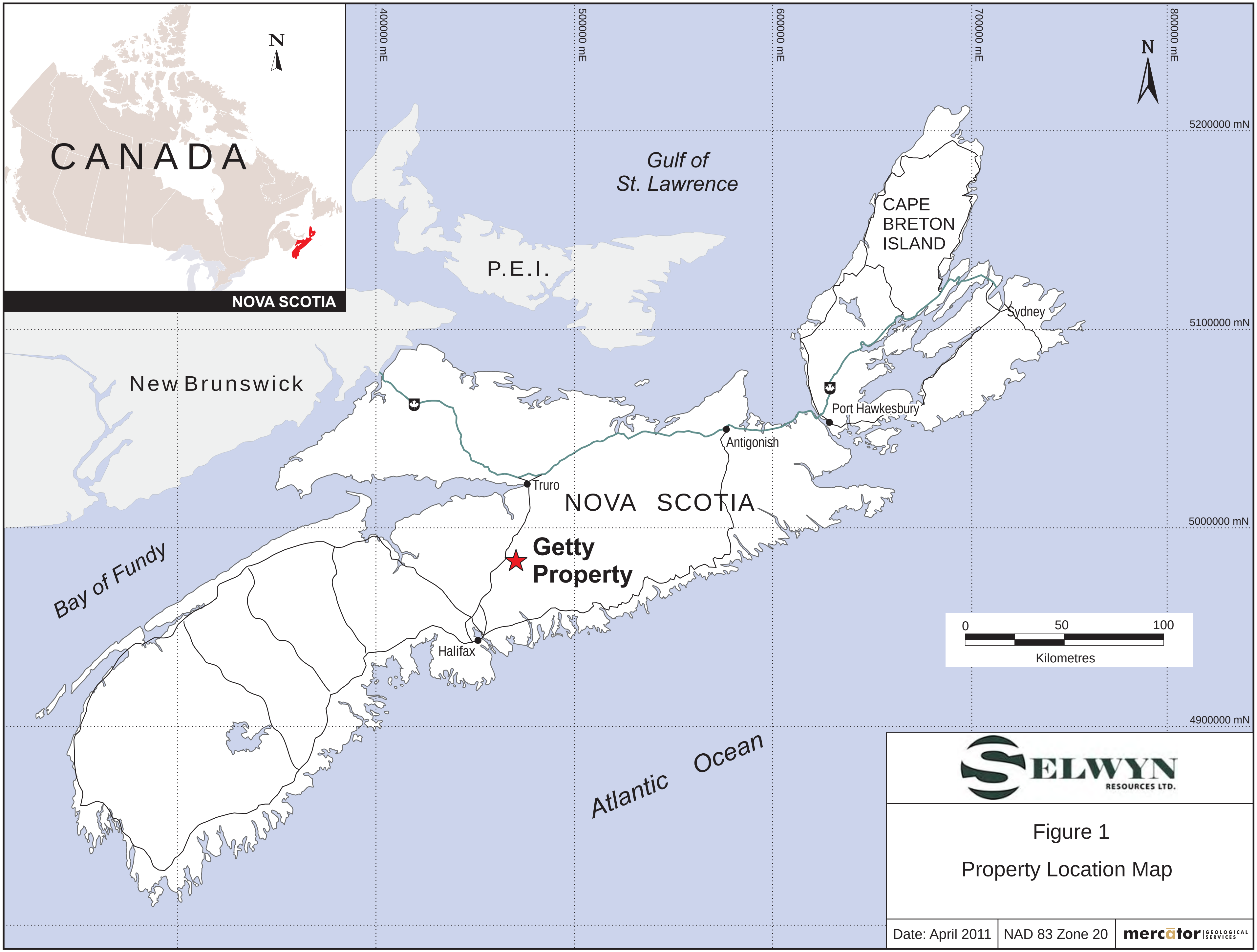


Figure 1

Property Location Map

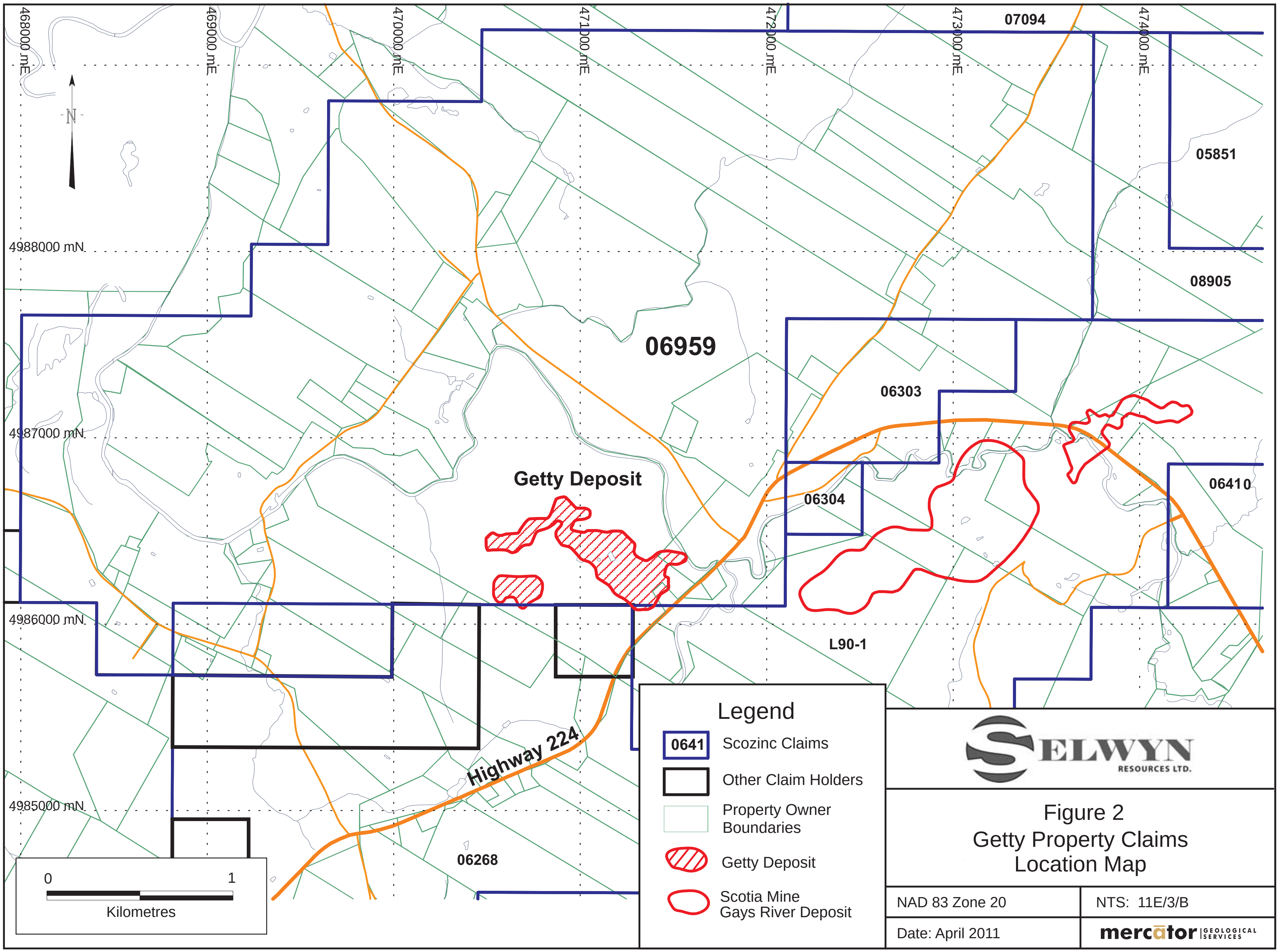


Figure 2
Getty Property Claims
Location Map

September 12th, 2006. Multiple applications for exploration licences covering the deposit were received at that time by the Registrar of Mineral and Petroleum Titles, and all claims were therefore put up for tender under provisions of Section 34 of the Act (1990, c. 18, s. 34.). Acadian submitted the winning bid for this tender and was awarded the exploration licences detailed in Section 3.1, Table 2. Details of bids received and associated work requirements have been deemed confidential by the Minister of Natural Resources.

Table 2: Details of Getty Claim Group

Licence No.	**No. of Claims**	**Claims**	**Tract**	**NTS Map**	**Expiry Date**
06959	62	Q	17	11E3B	20-Oct-2011
		ABCDEFGHJKLMNOPQ	30	11E3B	“
		ABCDEFGHJKLMOPQ	31	11E3B	“
		ABGHJK	32	11E3B	“
		AB	42	11E3B	“
		ABCDEFGHJK	43	11E3B	“
		ABCDEFGHJKLM	44	11E3B	“

At the effective date of this report exploration licences described above were in good standing as represented in records of the Nova Scotia Department of Natural Resources. This assertion does not constitute a legal search of title by Mercator with respect to ownership or status of the licences, but Mercator has no reason to question their status.

Acadian advised Mercator that surface rights to lands covering the Getty deposit are owned under separate titles by Allan Benjamin, David Benjamin and Heather Killen. Mercator did not review the access agreements for purposes of this report but assumes that similar access permission to enter the lands for exploration purposes will be established by Selwyn. The mineral exploration claims and permits currently in place with respect to the Getty project are adequate for execution of technical programs recommended in this report. Permits necessary to do the proposed program will be applied for as required. There is adequate suitable land within the claim area for the recommend work program and future mining activities; however, Selwyn does not hold surface rights to this land. Selwyn will negotiate suitable purchase arrangements when the economic viability of the project has been demonstrated.

3.2 Agreement with Globex Resources Ltd.

Acadian advised Mercator and Selwyn that Licence 06959 that covers the Getty deposit, plus certain peripheral claims in the area, are subject to an agreement between Acadian and Globex Resources Ltd., dated October 10th 2006, that provides Globex with a 1% Net Smelter Return (NSR) royalty interest in the associated claims plus 25,000 common shares of Acadian. Agreement terms also allow Acadian to purchase 50% of the NSR for $300,000 CDN. Mercator did not review or confirm terms of the Acadian-Globex agreement for purposes of this report and has relied upon Acadian and Selwyn for this information.

3.3 Summary of Exploration Title and Regulatory Information

Mineral exploration licences in Nova Scotia are issued under the province's Mineral Resources Act (1990 and as subsequently amended) (the Act) and provide a licencee with exclusive right to explore for specified minerals within the licenced area, subject to terms and conditions of the Act. Individual claims held under a mineral exploration licence measure 16.188 hectares in surface area (~forty acres) and are renewable on a yearly basis. No equivalence to "patented claim status" exists under the Act. Retention of claims in good standing from year to year requires filing of annual renewal fees and documents for each exploration licence as well as meeting minimum yearly work commitment and reporting requirements. Under normal circumstances, fees and minimum work requirements set out under provision of the Act vary according to the year of licence issue and are summarized in Table 3. Payment of cash in lieu of work on a claim or claims can be made once in any five year period.

Table 3: Standard Claims Renewal Fees and Work Requirements

Year of Issue	Renewal Fee	Assessment Expenditure
2 through 10	$10.68 per claim	$200.00 per claim
11 through 15	$21.36 per claim	$400.00 per claim
16 through 25	$85.44 per claim	$800.00 per claim
26 and beyond	$170.88 per claim	$800.00 per claim

An exploration licence conveys an exclusive right to explore for named minerals but does not provide certainty with regard to land access or ownership of minerals. Access to lands is at the discretion of surface title holders and a Mining Lease or Special Mining Lease must be granted by the government to establish ownership of mineral resources for which production is planned. Mining activities can only be initiated after an Environmental Approval has been granted and various permits relating to industrial, environmental and engineering aspects of the proposed mining operation have been obtained. These permits have not been obtained by Acadian or Selwyn for the Getty property.

4.0 Accessibility, Climate, Physiography and Infrastructure

4.1 Accessibility

The property is located at Gays River, Halifax County, approximately 45 kilometres northeast of the provincial capital city of Halifax. The area is directly accessible from paved provincial Highway 277 and is approximately 700 meters northwest of Acadian's Scotia Mine complex (Figure 2). Access to the Trans-Canada Highway (Route 102) is possible at Enfield, approximately 15 kilometres to the west and Robert Stanfield International Airport is located twenty kilometres southwest of the mine site. On the property scale, access to the deposit area is excellent, being provided by several private roads, field access trails and forestry trails associated with land holdings that adjoin Highway 224 (Figure 2).

4.2 Climate

The property is situated in central Nova Scotia where northern temperate zone climatic conditions are present and are moderated by relative proximity to the Atlantic Ocean. Distinct seasonal variations occur, with winter conditions of freezing and potentially substantial snowfall expected from late November through late March. Spring and fall seasons are cool, with frequent periods of rain. Summer conditions can be expected to prevail from late June through early September, with modest rainfall.

The following climate information reported for nearby Robert Stanfield International Airport during the 30 year period ending in 2000 characterizes seasonal precipitation and temperature trends in the area. The average July daily mean temperature for the reporting period was 18.6 degrees Celsius with a corresponding average maximum daily temperature of 23.6 degrees Celsius. Average daily winter temperature for January was minus 6 degrees Celsius with a corresponding average daily minimum being 10.6 degrees. Mean annual temperature is 6.3 ºC, and mean annual precipitation is 1,452.2 mm. Climate conditions permit many exploration activities, such as core drilling and geophysics, to be efficiently carried out on a year-round basis. Other activities, such as geochemical surveys and geological mapping are typically limited by winter snow cover.

4.3 Physiography

Cleared farmland and intervening small woodlots characterize the property area and the north-flowing Gays River follows a prominent valley along the east and north sides of the property. A small north flowing stream also occurs near the west property boundary and lesser seasonal drainages are present locally. Maximum topographic relief is approximately 55 meters above the Gays River valley bottom which has an average elevation in this area of approximately 10 meters above sea level (ASL). Most elevation change occurs along the narrow river valley corridor and rolling farmland with mixed forested areas is otherwise present. Almost all of the area underlain by the resource estimate consists of cleared farmland.

4.4 Infrastructure

The property area is rural and has been extensively development for agricultural purposes in the past. The largest local employers are an open pit gypsum mine and rail shipment facility operated by National Gypsum Limited at nearby Milford, and the Scotia Mine zinc-lead mining operation operated by Acadian on the adjoining property to the southeast. Forestry industry interests are also represented in the immediate area, which occurs entirely within the Halifax Regional Municipality. Access to mainline rail facilities is possible at nearby Enfield and direct access to deep-water shipping facilities with post-Panamax capacity is present through the ice-free deep water port of Halifax. Year-round deep water access is also possible at the port of Sheet Harbour that is accessible via paved provincial highways and located 100 kilometres to the southeast of the Getty property.

Halifax is the provincial capital and in combination with surrounding communities forms a major center of population, government, business, education, industry and transportation services. Robert Stanfield International Airport is located approximately 20 kilometres southwest of the property and provides daily domestic and international airline service. Access to the regional electrical grid is also possible.

In summary, the Getty property is well positioned with respect to existing infrastructure and support services that could be beneficial to future mining at the site. The most significant infrastructure factor is direct proximity to the Scotia Mine complex, located approximately 700 meters to the southeast.

5.0 History

5.1 Introduction

Records of intermittent lead and zinc exploration in the Gays River area date to the late 1800's and the following brief summary of exploration activities reflects information gathered from various assessment and open file reports obtained from the NSDNR archives. This chronological review of exploration history includes investigations that pertain to areas not included within the Getty deposit limits, as described in this report.

These were included to better illustrate character and results of exploration in the surrounding area.

5.2 Summary of Exploration Activities

Pertinent aspects of the area's history of exploration and economic assessment are summarized below and reflect review of assessment report and mineral occurrence file records archived at NSDNR as well as other public record information. Three historic mineral resource estimates are included in the summary and results of these are more fully considered in report Section 5.3.

- First reports of zinc-lead mineralization in the Gays River area date to the late 1800's and from this time until the 1950's exploration consisted of limited amounts of mapping, pitting, trenching and sampling with up to 3% lead values being reported. Most activities focused on the area immediately around the adjacent Scotia Mine site, particularly along the South Gays River, where outcropping Gays River Formation dolomite hosting low grade zinc and lead mineralization was trenched and drilled in the 1950's in the "Gays River Lead Mines Area" (Campbell, 1952). However, with the exception of regional soil geochemical surveying by Penarroya Ltd. in 1964 (Rabinovitch, 1967) that did not identify the Getty deposit, no substantial mineral exploration efforts appear to have been carried out on the current Getty property prior to it's acquisition by Getty in 1972.

- Exploration in the current deposit area was initiated in 1972 by Getty and joint venture partner Skelly Mining Corporation under terms of an option - purchase agreement with Millmore-Rogers Syndicate. The adjoining Gays River property (now Acadian's Scotia Mine) was optioned by Imperial Oil Limited (Esso) and Cuvier Mines Limited (Cuvier) from Millmore-Rogers Syndicate at approximately the same time. The Esso-Cuvier property was immediately investigated by core drilling that ultimately resulted in definition of the Gays River zinc-lead deposit that was placed in production by Esso in 1978. Between 1978 and 1981, 554,000 tonnes of zinc/lead ore was mined with an average grade of 2.12% zinc and 1.36% lead (Roy et. al., 2006). Esso ceased production in 1982 after encountering substantial problems with both mining conditions and water inflows.

- Discovery of the Getty zinc-lead deposit is attributed to drill hole GGR-12 which was completed in 1972 and intersected 4.63 meters of dolomite grading 15.48% combined zinc-lead, beginning at a down hole depth of 93.11 meters. Subsequent completion of over 200 holes by Getty and Imperial on and around the property served to delineate a nearly continuous mineralized zone measuring approximately 1300 meters in length and up to 200 meters in width (Comeau, 1973, 1974; Comeau and Everett, 1975).

- Getty retained MPH Consulting Limited (MPH) to assess three development scenarios for the deposit and Riddell (1976) reported results of this work, which showed that production of 375,000 tonnes per year would be necessary to support a viable, stand-alone open pit operation.

- In 1980 economic aspects of developing the deposit based on an in-house tonnage and grade model were assessed by Esso (MacLeod, 1980). This study concluded that mining through open-pit methods as an ore supplement to the Gays River deposit would be economically viable, provided that important operating assumptions were met. The earlier MPH work was also reviewed at this time and some economic models updated. None of the work indicated that profitable stand-alone development of the deposit could be expected under market conditions of the time. George (1985) subsequently reviewed earlier evaluations and also reached a negative conclusion regarding development potential.

- Claims covering the Getty deposit were placed under closure in 1987 by the Nova Scotia government and a tender was subsequently let for acquisition of exploration rights to the property. In 1990 Westminer Canada Limited (Westminer) was deemed the successful bidder and awarded a Special Exploration Licence for further assessment of the deposit.

- In 1992 Westminer completed a resource estimate and preliminary economic assessment of the deposit based on Getty drilling results, with potential development in conjunction with the adjacent Gays River deposit being considered (Hudgins and Lamb, 1992). Results showed that milling of about 550 tonnes per day of Getty ore could be undertaken at a low cost if excess milling capacity at Gays River was being filled by such material. Westminer also indicated that zinc oxide production from the deposit would result in a substantially better financial return to the mine in comparison with a conventional smelter contract for sulphide concentrates. Attempted renewals of the Getty Special Exploration Licence by Westminer for three consecutive years were not successful.

- Pasminco Resources Canada Company (Pasminco) acquired the adjacent Scotia Mine deposit and infrastructure in 1999 through purchase of Savage Resources Inc., and in 2000 Pasminco submitted an application to NSDNR for a Special Mining Lease covering the deposit. No lease was issued and the closed status of the property was maintained.

- Between 1992 and September 2006 Getty property claims were maintained under government closure and no work was carried out.

- In September, 2006 the provincial government tendered exploration rights to the closed Getty property and Exploration Licences 6959 and 6960 were subsequently issued to Acadian on October 20th, 2006 as successful bidder under the tendering process. In December, 2007 Mercator completed an inferred resource estimate for the property, on behalf of Acadian, which was reported by Cullen et al. (2007) and update by Cullen et al. (2008). Acadian completed a total of 138 new drill holes in support of these estimates.

5.3 Previous Mineral Resource or Reserve Estimates

Four previous estimates of tonnage and grade for in-situ mineralization comprising the Getty deposit are available in the public record. The earliest of these was prepared for Getty by MPH Consulting Limited (Riddell, 1976) and was revised in 1980 as part of a Mine Valuation Study carried out for Esso (MacLeod, 1980). Subsequently, Westminer developed an in-house estimate and preliminary economic assessment of the deposit based on historic drilling (Hudgins and Lamb, 1992). The fourth estimate was completed in December, 2007 by Mercator for Acadian and reported by Cullen et al (2007).

Results of the first three historic estimates are presented below in Table 4a and all pertain to areas currently covered by Acadian exploration licences. These pre-date National Instrument 43-101 (NI 43-101) and have not been classified under Canadian Institute of Mining, Metallurgy and Petroleum Standards for Reporting of Mineral Resources and Reserves: *Definitions and Guidelines* (the CIM standards). On this basis they should not be relied upon. Table 4b presents the Cullen et al. (2007) NI43-101 compliant resource estimate completed by Mercator, which has an effective date of December 12th, 2007.

Table 4a: Historic Resource Estimates for Getty Deposit Not NI 43-101 Compliant

Reference	**Tonnes**	**Zn + Pb %**	**Zn %**	**Pb %**
Riddell(1976)	4,470,400	3.71	1.87	1.84
MacLeod(1980)	3,149,600	2.97	1.60	1.37
Hudgins and Lamb(1992)	4,490,000	3.20	1.87	1.33

Notes: *With regard to the historic mineral resource estimates stated above 1) a qualified person has not done sufficient work to classify the historical estimate as current mineral resources or mineral reserves; 2) the issuer is not treating the historical estimate as current mineral resources or mineral reserves as defined in sections 1.2 and 1.3 of NI43-101; and 3) the historical estimate should not be relied upon.*

Table 4b: Mercator NI 43-101 Compliant Resource Estimate for Getty Deposit Effective December 12th, 2007

Reference	**Tonnes**	**Zn + Pb %**	**Zn %**	**Pb %**
Cullen et al. (2007)	4,160,000	3.21	1.81	1.40

Riddell(1976) used a 2% (zinc% + lead%) cut-off, Macleod (1980) used 1.5% zinc cut-off and Hudgins and Lamb (1992) used a 1.5% zinc-equivalent cut-off defined as zinc equivalent = zinc% +(lead % x 0.60). Figures for the previous Mercator estimate that are presented in Table 4b reflect application of a 2% zinc + lead cut-off. The Riddell (1976) and MacLeod (1980) estimates are based on drill-hole-centered polygonal methods of volume estimation along with subjectively determined specific gravity factors reflecting general experience. Both estimates include length-weighted drill hole grade assignments to polygons with subsequent tonnage-weighting to determine deposit grades. In contrast, Hudgins and Lamb (1992) used Surpac® deposit modeling software, a cross sectional method of volume estimation, a single assigned specific gravity factor of 2.75 g/cm^3 and calculated average deposit zinc and lead grades as the length-weighted averages of all qualifying drill hole intercepts. Further discussion of historic resource estimates plus that by Mercator appears in report section 16.4.

6.0 Geological Setting

Carboniferous age sedimentary sequences in central Nova Scotia occur near the current southern margin of the extensive Maritimes basin, development of which began after the mid-Devonian Acadian Orogeny (Figure 3). Northeast trending faulted sub-basins evolved over much of the current central Nova Scotia area, where sedimentation from latest Devonian through Mississippian time was initially terrigenous clastic in nature, evolving to mixed marine carbonates, evaporites and clastics. Horton Group rocks record the early terrigenous and lacustrine clastic phase of deposition while overlying Windsor Group rocks record multiple transgressive-regressive marine depositional cycles. Pennsylvanian sedimentation marks further evolution of the Maritimes basin to predominance of clastic fluvial /lacustrine or shallow marine clastic conditions (Fralick and Schenk, 1981).

The Getty deposit is hosted by lower Mississippian age dolostone of the Windsor Group's Gays River Formation. Well defined carbonate banks characterize this formation and in most instances are associated with well-defined paleo-basement high features. On depositional basin scale, Gays River Formation bank carbonates and laminated limestone of the laterally equivalent Macumber Formation mark the onset of marine depositional conditions after a prolonged period of predominantly terrigenous clastic sedimentation represented by Horton Group siliciclastic rocks.

Carboniferous strata in Central Nova Scotia occur within the Shubenacadie and Musquodoboit sub-basins of the larger Maritimes basin and were described by Giles and Boehner (1982). Geometry of both sub-basins was significantly influenced by strong northeast trending structural grain in basement sequences of the Cambro-Ordovician Meguma Group. Deformation was heterogeneously distributed across the sub-basins and at present is now represented by northeast trending normal and thrust faults which are locally associated with open to moderately folded structural domains. Deformation features are essentially absent near the southern margins of the basins but become more prevalent and pervasive toward the northern limits, where effects of the regionally significant Cobequid-Chedabucto fault system are represented. Minor faults or fracture zones may be present at Getty but no structural complexity is evident in either the surface morphology or drill logs.

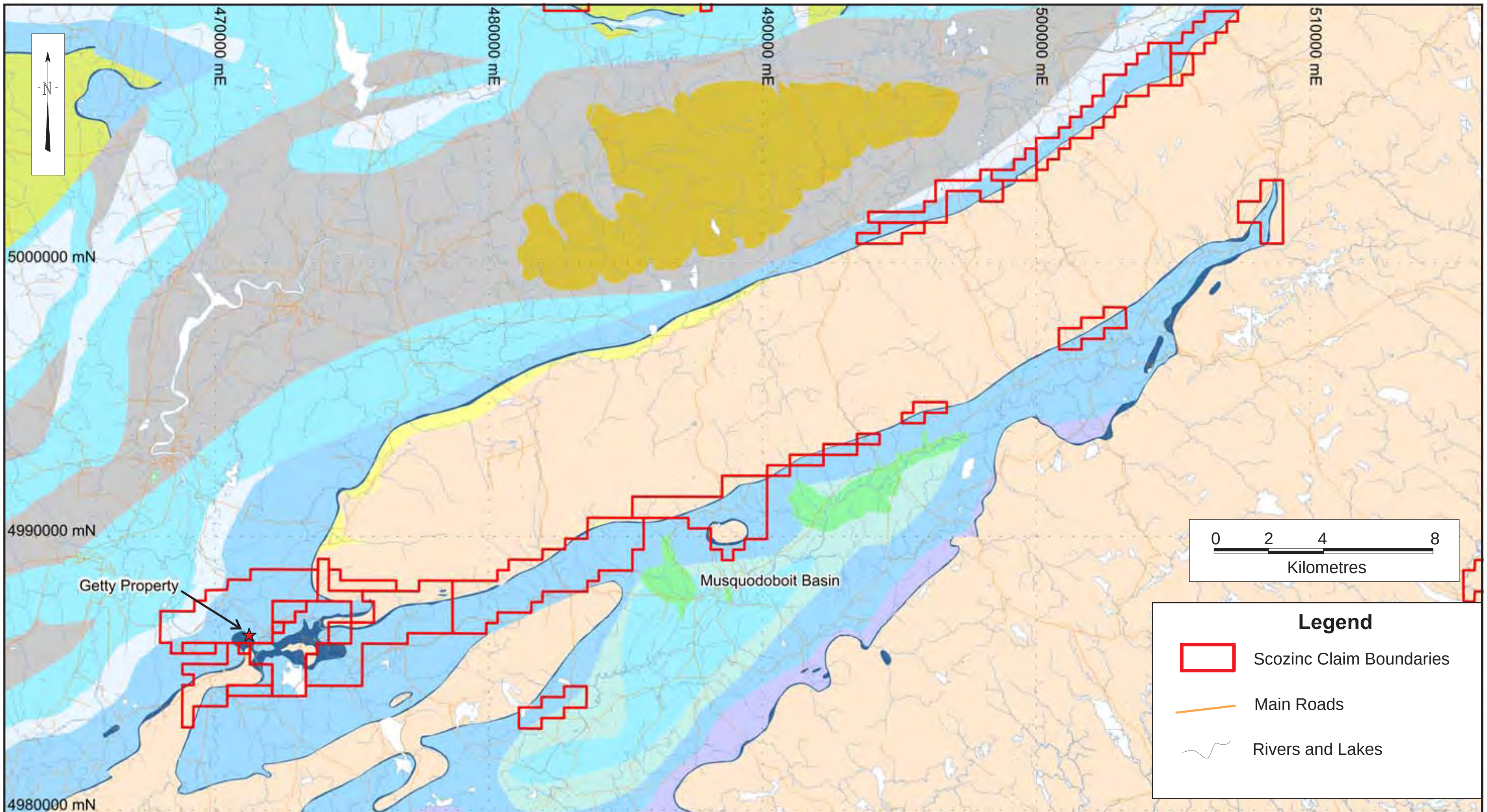
7.0 Deposit Geology

7.1 Stratigraphy

Geology in the Getty deposit area has been interpreted from compiled results of Giles and Boehner (1982) plus results of various mapping and diamond drilling campaigns carried out in the area. The actual deposit does not outcrop, but was delineated by Getty through drilling (eg. Bryant, 1975, Comeau, 1973, 1974; Palmer and Weir, 1988a, b).

As represented in Figure 4, the Getty deposit is hosted by a northwest trending Gays River Formation carbonate bank complex that occurs as a direct extension to the larger, northeast trending carbonate bank that hosts Scotia Mine's zinc lead resources and reserves. Both banks developed along paleo-basement highs comprised of Cambro-Ordovician age Goldenville Formation quartzite and greywacke. At Getty host dolostone ranges in true thickness from less than a meter to a maximum of about 45 meters.

The carbonate host sequence occurs above a thin sedimentary breccia or conglomerate unit comprised predominantly of Goldenville Formation debris with a small carbonate matrix component resting unconformably on Goldenville Formation basement. Carrolls Corner Formation evaporites lie stratigraphically above the Gays River Formation and are comprised locally of gypsum and anhydrite with minor amounts of interbedded dolomitic limestone and siltstone. With possible exception of local clay and sand



Early Cretaceous
Clay, sand, silt and lignite; mappable limits not clearly defined

Scotch Village Formation
Sandstone, red and grey shale, siltstone

Watering Brook Formation
Grey mudstone and shale with intercalated gypsum, anhydrite and halite; evaporites most abundant in lower part of formation

Green Oaks Formation
Maroon to reddish brown siltstone and fine grained sandstone, with intercalated marine limestone and dolostone; with associated anhydrite or gypsum in the Shubenacadie Basin

MacDonald Road Formation
Gypsum, anhydrite and minor halite, with interbeds of grey and maroon siltstone and sheet-like carbonate members; cyclic repetition of these rock units is characteristic

Gays River/ Macumber formations
Dolostone, limestone, thinly bedded, argillaceous + bituminous, locally thickly bedded and fossiliferous in mound-shaped deposits resting upon pre-Carboniferous rocks; laminated and/or banded, peloidal, sparsely fossiliferous

Carrolls Corner Formation
Anhydrite, gypsum, with minor dolostone and mustone in thin beds; includes undifferentiated shale and mudstone breccia with minor gypsum and anhydrite in proximity to the faulted northern margin of the Shubenacadie Basin

Elderbank Formation
Limestone, dolostone, conglomeratic sandstone and grey siltstone; very minor gypsum and anhydrite; cyclic repetition of these rock units is characteristic

Meaghers Grant Formation
Sandstone, siltstone and dark grey locally dolomitic shale; also arenaceous oolitic and stromatolitic dolostone; numerous interbeds of gypsum or anhydrite occur in the transition zone with the Carrolls Corner Formation

Coldstream Formation
Reddish brown polymictic conglomerate and conglomeratic sandstone with minor dark grey shale; known mainly from the subsurface along the southern perimeter of the Shubenacadie Basin

Undivided Horton Bluff and Cheverie Formations
Sandstone conglomeratic sandstone, and minor shale, with a basal cobble conglomerate; includes minor coal in thin beds

Halifax and Goldenville Formations

Note: Geology after Giles & Boehner (1982)

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Figure 3
Regional Geology Map of Getty Deposit

Date: April 2011 | NAD 83 Zone 20 | mercator GEOLOGICAL SERVICES

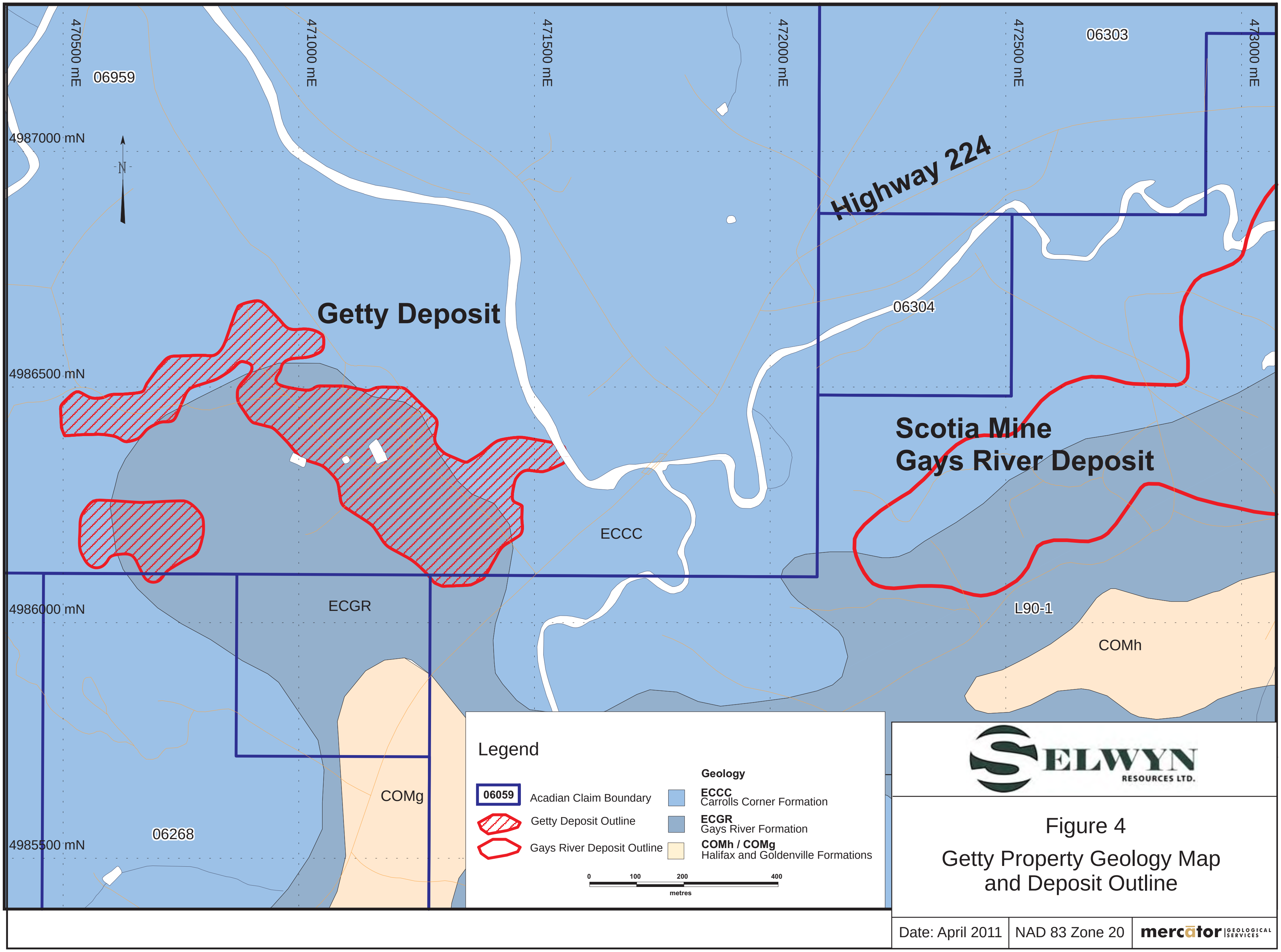

Figure 4
Getty Property Geology Map and Deposit Outline

accumulations of Cretaceous age, Carrolls Corner Formation rocks are the youngest sequences of the local bedrock section. Figure 5 presents a stratigraphic column for the deposit area.

Historical and the current drilling on the Getty property has shown that evaporite cover at the Gays River Formation contact was in many instances preferentially removed by erosion and karst-related solution processes during Cretaceous time, leaving a trough or trench parallel with the carbonate contact in many areas. Stratified Cretaceous fill sedimentary material followed by Quaternary material of glacio-fluvial origin infilled this trough, and is termed "Trench" material on the adjacent Scotia Mine property. Similar material exists in some areas adjacent to the Getty deposit but in many instances is difficult to distinguish from less consolidated overburden material that is of glacial origin.

7.2 Deposit Type

Description

The Getty deposit carbonate bank forms a northwest extension to the adjacent Gays River bank that hosts Scotia Mine zinc-lead resources and reserves. While broadly similar, carbonate bank slopes at Getty are generally gentler than those seen at Gays River. Figure 6 depicts a typical bank cross section illustrating occurrence of thickest carbonate on the bank top, with progressive thinning down dip on the paleo-topographic high. Variations existed locally in basement paleo-slope angles and appear to have directly influenced corresponding carbonate bank morphology. Areas with steep basement slopes tend to show rapid thinning of carbonate away from the thicker bank tops, with correspondingly steep contact surfaces with overlying evaporites. Gentle slope areas show greater lateral and down-dip continuation of thicker carbonate and corresponding lower average contact dips with the overlying evaporite. Based on the drilling carried out to date at Getty, the maximum carbonate thickness encountered along the basement high trend is 45.48 meters in drill hole GGR-221.

Gays River Formation carbonate banks include intricately intercalated algal, peloidal and coraline lithofacies, with abundance of bindstone, bafflestone, packstone and micrite. These facies show transition downdip to thin (typically <5 meters), variably laminated algal/silty carbonates that are lateral equivalents to laminated carbonates of the Macumber Formation. The latter occurs basinward of the underlying Horton Group's stratigraphic pinchout and is not present in the deposit area.

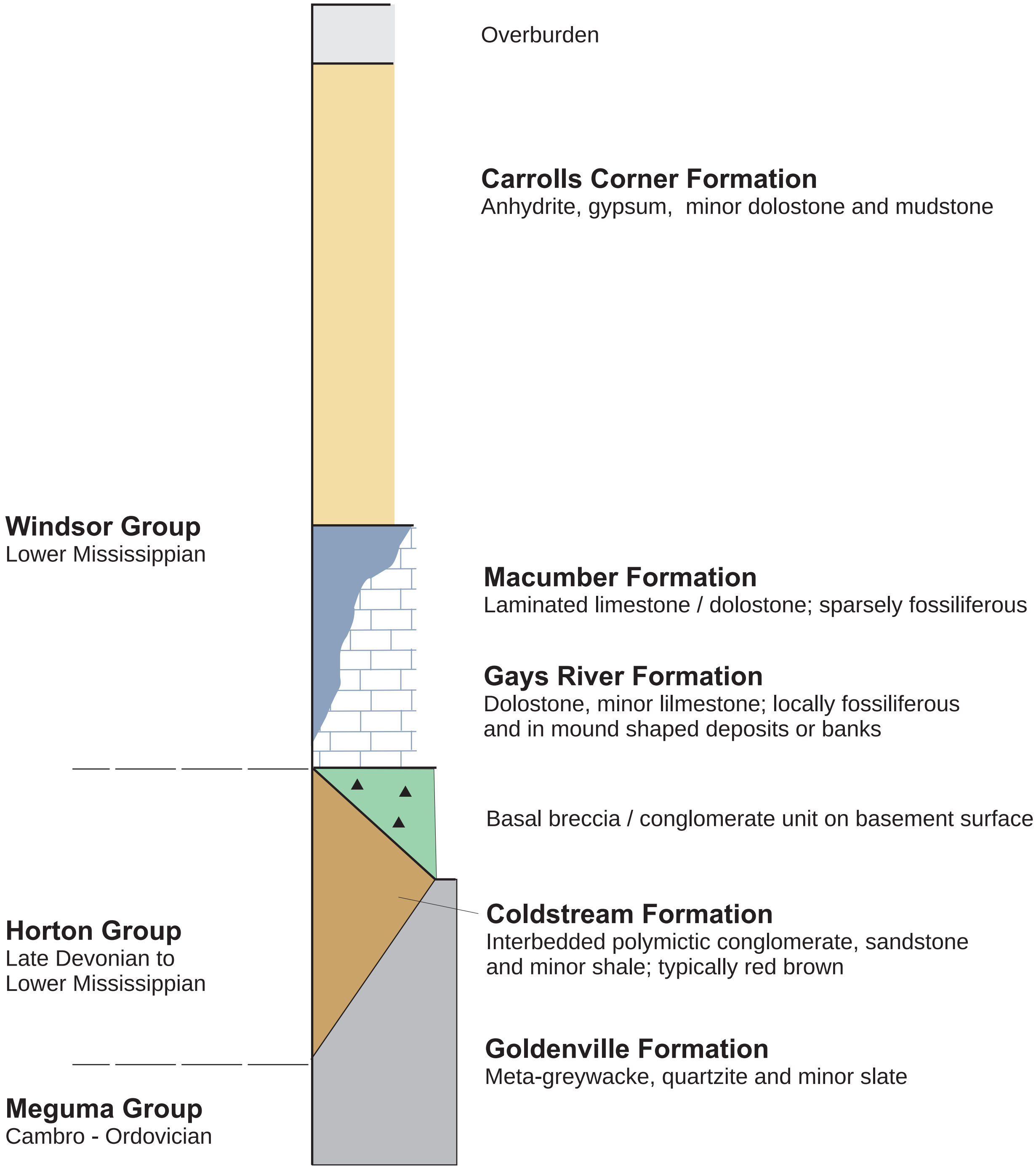

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Figure 5

Stratigraphic Column for Getty Deposit Area

Date: April 2011

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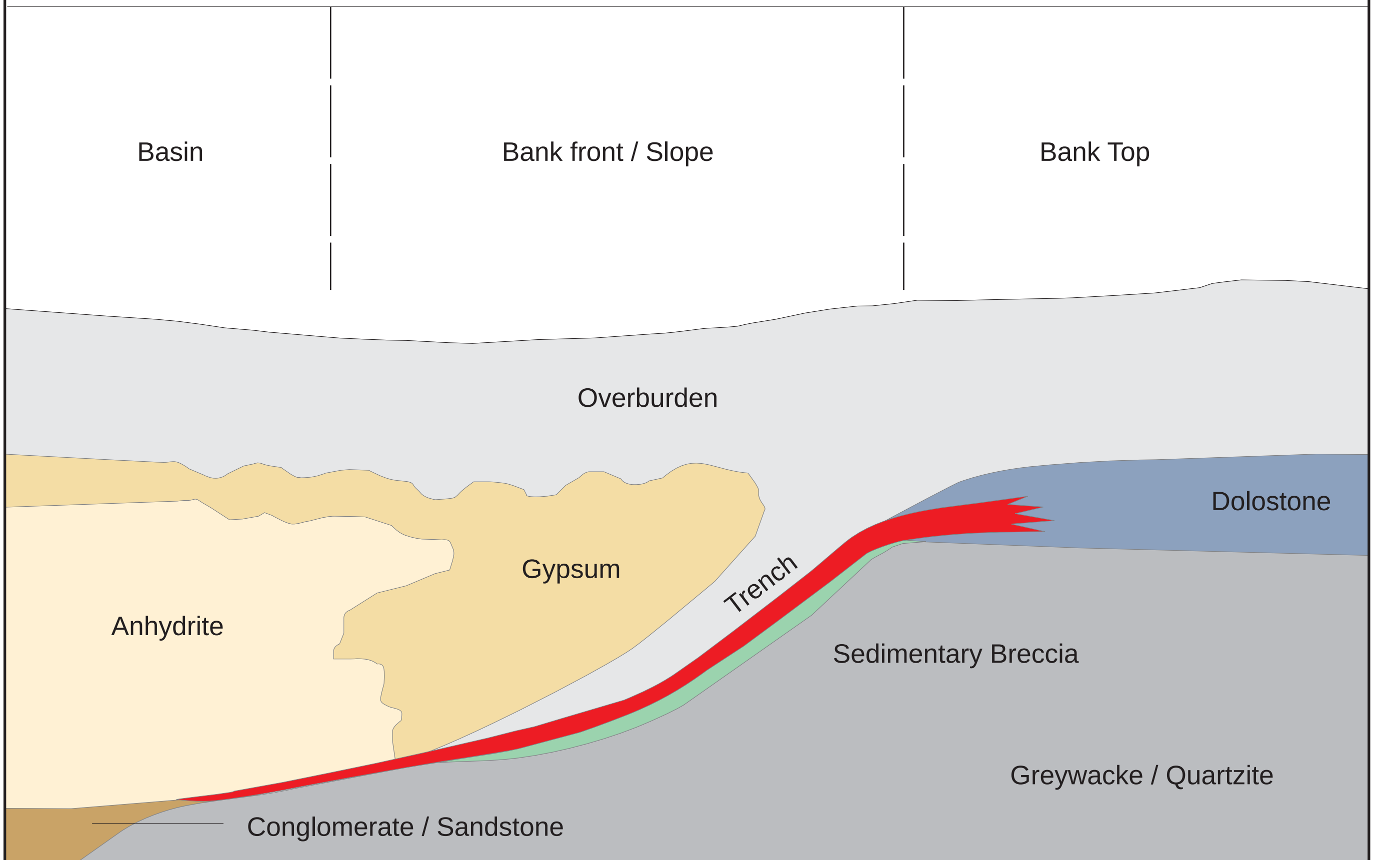

Lead / Zinc mineralization in dolostone

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Figure 6

Carbonate Bank Cross Section
Not to scale

Date: April 2011

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Genetic Model

The adjacent Scotia Mine deposit has been the subject of extensive academic and government research and reporting since its discovery in 1971. Much of this work was summarised by Roy et. al. (2006) and the deposit is a considered an example of the Mississippi Valley Type (MVT) class of carbonate hosted, stratabound, base metal deposits. Prominent examples of the paleo-basement high deposit setting occur along the Viburnum Trend of Southeast Missouri, but are characterised in that area by dominance of lead mineralization over that of zinc (Sangster et. al., 1998; Akande and Zentilli, 1983; MacEachern and Hannon, 1974).

Localization of base metals within the Getty bank complex is believed to have resulted from interaction between metal-bearing basinal fluids, potentially sourced in the Horton Group stratigraphic section or in basement sequences, and chemical reductants, possibly including hydrocarbon, that were present at sites of deposition within the bank. Kontak (1998, 2000) reported on fluid inclusion and other studies of ore from the adjacent Scotia Mine property and concluded that saline brines in the 100º C to ≤ 250º C temperature range were involved in the main mineralizing process and that these temperatures are higher than those typically seen in MVT districts. Héroux, et. al (1994) studied organic maturation and clay mineral crystallinity characteristics of Gays River Formation rocks of the Musquodoboit and Shubenacadie basins and identified a corridor of higher interpreted heat flow that occurs in part over the Scotia Mine and Getty deposit areas and is consistent with the higher fluid temperatures previously noted. It is clear that zinc and lead mineralization were superimposed on lithified and dolomitized host rocks (Akande and Zentilli, 1985; Kontak, 1998).

8.0 Mineralization

Zinc and lead sulphide mineralization are found throughout the Getty carbonate bank, along with trace amounts of iron sulphide in isolated areas. Base metal sulphides are also present to a lesser extent in carbonate matrix of the underlying conglomerate/breccia unit and within calcite or micrite filled fractures and joints present in underlying Goldenville Formation greywackes. While not extensively reported to date, galena has also been documented locally at the Scotia Mine deposit in thin (<20cm thick) discordant, steeply dipping veins that generally trend north-south (B. Mitchell, personal communication, 2007).

Drilling to date on the Getty deposit has shown that massive to submassive high grade mineralization like that commonly present along steep bank front zones at Scotia Mine is not present to a significant degree at Getty (Bryant, 1975). However, a clear association of higher zinc and lead grades with dolostone intervals on the northeast and north slopes of the Getty bank is recognized and lower grades over thicker intervals occur within the carbonate sections at the top of the bank. Mineralization is more poorly developed along the southwest side of the bank.

Sphalerite is the predominant base metal sulphide phase present and is typically honey yellow to buff or beige in colour and finely crystalline. Based on drill core observations, Bryant (1975) specified the following four modes of sphalerite occurrence within the deposit, with the first being the most common: (a) disseminated mineralization showing concentrations from trace to 10% or more, (b) semi-massive and massive mineralization as seams and replacements along bedding surfaces or laminae, (c) massive, porosity filling or surface coating mineralization in fossiliferous and vuggy carbonate, (d) mineralization associated with secondary calcite in small stringers and veinlets.

Silver is a trace constituent of the Getty sulphide assemblage but is not present at levels of economic significance. This parallels the situation at adjacent Scotia Mine where Roy et. al. (2006) reported historic silver values in mill concentrates that were typically less than 40 parts per million.

9.0 Exploration

Mercator completed a National Instrument 43-101 compliant Inferred Mineral Resource Estimate for Acadian on the Getty Deposit with an effective date of December 12, 2007. This initial estimate was subsequently updated in a new National Instrument 43-101 compliant resource in 2008 (Cullen et al., 2008) after a total of 10,620 meters of drilling in 138 diamond drill holes had been completed by Acadian on the Getty property under the direct supervision of Mercator staff. The information used to complete these estimates was compiled from the 2007-2008 drilling by Acadian plus historical drilling undertaken prior to Acadian's involvement in the property.

Acadian initiated a major diamond drilling program on the Getty property in July 2007, and Mercator provided all site supervision, logging, sampling and quality control/quality assurance services to Acadian for this program, which consisted of 138 diamond drill holes. The purpose of the drilling was to upgrade geological confidence in the deposit, provide a basis for the new mineral resource estimate and to provide a higher category classification to the mineral resource estimate (Cullen et al, 2008). Details of the drilling program are presented below in section 10.0 of this report.

10.0 Drilling

10.1 General

Historic diamond drilling information pertaining to the Getty deposit was compiled by Westminer in a digital database containing information for approximately 181 vertical holes totalling 16,875 meters of drilling. The Westminer database was originally prepared to support the resource estimate reported by Hudgins and Lamb (1992) and to this end, collar coordinates, lithologic codes, geologic legend and individual drill core assay interval results were compiled from original drill logs, checked for errors, and entered into the original digital database. All historic holes were initially coordinated to local Getty reference grid but Mercator subsequently transformed all drill hole coordinates into the Scotia Mine grid using historic tie points for which Acadian surveyors provided up to date mine grid coordination. Universal Transverse Mercator (UTM) coordinates (Zone 20, NAD 83 Datum) were also calculated by Mercator for all holes in the project database and a listing of drill hole coordinates and orientation data for the deposit in the block model grid system appears in Appendix 2. Mercator staff physically checked all drill hole entries in the database against the original hard copy logs.

Between July 2007 and April 2008, Acadian completed 10,620 meters of drilling in 138 diamond drill holes on the Getty property under the direct supervision of Mercator staff. The drilling program focused on 1) validation of past drilling results, 2) infilling in areas where insufficient information existed to define mineral resources or in areas where upgrading of existing Inferred mineral resources to Indicated or Measured categories was possible, 3) re-drilling of historic holes where information on sampling and assays were missing and 4) extension of mineralized zone limits beyond those previously defined. Table 5 below presents collar information for all drill holes completed by Acadian during the 2007-2008 program and a drill collar location plan is included in Appendix 4.

Table 5: Location and Attitude Information for Acadian Drilling Program

Hole Number	**Collar Coordinates (Mine Grid) Easting (m)**	**Northing (m)**	**Collar Elevation (m)**	**Angle (Deg.)**	**Depth (m)**
S992-07	6893.91	6584.66	556.35	-90	74
S993-07	6929.30	6618.11	549.27	-90	94
S994-07	6856.41	6554.85	557.89	-90	80
S995-07	6821.70	6521.68	555.54	-90	80
S996-07	6848.41	6595.56	556.96	-90	71
S997-07	6930.65	6508.78	556.57	-90	77
S998-07	6781.44	6593.48	557.26	-90	56
S999-07	6814.47	6624.98	555.77	-90	59
S1000-07	6885.79	6686.53	545.67	-90	86

Hole Number	Collar Coordinates (Mine Grid) Easting (m)	Northing (m)	Collar Elevation (m)	Angle (Deg.)	Depth (m)
S1001-07	6845.17	6658.82	549.86	-90	68
S1002-07	6786.06	6490.32	553.46	-90	61
S1003-07	6768.48	6552.21	555.35	-90	55
S1004-07	6752.62	6685.67	552.13	-90	70
S1005-07	6721.44	6644.97	554.69	-90	62
S1006-07	6686.72	6625.80	557.38	-90	47
S1007-07	6677.94	6663.15	555.31	-90	59
S1008-07	6683.03	6555.39	561.89	-90	41
S1009-07	6660.73	6593.76	562.19	-90	44
S1010-07	6614.98	6667.11	558.38	-90	50
S1011-07	6659.09	6707.74	551.81	-90	62
S1012-07	6682.36	6743.91	548.51	-90	73
S1013-07	6565.82	6741.08	553.64	-90	41
S1014-07	6578.49	6782.15	548.88	-90	44
S1015-07	6548.12	6785.40	548.88	-90	35
S1016-07	6535.89	6832.24	545.65	-90	35
S1017-07	6617.88	6791.98	549.48	-90	47
S1018-07	6609.90	6750.15	551.23	-90	44
S1019-07	6716.98	6769.90	548.11	-90	41
S1020-07	6685.49	6840.50	545.40	-90	92
S1021-07	6731.32	6614.94	555.01	-90	88
S1022-07	6720.95	6531.89	558.79	-90	38
S1023-07	6681.89	6793.99	548.38	-90	89
S1024-07	6726.11	6814.06	547.27	-90	116
S1025-07	6651.11	6897.88	541.49	-90	62
S1026-07	6622.50	6932.19	539.15	-90	71
S1027-07	6597.45	6897.27	541.61	-90	56
S1028-07	6627.40	6863.73	543.79	-90	62
S1029-07	6695.96	6898.51	542.29	-90	82
S1030-07	6565.23	6857.10	544.22	-90	53
S1031-07	6749.13	6795.28	547.15	-90	110
S1032-07	6546.38	6900.80	540.64	-90	46
S1033-07	6654.41	6851.35	544.55	-90	66
S1034-07	6774.93	6837.90	544.93	-90	121
S1035-07	6721.65	6897.27	542.28	-90	109
S1036-07	6805.61	6879.92	543.86	-90	146
S1037-07	6751.97	6930.99	539.29	-90	107
S1038-07	6772.03	6951.67	537.47	-90	104
S1039-07	6603.08	7032.43	533.53	-90	78
S1040-07	6794.17	6918.98	541.32	-90	137
S1041-07	6670.44	6962.86	537.76	-90	61
S1042-07	6673.35	7031.89	529.53	-90	62
S1043-07	6744.07	6997.20	531.85	-90	80
S1044-07	6964.92	6534.27	554.71	-90	68
S1045-07	6993.70	6571.80	549.40	-90	80

Hole Number	**Collar Coordinates (Mine Grid)**		**Collar Elevation (m)**	**Angle (Deg.)**	**Depth (m)**
	Easting (m)	**Northing (m)**			
S1046-07	6728.98	7029.90	527.17	-90	89
S1047-07	7033.36	6544.93	548.43	-90	62
S1048-07	7070.89	6511.28	547.12	-90	89
S1049-07	6698.73	6997.98	531.93	-90	60
S1050-07	7036.00	6590.68	545.38	-90	95
S1051-07	6731.34	6719.44	550.07	-90	76
S1052-07	6864.45	6441.26	552.43	-90	92
S1053-07	6857.46	6523.76	557.03	-90	89
S1054-07	6913.68	6433.70	553.87	-90	116
S1055-07	6999.86	6326.58	546.89	-90	151
S1056-07	6952.4	6314.51	544.55	-90	83
S1057-07	6975.89	6618.16	546.16	-90	101
S1058-08	6925.51	6667.45	545.26	-90	101
S1059-08	6997.46	6512.28	553.10	-90	71
S1060-07	7032.31	6419.19	548.38	-90	96
S1061-08	7005.67	6381.08	550.01	-90	121
S1062-08	7103.53	6470.53	544.62	-90	92
S1063-08	6795.97	6801.93	546.91	-90	107
S1064-08	6898.19	6224.86	535.36	-90	43
S1065-08	6853.43	6228.90	537.35	-90	64
S1066-08	6883.95	6318.98	540.69	-90	60
S1067-08	6883.85	6114.43	538.11	-90	48
S1068-08	6917.47	6721.67	544.39	-90	113
S1069-08	6906.40	6055.05	532.45	-90	71
S1070-08	6908.98	6368.17	548.36	-90	92
S1071-08	6826.52	6747.33	549.09	-90	88
S1072-08	6851.27	6786.47	546.98	-90	95
S1073-08	6742.15	6144.40	530.59	-90	27
S1074-08	6607.02	6107.87	524.85	-90	78
S1075-08	6947.63	6763.13	542.18	-90	113
S1076-08	6672.95	6163.98	528.14	-90	43
S1077-08	6811.59	6037.49	526.52	-90	60
S1078-08	6533.73	6301.72	543.98	-90	83
S1079-08	6549.57	7039.43	528.97	-90	80
S1080-08	6584.42	6310.65	543.13	-90	68
S1081-08	6637.48	6293.16	538.46	-90	32
S1082-08	6561.66	7000.93	531.65	-90	77
S1083-08	6616.27	6221.05	529.77	-90	44
S1084-08	6500.18	6997.60	530.26	-90	101
S1085-08	6526.73	6184.70	528.75	-90	117
S1086-08	6482.64	6911.99	538.37	-90	76
S1087-08	6468.44	6959.88	533.30	-90	95
S1088-08	6538.84	6228.15	532.35	-90	51
S1089-08	6535.10	6226.14	532.34	-90	95
S1090-08	6537.21	6351.61	552.64	-90	86

Hole Number	Collar Coordinates (Mine Grid) Easting (m)	Northing (m)	Collar Elevation (m)	Angle (Deg.)	Depth (m)
S1091-08	6728.05	7111.32	513.44	-90	83
S1092-08	6604.71	6354.78	550.65	-90	80
S1093-08	6763.48	7081.30	514.80	-90	59
S1094-08	6521.74	6394.32	560.35	-90	86
S1095-08	6803.17	7074.47	512.95	-90	72
S1096-08	6478.63	6368.11	556.93	-90	104
S1097-08	6434.31	6928.53	533.35	-90	95
S1098-08	6538.88	6442.45	564.27	-90	68
S1099-08	6468.35	6412.56	561.40	-90	112
S1100-08	6472.48	6865.00	539.96	-90	57
S1101-08	6512.89	7035.97	529.15	-90	104
S1102-08	6551.60	6494.31	564.66	-90	71
S1103-08	6594.06	6495.90	565.40	-90	62
S1104-08	6440.43	6964.51	531.46	-90	50
S1105-08	6557.47	6553.06	564.25	-90	122
S1106-08	6610.53	6545.52	566.28	-90	62
S1107-08	6518.11	6592.52	562.51	-90	101
S1108-08	6422.59	6869.34	539.52	-90	58
S1109-08	6467.99	6317.44	549.34	-90	59
S1110-08	6369.43	6864.19	537.50	-90	41
S1111-08	6389.85	6915.57	533.73	-90	73
S1112-08	6668.56	6196.65	528.77	-90	30
S1113-08	6656.95	6116.13	526.39	-90	78
S1114-08	6281.48	6867.30	535.48	-90	23
S1115-08	6662.51	6243.31	531.36	-90	26
S1116-08	6570.75	6406.75	561.01	-90	68
S1117-08	6257.15	6957.27	528.04	-90	62
S1118-08	6490.24	6252.22	539.16	-90	104
S1119-08	6551.70	6113.51	523.32	-90	77
S1120-08	6314.82	6982.61	527.53	-90	36
S1121-08	6236.26	6900.80	529.95	-90	38
S1122-08	6571.44	6219.21	530.35	-90	75
S1123-08	6960.44	6664.49	544.90	-90	116
S1124-08	6896.65	6538.24	557.69	-90	80
S1125-08	6987.14	6469.86	553.76	-90	89
S1126-08	6817.12	6150.50	534.95	-90	38
S1127-08	6489.42	6146.45	529.21	-90	137
S1128-08	6851.05	5283.15	543.74	-90	218
S1129-08	6256.73	6257.29	555.39	-90	177

The complete Getty project drilling database includes results of the 138 diamond drill holes recently drilled by Acadian and the 184 historic drill holes completed during the 1970's, 181 of which were drilled by Getty and total 16,875 meters of drilling. The three remaining holes were completed by Esso during the same time period and totalled 157 meters of drilling. The resource outline pertinent to this report includes all of the 138 Acadian holes and 68 of the historic drill holes. Additional relevant drilling information is included in Appendix 2.

All holes were drilled vertically and mineralized intercepts from holes drilled on the bank top, where mineralization is generally horizontal, represent true width. Mineralization intercepts from holes drilled on the bank front, where mineralization slopes, true width is 60-70% of intercept the width. A detailed plan of hole locations relative to mineralization is presented in Appendix 4. Drill hole core recovery for Acadian drilling was in excess of 90% and recovery was not a factor in the resource estimation. A review of logs for historic drill holes and re-logging of select historic holes by Mercator did not identity core loss as an issue.

10.2 Logistics of Acadian Drill Program

Logan drilling of Stewiacke, Nova Scotia was contracted to complete 2007-2008 drilling utilizing skid mounted Longyear 38 drilling equipment equipped to recover NQ sized drill core (4.76 cm diameter). One drill was typically employed, but a second drill was periodically on site. Both machines typically operated on a 24 hour per day basis. Mercator was contracted to manage day to day drilling operations and provided onsite supervision, transportation of core to the secure logging facility at Acadian's Scotia Mine, plus logging of drill core and supervision of core sampling services. A registered land surveyor surveyed drill hole collars and all drill holes were coordinated to the local Scotia Mine grid system.

11.0 Sampling Method and Approach

11.1 Getty and Esso Programs: 1972 to 1975

Government assessment reports were reviewed to identify core logging and sampling procedures applicable to the Getty and Esso drilling programs carried out between 1972 and 1975. These showed that drill core was typically logged by staff geologists who produced hard copy lithologic logs for each drill hole. Detailed information related to lithology and mineralization was systematically recorded in the logs along with complete records of core sampling and major analytical results. There is no specific description of sample marking, cutting, handling, tagging or shipping protocols, but industry standard marking and tagging of sample intervals is evident in the archived drill holes viewed and sampled by Mercator staff in 2007 at the Nova Scotia Department of Natural Resources core library in Stellarton, Nova Scotia (core library). Half-core samples were typically submitted for analysis and sample intervals reflected visually determined mineralized zone limits. A sample interval of 5 feet was commonly used but no standard appears to have been established by either company. Non-mineralized carbonate was rarely sampled. Core was logged in imperial measure and drill logs were transformed to metric equivalents subsequently during the digital data entry process.

Core from the original Getty drilling program was placed in marked core boxes and retained in covered storage in the local area until 1984. At that time NSDNR took procession of the core and it was archived at the core library in Stellarton. Esso core was stored at the Gays River mine site, with mineralized intervals typically retained in covered storage and the remaining non-mineralized intervals stored out of doors where rapid deterioration of boxes and core took place. Core storage facilities established by Esso deteriorated over the years and in some cases have been demolished. No accurate records exist of archived core or of core salvaged from the deteriorated buildings. As a result, it is unclear whether core from the Esso holes completed at Getty is included in the non-inventoried remnants of archived core that currently exists at the Scotia Mine facility. With no evidence to the contrary, it is assumed that this core has been lost or destroyed and is not available for review at present.

11.2 Acadian Program: 2007-2008

All drill core was transported on a daily basis from the site to the nearby Scotia Mine owned by Acadian/ScoZinc. Core was photographed, logged and sampled in a secure logging facility and then continuously sampled through the carbonate and basal breccia intervals using a nominal 1.0 meter sample length. A mechanical core splitter was used to create half core samples, with one half retained for archival purposes and the other placed in a pre-numbered plastic sample bag along with a corresponding paper sample tag and submitted for laboratory analysis. Sample numbers were recorded in both the core log and in sample record logs for the drill hole. In accordance with the quality assurance and quality control protocol set up by Mercator for this drill program, the archive portion of every 40th sample in the core sample sequence was quarter split and one quarter was sent to ALS Chemex, an ISO certified third part commercial laboratory, for analysis of metal levels. Results of this program appear in Section 13.2 of this report.

After insertion of quality control samples, including blanks and standards, all bagged samples were checked for sequence, placed in sealed plastic buckets and shipped to Eastern Analytical in Newfoundland for multi element ICP analysis. As discussed later in Section 13.2, systematic check sample pulps were prepared and forwarded to Mercator by Eastern Analytical, where standards and blanks were inserted prior to submission to ALS Chemex in Sudbury for analysis.

11.2.1 Acadian Re-sampling of Getty Drill Holes

Ten drill holes completed by Getty in 1972, representing a wide grade and location range within the deposit, were selected by Mercator for re-sampling as part of the project quality control and assurance program. This work was carried out by Mercator geologists during 2007 and 2008 on core from ten Getty drill holes (Table 6) archived at the Stellarton core library maintained by Nova Scotia Department of Natural Resources. Quarter core samples of the historically half-core sampled carbonate intervals were collected from the selected holes, ensuring a quarter of the core remained for archival purposes. Assay comparison tables for this sampling program appear in report Section 13.2.2, along with descriptions of sample handling, lab information and analytical procedures. Eastern Analytical (Eastern) was the primary lab used for the 2007/2008 Getty program and ALS Chemex (ALS) was used for check samples.

Table 6: Historic Drill Holes Re-sampled In 2007

Drill Hole	**Drill Hole**	**Drill Hole**	**Drill Hole**	**Drill Hole**
GGR-39A	GGR-96	GGR-125	GGR-130	GGR-167
GGR-178	GGR-193	GGR-208	GGR-211	GGR-217

12.0 Sample Preparation, Analyses and Security

12.1 Getty and Esso Programs

Reports documenting the Getty and Esso drilling programs in the Getty deposit area do not provide detailed descriptions of sample preparation methodologies, analytical procedures or security considerations. However, both Getty and Esso were major, reputable exploration companies carrying out exploration programs in various settings at that time. More specifically, Esso was also in the process of defining reserves at the adjacent Gays River mine at the time and appears to have employed the same operating protocols for Getty drilling as were applied at the adjacent development property. Mercator is of the opinion that, while not specifically detailed in historic reporting, procedures employed by both Getty and Esso for sample preparation, record keeping, chemical analysis, and security, would have met industry standards of the day. This assertion is supported by review of original drill logs and supporting data, physical review of archived core and through recognition that both companies completed resource estimate and preliminary development assessments based on the same historic drilling results.

12.2 Acadian Programs

12.2.1 Sample Security and Chain of Custody

In accordance with the sample protocol established by Mercator for Acadian's 2007-2008 Getty drilling program, all drill core was delivered from the drill site to the secure and private core logging facility at Acadian's Scotia Mine by either Logan Drilling Limited staff or Mercator field staff. Drill core logging was carried out by a Mercator geologist who also marked core for sampling and supervised core splitting by a technician using a rock saw. Sample tag numbers from a three tag sample book system were used for the program, with one tag showing corresponding down hole sample interval information placed in the sampled core boxes at appropriate locations, one tag lacking down hole interval information placed in the core sample bag for shipment to the laboratory, and the third tag with sample interval information retained in the master sample book for future reference and database entry purposes. After sampling, core boxes were closed and placed in storage at the Scotia Mine site. Sealed sample bags were placed in an ordered sequence prior to insertion of quality control samples, preparation of sample shipment documentation, checking, and placement in plastic buckets for shipment by commercial courier to Eastern Analytical Limited (Eastern), a recognized commercial laboratory located in Springdale Newfoundland. A check pulp sample split was prepared at Eastern for every 25th submitted sample and these were labelled, placed in a sealed envelope and returned to Mercator. After insertion of certified standard and blank samples, all check samples were sent to ALS Chemex in Sudbury, ON for independent analysis of zinc and lead levels. All other prepared pulps and coarse reject material was stored at Eastern until the end of the program, at which time they were shipped back to Acadian's Scotia Mine for secure archival storage.

In the case of the re-sampling program of historic Getty drill holes, archived half core from the holes was accessed at the NSDNR core library in Stellarton and split to produce quarter core samples. The sample interval was recorded using the same three tag system described previously for the Acadian core and samples were processed as described above for Acadian drilling program core samples. Samples were sent to Eastern via commercial courier where laboratory analysis was completed and pulp and reject material was handled as noted above.

12.2.2 Core Sample Preparation

Core samples received by Eastern were organized and labelled and then placed in drying ovens until completely dry. Dried samples were crushed in a Rhino Jaw Crusher to consist of approximately 75% minus 10 mesh material. The crushed sample was riffle split until 250 to 300 grams of material was separated and the remainder of the sample was bagged and stored as coarse reject. The 250 – 300 gram split was pulverized using a ring mill to consist of approximately 98% minus 150 mesh material. All samples underwent ICP analysis, for which a 0.50g portion of the pulverized material was required. Those samples containing greater than 2200 ppm of zinc or lead were then processed using ore grade analysis for which 0.20g of pulverized material was required. Laboratory sample preparation equipment was thoroughly cleaned between samples in accordance with standard laboratory practise.

Check sample splits of pulverised core were submitted to the ALS Chemex laboratory facility in Sudbury, Ontario as part of the project quality control and assurance protocol. This material was prepared in approximately 100 gram bagged splits by Eastern and returned to Mercator for subsequent submission to ALS Chemex. Since the received split material had already been pulverised, further preparation was limited to homogenization and splitting of a 0.4g portion for subsequent analysis.

12.2.3 Core Sample Analysis

Eastern Analytical procedures outlined below pertain to all core samples from the 2007-2008 Acadian drill program, including those from the Getty core re-sampling and hole twinning components. Descriptions are for assay procedures, quality determinations and additional details appear in Appendix 2.

- ICP Analysis: A 0.50 gram sample is digested with 2ml HNO3 in a 95^{o}C water bath for ½ hour, after which 1ml HCL is added and the sample is returned to the water bath for an additional ½ hour. After cooling, samples are diluted to 10ml with de-ionized water, stirred and let stand for 1 hour to allow precipitate to settle.

- For ore grade analysis base metals (lead, zinc, copper), a 0.20g sample is digested in a beaker with 10ml of nitric acid and 5ml of hydrochloric acid for 45 minutes. Samples are then transferred to 100ml volumetric flasks and analyzed on the Atomic Absorption Spectro-Photometer (AA). The lower detection limit is 0.01% and the upper detection limit is >2200 ppm lead or zinc.

- For silver, a 1000mg sample is digested in a 500ml beaker with 10ml of hydrochloric acid and 10ml of nitric acid with the cover left on for 1 hour. Covers are then removed and the liquid is allowed to evaporate leaving a moist paste. 25ml of hydrochloric acid and 25ml of deionised water are then added and the solution is gently heated and swirled to dissolve the solids. The cooled material is transferred to 100ml volumetric flask and is analyzed using AA. The lower detection limit is 0.01oz/t of silver with no upper detection limit.

- A prepared sample is digested in 75% aqua regia for 120 minutes. After cooling, the resulting solution is diluted to volume (100 ml) with de-ionized water, mixed and then analyzed by inductively coupled plasma - atomic emission spectrometry or by atomic absorption spectrometry.

13.0 Data Verification

13.1 Review and Validation of Project Data Sets

Review by Mercator of all government assessment reports and internal Acadian files available from the Scotia Mine site established that typed lithologic logs with complete assay records from the Getty drilling era were available. However, original sample record books, laboratory reports and other associated information were not found. The digital drill hole database used for the Westminer's 1992 resource estimate was also obtained from Acadian and validated against the original hard copy drill log and assay record entries. Checking of digital records included manual inspection of individual database lithocode entries against source hard copy drill logs as well as use of automated validation routines that detect specific data entry logical errors associated with sample records, drill hole lithocode intervals, collar tables and down-hole survey tables. Drill hole intervals were also checked for sample interval and assay value validity against the original drill logs. Database entries were found to be of consistently acceptable quality but minor lithocode and assay entry corrections were made by Mercator. These were incorporated to create the validated and functional drilling database used in the resource estimate. As noted earlier, original assays certificates were not found for any of the historic drilling programs and no records of the laboratories to which samples were submitted for analysis, or methods of analysis, were documented in any of the historic drilling reports reviewed for the resource estimate.

As part of the validation process, Mercator staff visited the NSDNR Core Library in Stellarton, Nova Scotia to review and sample core from the archived Getty drill holes. Nineteen holes where examined but only one hole GGR-212 was re-logged in detail and ten holes, previously identified in report Table 6 were re-sampled and analysed for purposes of quality control and quality assurance. These provided additional verification of historical assays and logging results. Results of this and related programs are presented below under separate headings.

13.2 Quality Control and Quality Assurance (QA/QC)

13.2.1 Historic Drilling Programs

Assessment reports documenting Getty and Esso drilling programs do not specifically address QA/QC issues. No evidence was noted of independent certified standards being submitted with core samples from either company nor is there any evidence of systematic submission of blank samples or systematic provision for duplicate sample splits to be prepared and analysed. Similarly, detailed descriptions of sample preparation methodologies, analytical procedures or security considerations are not present in any of the historic documentation reviewed for this report. This situation was not uncommon in exploration program reporting during the 1970's era and later, when reliance was placed to a substantial degree on standards, duplicate samples and other quality assurance and control procedures implemented by the commercial laboratories providing analytical work.

As noted earlier, both Getty and Esso were major, reputable companies at the time of their drilling programs on the Getty deposit and that Esso was completing reserve delineation and mine planning work for the adjacent Gays River (Scotia Mine) project that entered commercial production in 1979. Both companies are considered credible and Mercator's review of drill logs and associated sample data did not reveal any points of obvious concern with respect to use of historic results for the project.

Notwithstanding the above, the lack of laboratory assay certificates and information on sampling and laboratory procedures necessitated a review of and re-sampling of archived Getty core and the twinning of a number of Getty-era drill holes within the resource area. These safeguards were implemented and results are discussed below.

13.2.2 Overview of Acadian Programs

Mercator, on behalf of Acadian, established and administered a quality control and quality assurance program for the Getty 2007-2008 drilling project. All drill core samples, including samples associated with the twinned and re-sampled historic drill holes, were subject to project quality control and assurance (QA/QC) protocols. The program included insertion of blind certified standards and in-house blanks, analysis of quarter core duplicate samples, duplicate analysis of prepared pulps and submission of check sample pulps to an alternate commercial laboratory for analysis. Details of each program component are presented below.

13.2.2 (a) Certified Standard Samples

Certified standard materials were obtained from the Canadian Resource Laboratories of Delta, BC for use in the 2007 drilling program, these being CDN-SE-1 and CDN-SE-2. Table 5a presents the expected parameters for the CDN-SE-1 and 2 standards. At the onset of the program, only CDN-SE-1 was used. The second standard was introduced in Hole S1035 and from that point forward the two were alternated in the sample sequence. Pre-packaged prepared sample pulps of the standard material, weighing approximately 50 grams, were inserted in the core sample stream at intervals of every 35th sample and recorded as such. At first, standards were numbered in sequence with the sample stream; however, as of mid-September 2007 a separate sample book and associated tags were used. Certified value and error margin information for the two standards appear in Table 7 and results for the 79 certified standard samples returned for the Acadian program are presented below in Figures 7 and 8.

Table 7: CDN Laboratories Ltd. Standards - Certified Values

Standard	Gold g/t	Silver g/t	Copper %	Lead %	Zinc %
CDN-SE-1	0.480 ± 0.034	712 +/- 57 g/t	0.097 ± 0.005	1.92 ± 0.09	2.65 ± 0.20
CDN-SE-2	0.242 ± 0.018	354 ± 21 g/t	0.049 ± 0.003	0.957 ± 0.044	01.34 ±.11

Date of Certification: May 15th, 2007

Review of CDN-SE-1 results indicate zinc levels generally fall within expected parameters, while lead results tend to systematically group near the low limit of the acceptable value range, with maximum variation being 0.09% (Figure 7). Analytical results for both lead and zinc reported for CDN-SE-2 appear in Figure 8 and typically group near the lower error limit for respective certified values. As presented in Table 8, calculated mean zinc and lead values for the CDN-SE-1 standard data set fall within acceptable ranges for the standard. The mean zinc value for the CDN-SE-2 data set also falls within the standard's acceptable range, while the mean lead value for CDN-SE-2 falls 0.01% below the lower range limit for the standard (Table 8).

Table 8: Descriptive Statistics for CDN-SE-1 and CDN-SE-2 Certified Standards

Parameter	CDN-SE-1 Zinc	Certified Value Zinc %	CDN-SE-1 Lead	Certified Value Lead %
Mean	2.641	2.65 ± 0.20	1.83	1.92 ± 0.09
Variance	0.031		0.002	
Standard Deviation	0.176		0.047	
Maximum	3		1.96	
Minimum	2.28		1.74	
Number	54		54	

Parameter	CDN-SE-2 Zinc	Certified Value Zinc %	CDN-SE-2 Lead	Certified Value Lead %
Mean	1.2424	1.34 ±.11	0.90	0.957 ± 0.044
Variance	0.0021		0.0005	
Standard Deviation	0.046		0.024	
Maximum	1.34		0.95	
Minimum	1.12		0.85	
Number	25		25	

While some results for both standards show slight systematic departures within certified mean value ranges, this variation is not considered to be of sufficient magnitude to impact substantively on grade estimation within the deposit model. A similar conclusion applies to lead results for standard CDN-SE-2, which returned a mean value exceeding the lower range limit by 0.01%. On the basis of these combined results, associated core sample data are interpreted to be of acceptable accuracy for resource estimate use.

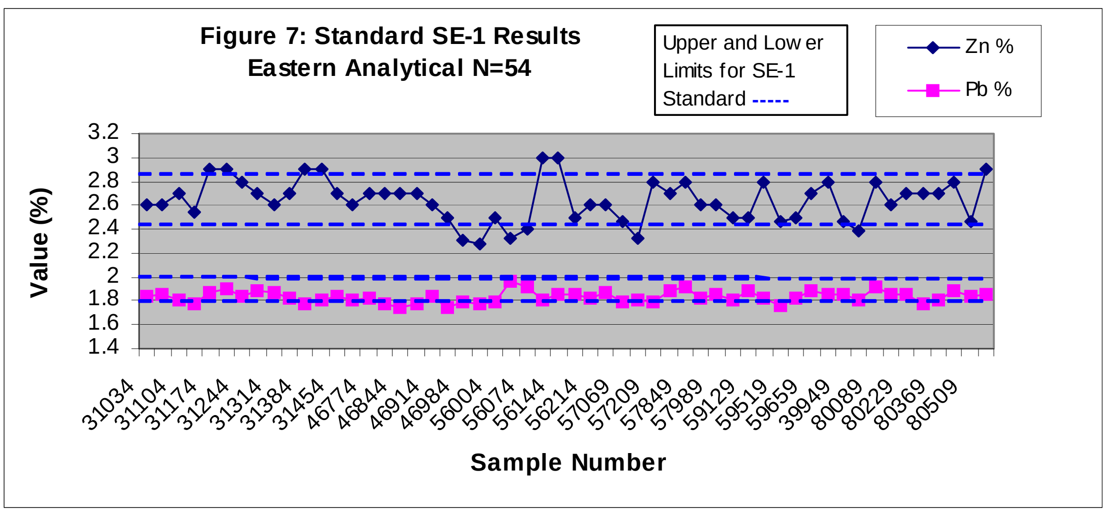

Figure 7: Standard SE-1 Results

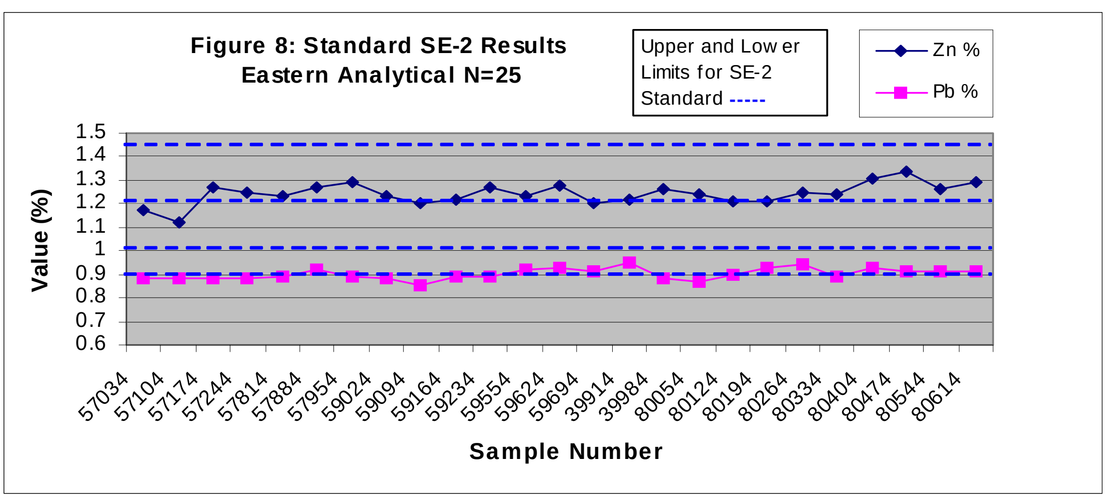

Figure 8: Standard SE-2 Results

13.2.2 (b) Blind Blank Samples

Blank samples of comparable weight to normal 1.0 m half core samples were systematically inserted at intervals of every 20th sample in the laboratory submission stream. These blank samples formed part of the continuous sample number series and consisted of non-mineralized anhydrite half-core collected from historic drill hole CBB-3. Blank samples were blind to the receiving laboratory. As with the case of Certified Standards, details on the blank sample program are reported in the Kennedy (2008) QAQC report that appears in Appendix 2. Summarized results are discussed.

Figures 9 and 10 are graphical representations of zinc and lead analytical results for the 135 blank samples submitted in support of the Acadian drilling program. Levels of both metals are relatively low, with zinc values not exceeding 203.56 ppm (mean 30.28 ppm) and lead not exceeding 273.60 ppm (mean 23.44 ppm). Descriptive statistics for the lead and zinc datasets appear in Table 9. Review of blank sample values relative to adjacent sample values showed no obvious indication of systematic cross contamination between blank samples and those of proceeding or subsequent higher grade samples. However, while blank sample materials showed no visual evidence of sphalerite or galena mineralization, variation in lead and zinc levels reflected in the blank sample population attributable to natural heterogeneity within the source anhydrite sequence was not quantified independently of the core sample stream. As a result, laboratory cross contamination at the level of a several tens of ppm would not be discernible based on the blank sample data set. Notwithstanding this limitation, maximum values for both lead and zinc reported for blank samples are low and mean population values are very low. On this basis, results for the 135 blank samples are interpreted as defining an acceptable range of variation and that cross-contamination, if any, is not represented at a level that is significant to resource estimation. In future, it is recommended that consideration be given to quantitatively assessing blank sample core materials prior to use, so that closer control of cross-contamination potential can be realized.

Table 9: Descriptive Statistics for Anhydrite Blank Samples Data Set

Parameter	**Zinc**	**Lead**
Mean	30.28	23.44
Variance	1416.72	1142.36
Standard Deviation	37.64	33.80
Maximum	203.56	273.60
Minimum	2	2
Number	135	135

13.2.2 (c) Quarter Core Duplicate Samples

Every 40th sample of the Acadian core sample sequence for the 2007-2008 program was quarter split and one quarter of the archive half core was submitted to Eastern Analytical for analysis, in addition to the standard half sample, as part of the normal sample numbering sequence up to and including hole S1020. Subsequent to hole S1020 a distinct

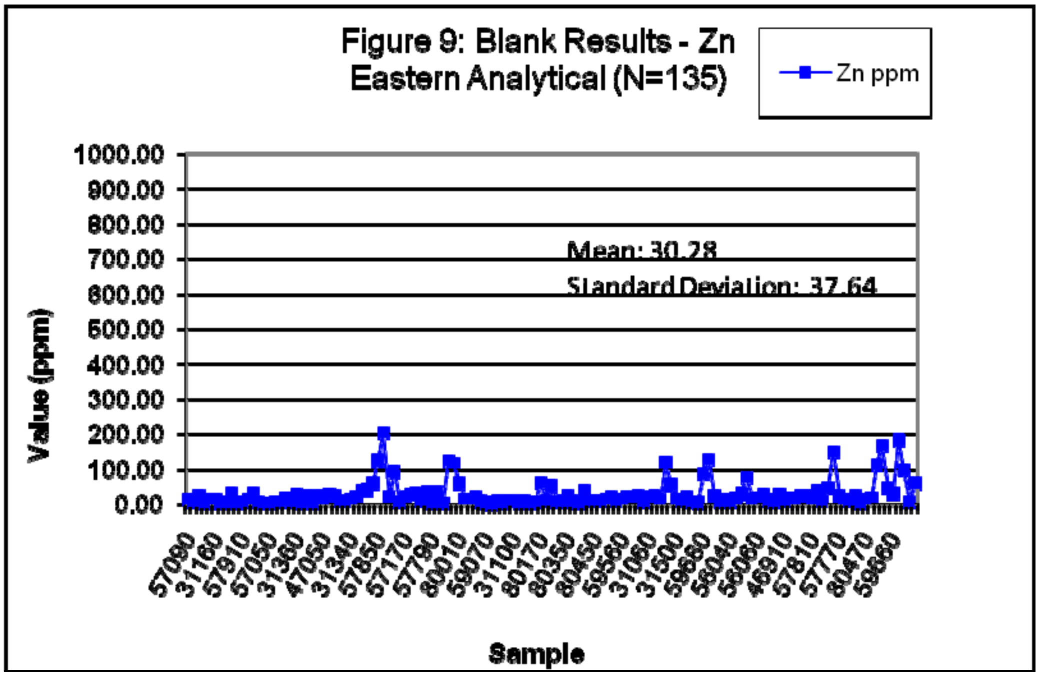

Figure 9: Blank Results - Zn

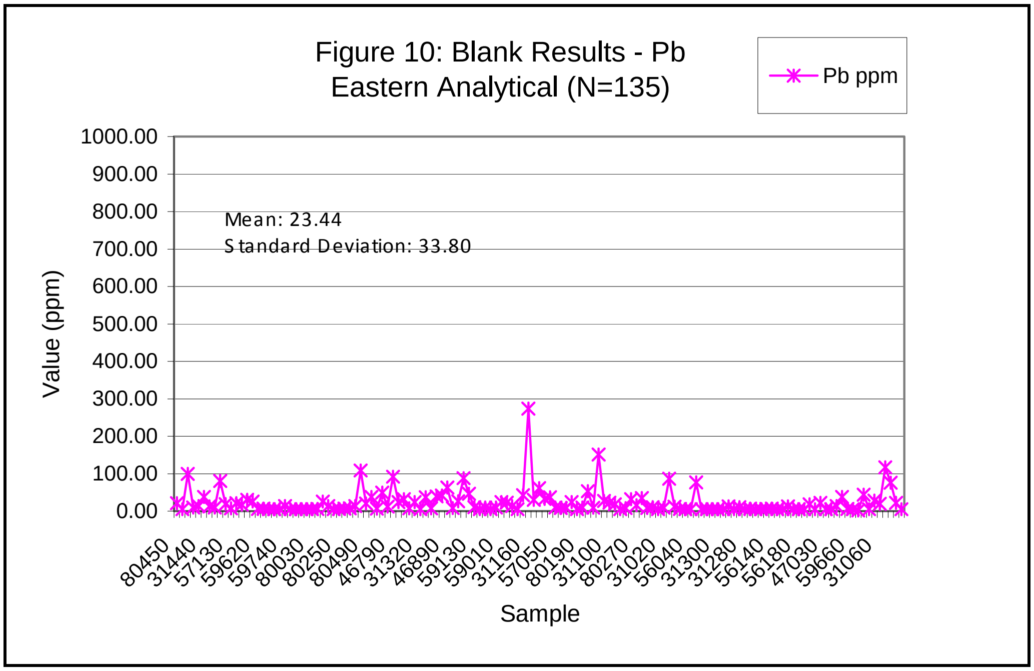

Figure 10: Blank Results - Pb

sample book was used and quarter core samples were marked accordingly. In total, analytical results for 64 duplicate quarter core pairs were received and are discussed by Kennedy (2008) in the QAQC report included in Appendix 2. Summarized results are discussed below.

Figure 11 presents lead and zinc data for the program and average grade variation between quarter core samples and corresponding half core samples is 0.11% for zinc and 0.09% for lead. Some degree of variability is expected within core split samples due to distribution heterogeneity of mineralization within the sample interval. Review showed that mean calculated variation is substantially influenced by results from four samples with variations between 0.6% Zn and 0.8% Zn. With removal of these and recalculation, mean variation for zinc for the remaining 61 samples drops to 0.06% and that for lead drops to 0.07%. These figures better reflect the majority of quarter core program results. Correlation coefficients calculated for both lead and zinc quarter core programs, inclusive of the four higher grade values, are both 0.98 (98%) and are interpreted as indicating an acceptable degree of homogeneity of mineralization in the majority of sampled intervals. Results also indicate that standard half core sampling carried out during the 2007-2008 drilling program, as well as in historic programs, provided acceptably representative samples of the core intervals.

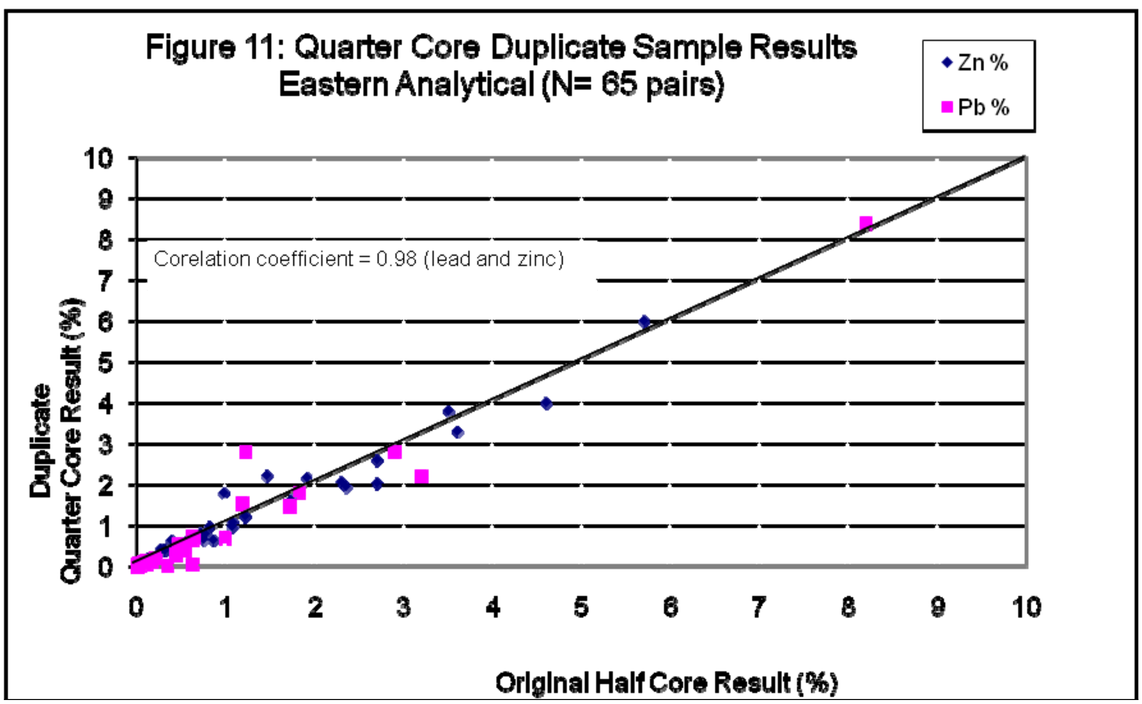

Figure 11: Quarter Core Duplicate Sample Results

13.2.2 (d) Duplicate Sample Splits

A duplicate split of prepared pulp material was requested from every 25th sample of the normal core sample stream and the laboratory was instructed to complete and report zinc and lead levels for these splits. Splits were labelled “A” and “B” respectively and results for the resulting duplicate pulp pairs are displayed in Figures 12 and 13 below. In total, 97 pairs were considered and average variation between the pulp duplicate samples is 0.03% for zinc and 0.03% for lead, with the datasets supporting correlation coefficients of 0.999 (99.9%) for zinc and 0.997 (99.7%) for lead. The high degree of correlation between the pulp splits is interpreted as indicating that precision within the data set is acceptable for current resource estimation purposes.

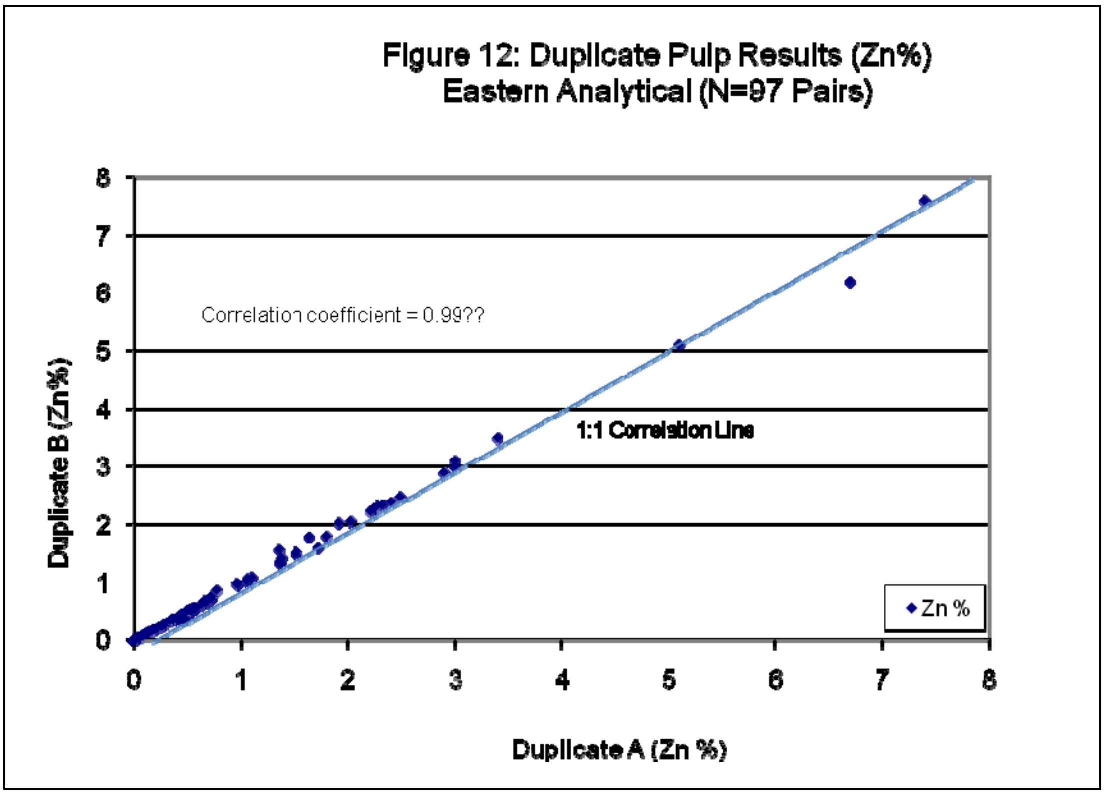

Figure 12: Duplicate Pulp Results (Zn%)

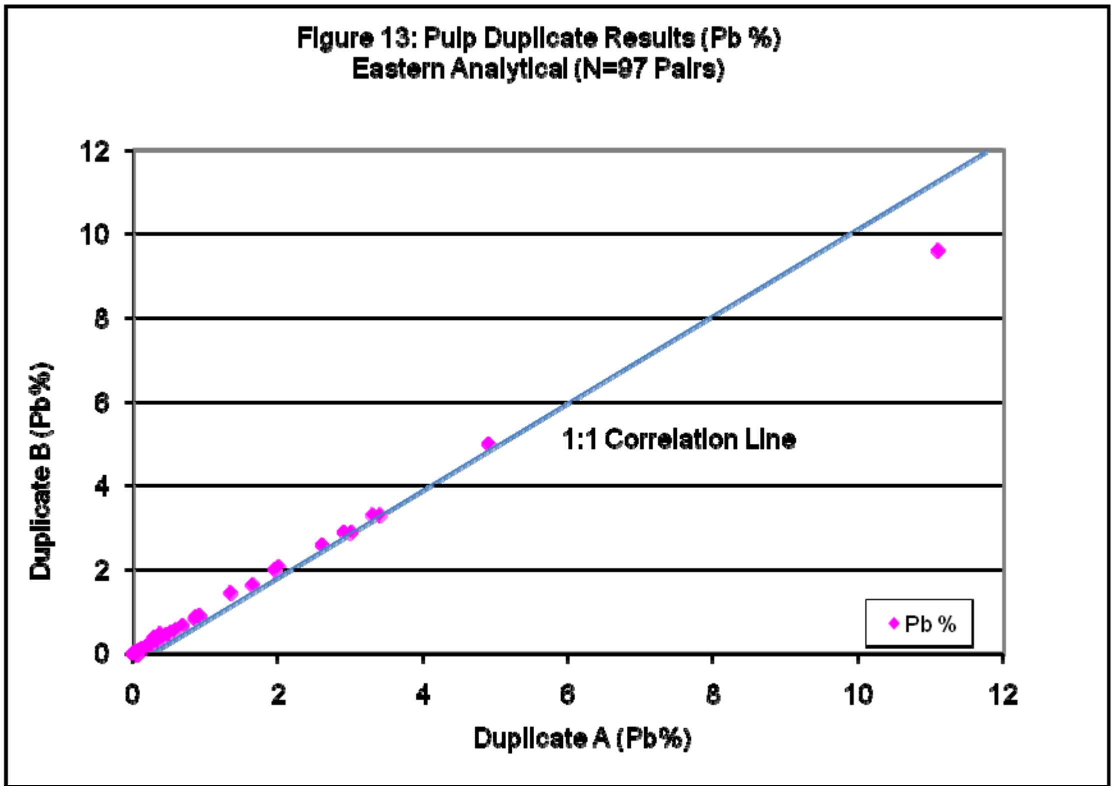

Figure 13: Duplicate Pulp Results (Pb%)

13.2.2 (e) Check Samples

A check sample split was prepared from the same crushed sample material prepared from every 25th core sample used for duplicate split purposes. The core was pulverized to -150 mesh, labelled, placed in a sealed envelope and returned to Mercator. All check samples were then sent to ALS Chemex in Sudbury, ON for independent analysis of zinc and lead levels. To provide quality control at the secondary laboratory, blank and standard samples were blindly inserted into check sample shipments to ALS Chemex. Results returned for these blanks and standards were acceptable and are presented in the Kennedy (2008) QA/QC report (Appendix 2). Figures 14 and 15 present correlated lead and zinc results for the check sample pairs submitted to the two laboratories. Variation between pairs for the two data sets range between 0.01% to 1.75% for zinc and 0.01% and 1.14% for lead. Correlation coefficients of 0.98 (98%) for zinc and 0.99 (99%) for lead were calculated for the two check sample data sets and indicate a high degree of correlation. In combination, results are considered acceptable for use of associated core sample data for resource estimation purposes.

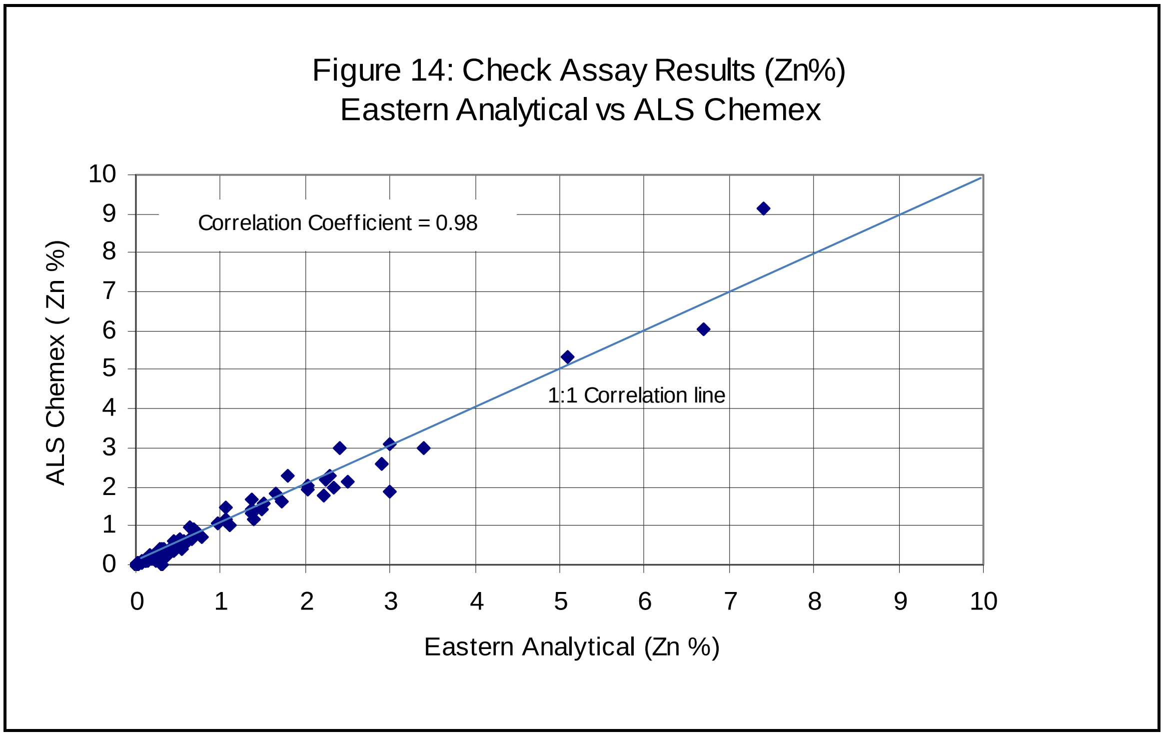

Figure 14: Check Assay Results (Zn%)

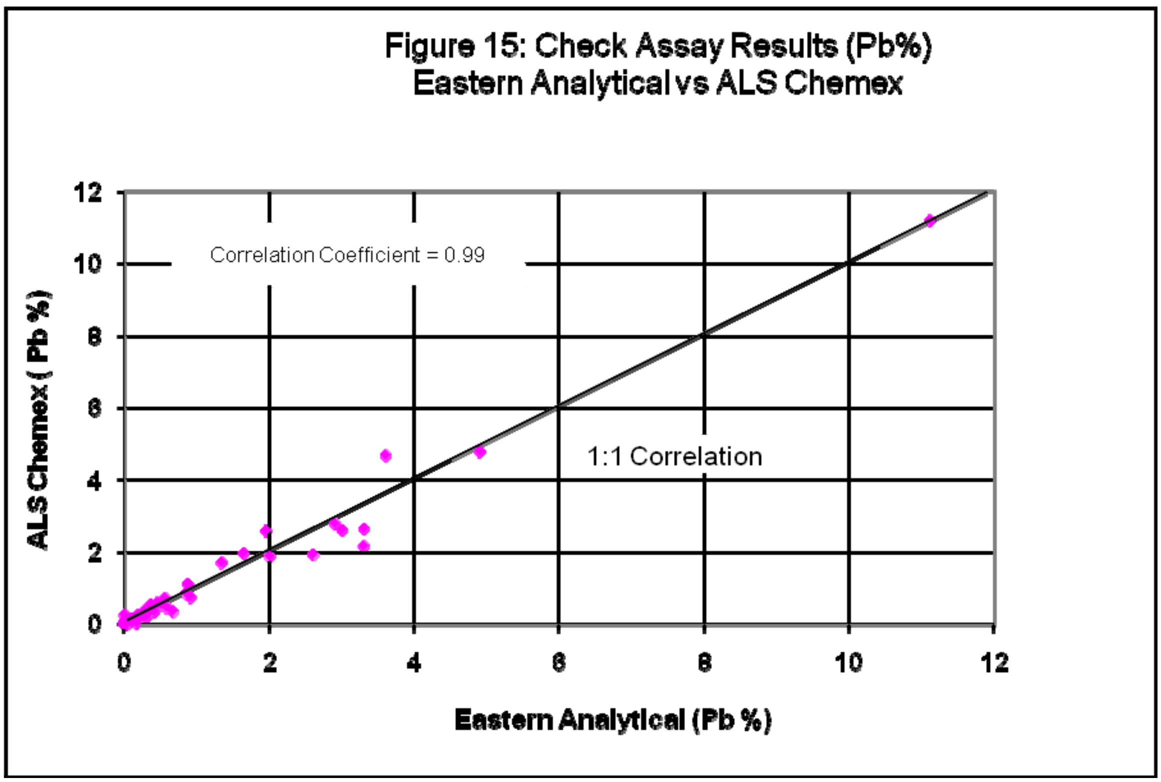

Figure 15: Check Assay Results (Pb%)

13.2.3 Re-sampling of Historic Drill Holes

As noted previously, 10 historic drill holes were twinned and ten additional historic drill holes were re-sampled as part of the Acadian QA/QC program (Table 10).

Table 10: *Listing of Re-sampled and Twinned Historical Drill Holes

Holes Selected For Re-sampling				
GGR-39A	GGR-96	GGR-125	GGR-130	GGR-167
GGR-178	GGR-193	GGR-208	GGR-211	GGR-217
Holes Selected For Twinning				
GGR-190	GGR-215	GGR-227	GGR-169	GGR-183
S-277	GGR-212	GGR-190	GGR-37	GGR-166

**GGR Series by Getty, S-277 by Esso*

Samples of archived drill core were collected by Mercator geologists from the Government of Nova Scotia Stellarton core library during 2007 and 2008. Quarter core samples of the historically half-core sampled carbonate intervals were prepared to ensure that a quarter core portion remained for archival purposes. Sample handling, lab information and analytical procedures were as outlined previously in this report. In total, 64 quarter core samples of archived core were collected from the ten re-sampled drill holes and submitted for analysis. Re-sample intervals were established as closely as possible to original intervals recorded in Getty drill logs. Figures 17 and 18 present lead and zinc results for the two sample sets and show that while variation exists, the majority of pairs are distributed evenly about the 1:1 correlation lines. Correlation coefficients of 0.93 (93%) for zinc and 0.94 (94%) for lead indicate that reasonable correlation exists between the two data sets.

Several factors contribute to the correlation patterns illustrated in Figures 16 and 17, prominent of which are (1) distribution heterogeneity of mineralization within sample intervals, (2) laboratory analysis and sample preparation differences, (3) inaccurate location of re-sample intervals due to core tag location changes in the archived core boxes, and (4) transfer and mixing of core fragments in historic core boxes due to handling and transportation histories. The last factor listed may be especially significant, since much of the re-sampled material consisted of small pieces of half core and core fragments.

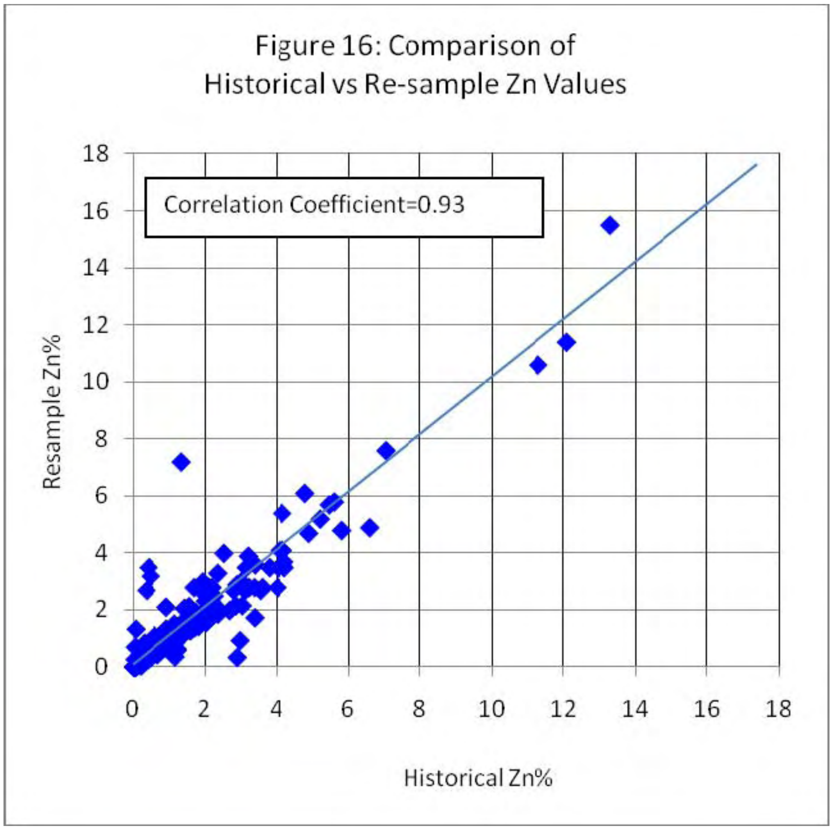

Figure 16: Comparison of Historical vs Re-sample Zn Values

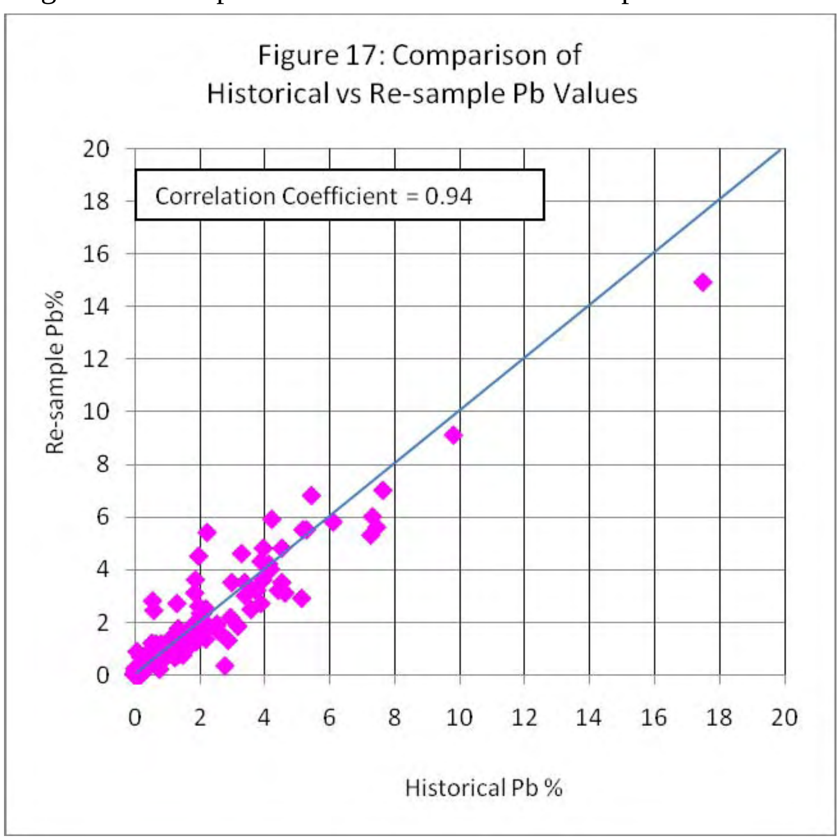

Figure 17: Comparison of Historical vs Re-sample Pb Values

Kennedy (2008 – see Appendix 2) discussed two of the check sample intervals showing strong variation, these being from drill hole GGR 211 (intervals: 27.40m to 28.93m and 30.45m to 31.97m). The historical and Eastern resample values are very similar, while corresponding check sample results from ALS are very low. In both instances, mis-labelling of the check sample split material appears to have occurred. All other check sample results for the data set returned values comparable to those from Eastern and from the original logs.

13.2.4 Twinning of Historic Drill Holes

The ten holes identified above in Table 11 were re-drilled during the 2008-2009 Acadian drilling program to assess collar locations, lithologies and assays of the historical database against results recorded in the project database that supports the resource block model. These holes were continuously sampled through the carbonate and basal breccia intervals using a nominal 1.0 meter sample length. Half core samples from the twin holes were split at the Acadian core logging facility at Scotia Mine and then placed in pre-numbered plastic sample bags along with a corresponding paper sample tag, the number of which was recorded in the core log and sample record logs for the drill hole. After insertion of quality control samples, including blanks and standards, all bagged samples were checked for sequence, placed in sealed plastic buckets and shipped to Eastern Analytical in Newfoundland for analysis according to the standard project protocol.

Table 11 presents a summary comparison of lithologic and weighted average core sample analytical results for twin holes and their original Getty-era equivalents. The Acadian holes show generally good correlation with respect to logged lithology from overburden interface depth through both the dolostone sequence. However, exceptions are present, the most significant being Hole S1043, a twin of historic hole GGR-215. This hole returned a similar dolostone thickness to the original hole but a lower overall grade for combined Zn + Pb. The twin hole was presumed to have been drilled approximately 10 meters from the historic collar location and this factor could alone account for the grade and lithological thickness differences noted above, but it is also possible that a larger discrepancy exists between the actual historic hole location and that recorded in the database. Hole pairs GGR-169 and S1122, GGR-166 and S1126, and GGR-37 and S1059 all showed discrepancies in dolostone thicknesses of 5 meters or greater, which may in part be explained by slight shifts in relative collar locations on the bank slope. It is probable that much of the cored dolostone variation between holes reflects differences in depths to which casing was set in the two programs, since dolostone is the first bedrock lithology encountered below overburden in much of the deposit area.

Table 11: Lithology and Weighted Averages for Historic and Twin Drill Holes

*Historic Hole	Lithology	Zn% +Pb% Weighted Average	Acadian Twin Hole (2007-08)	Lithology	Zn% +Pb% Weighted Average
GGR-190	Dolostone 7.93m	1.13 % over 30.99m	S1021	Dolostone 8.45m	0.82% over 27.50m
GGR-215	Dolostone 3.29 m	5.40% over 3.29m	S1043	Dolostone/ breccia 3.4m	10.52% over 3.4m
GGR-227	Dolostone 27.43m	0.82% over 30.99m	S1116	Dolostone 26.5m	0.82% over 27.50m
GGR-169	Dolostone 5.18m	1.15% over 2.68m	S1122	Dolostone 10.85m	2.09% over 2.5m
GGR-183	Dolostone 35.21m	4.28% over 23.17m	S1124	Dolostone 33.15m	2.55% over 21.6m
GGR-166	Dolostone 14.05m	1.45% over 16.8m	S1126	Dolostone 20.0m	1.48% over 7m
GGR-37	Dolostone 53.88m	3.4% over 22.38m	S1059	Dolostone 27.85m	3.14% over 22.5m
GGR-190	Dolostone 8.39m	Trace	S1021	Dolostone 10.6m	Trace
S277	Dolostone 2.4m	Trace	S1084	Dolostone 1.1m	Trace

** See Table 12 for tenth twin hole*

Assay values for recovered dolostone intervals for these twinned holes are comparable and fall within the low to moderate grade range.

In addition to the above, archived core from historic hole GGR-212 was re-logged due to lack of an original log and associated assay entries. The hole was also subsequently twinned and results of both re-logging and twinning are presented in Table 12, along with a comparison of visual estimates of lead and zinc mineralization. Notably, assay values for the hole were recorded in the Westminer database referenced by Hudgins and Lamb (1991), but associated support documents were not located by Mercator.

In summary, assay results for the ten re-sampled Getty drill holes indicate acceptable correlation between historical and re-sampled values and support correlation

Table 12: Re-logging and Twin Hole Comparison for Historic Hole GGR-212

Lithology and Assay Comparison			
Lithology	**Historic Hole GGR-212**	**Re-log of GGR-212**	**Twin Hole S1025**
Overburden	0.0 – 28.96 m	0.0– 28.80 m	0.0- 25.10 m
Dolomite	28.96–54.25 m	28.80–56.30 m	25.10m–58.4m
Greywacke		56.30–58.20 m	58.4– 62.00 m
Re-log of GGR-212 Visual % Estimation of Mineralization		**Twin Hole S1025 Visual Estimation of Mineralization**	
48.2-48.9 m: Trace Sphalerite		48.2-48.9 m: Trace Sphalerite	
48.9-50.9 m: 1% Sphalerite		48.9-50.9 m: 1% Sphalerite	
50.9-52.7 m: 3% Sphalerite, 1% Galena		50.9-52.7 m: 3% Sphalerite, 1% Galena	
52.7-56.3 m: 0.5% Sphalerite		52.7-56.3 m: 0.5% Sphalerite	
		56.1-58.4 m: 2% Sphalerite, 0,5% Galena	

coefficients of 0.93 (93%) for zinc and 0.94 (94%) for lead. The ten Acadian holes completed as twins to earlier Getty holes show generally good correlation with respect to logged bedrock geology but weighted average zinc and lead values show greater variability. Inconsistencies in the grade and unit thickness parameters are interpreted to reflect several potential factors, the most prominent of which are believed to be (1) slight historic hole location errors and (2) differential drilling and casing procedures between drilling programs in areas of deep overburden (>25 meters thickness).

Combined results of the Getty drill hole re-sampling and twin hole programs by Acadian generally support the earlier conclusion of Cullen et al. (2008), based on a smaller data set, that validated historic drilling information represented in Acadian's Getty deposit database is of acceptable quality for resource estimation purposes.

14.0 Adjacent Properties

Acadian's Scotia Mine complex adjoins the Getty property to the east and drilling results clearly show that the Getty deposit occurs as a contiguous extension of the carbonate bank complex that hosts zinc-lead mineralization at Scotia Mine. At the effective date of this report no mining was taking place at the Scotia Mine deposit. Roy et. al. (2006) reported in detail on mine reserves as well as feasibility study results. All Scotia Mine reserves were compliant with both the CIMM Standards and NI 43-101 and Acadian disclosed that mill throughput had reached an average of 2,000 tonnes per day during the last quarter of 2007, primarily processing low grade ore from initially developed areas of the mine. A mine life of 6 years for open pit production followed by slightly over 2 years of underground production from the deposit's Northeast Zone is represented in the feasibility study.

Table 13: Roy et. al. (2006) Scotia Mine Reserves: Effective July 13, 2006

Category	Type	Tonnes	Zinc %	Lead %
Proven	Surface	1,750,000	3.2	1.3
Probable	Surface	1,690,000	2.5	1.0
	Underground	1,150,000	5.7	3.2
	Subtotal	2,840,000	3.8	1.9
Total Proven + Probable	Surface and Underground	4,590,000	3.6	1.7

Notes: (1) 0.75% zinc equivalent cutoff; 15% dilution and 90% mining recovery; zinc equivalent = zinc% + (0.43 x lead %) (2) Estimate is NI 43-101 compliant

Acadian mined the Main Zone deposit by open pit methods during 2007 and 2008 at which time the operation was shut down. In April 2011 Minetech International Ltd. provided an updated NI 43-101 compliant mineral resource estimate for the Scotia Mine Main Zone and Northeast Zone deposits that was press released by Selwyn on April 6, 2011 (Selwyn, 2011)(Table 14, 15).

Table 14: Main Zone Mineral Resource Estimate (Selwyn, 2011)

Resource Category	Zn Eq. % Cutoff	Tonnes	Zn (%)	Pb (%)	Zn Eq. %
Measured	0.75	1,340,000	4.40	2.00	7.40
Indicated	0.75	1,790,000	3.60	1.60	5.90
Measured + Indicated	0.75	3,130,000	3.90	1.80	6.60
Inferred	0.75	1,740,000	3.10	1.10	4.80
Measured	1.50*	1,250,000	4.70	2.10	7.90
Indicated	1.50*	1,640,000	3.80	1.70	6.40
Measured + Indicated	1.50*	2,890,000	4.20	1.90	7.00
Inferred	1.50*	1,570,000	3.30	1.30	5.20
Measured	2.00	1,170,000	4.90	2.30	8.30
Indicated	2.00	1,500,000	4.00	1.90	6.80
Measured + Indicated	2.00	2,670,000	4.40	2.00	7.40
Inferred	2.00	1,340,000	3.50	1.40	5.60
Measured	7.00	540,000	7.40	3.70	12.90
Indicated	7.00	550,000	6.10	3.50	11.40
Measured + Indicated	7.00	1,090,000	6.80	3.60	12.20
Inferred	7.00	340,000	5.60	3.30	10.60

Notes:

1. A three dimensional block model was developed using Gemcom Surpac® Version 6.0.3 software

2. Cut-off grade for mineralized zone interpretation was 2% zinc-equivalent for the "low-grade" domain and 7% for the "high-grade" domain.
3. Block cut-off grade for defining Mineral Resources was 0.75% zinc-equivalent.
4. No top-cut grade was used. In the author's opinion, the use of a top cut would not have significantly affected the results.
5. Zinc price was $US 1.10 per lb, lead price was $US 1.15 per lb. Prices were based on current and going-forward LME contract prices.
6. Zones extended up to 50 metres down-dip from last intercept. Along strike, zones extended halfway to the next cross-section.
7. Minimum width was 2 metres.
8. Non-diluted.
9. Mineral resources that are not mineral reserves do not have demonstrated economic viability
10. Main Zone mineral resource estimate prepared by Tim Carew, M.Sc., P.Geo. ; base case denoted by “*”.
11. Specific gravity was calculated based on zinc and lead content. There are no other sulphides or dense minerals that are present in significant quantities.
12. Block kriging using "unfolding" was used for estimating block grades.
13. No mineral reserves of any category were identified and were outside the parameters this study.
14. Zinc-equivalency for lead was calculated based on relative metal prices, demonstrated .
15. Processing recoveries (86% & 84 % for lead and zinc, respectively), estimated smelter returns of 95% & 85 % respectively for lead and zinc) and demonstrated concentration factors (75% & 65% respectively for lead and zinc).

Table 15: Northeast Zone Mineral Resource Estimate (Selwyn, 2011)

Resource Category	**Zn Eq. % Cutoff**	**Tonnes**	**Zn (%)**	**Pb (%)**	**Zn Eq. %**
Indicated	2.00*	1,580,000	4.21	2.22	7.53
Inferred	2.00*	1,880,000	2.70	1.86	5.48

Notes:

1. Cut-off grade for mineralised zone interpretation was 0.5% zinc-equivalent for surface resources (less than 100 metres deep) and 2% at depth.
2. Block cut-off grade for defining Mineral Resources was 0.75% zinc-equivalent for surface resources (less than 100 metres deep) and 2% at depth.
3. No top-cut grade was used. In the author's opinion, the use of a top cut would not have significantly affected the results.
4. Zinc price was $US 1.10 per lb, lead price was $US 1.15 per lb. Prices were based on current and going-forward LME contract prices
5. Zones extended up to 50 metres down-dip from last intercept.
6. Along strike, zones extended halfway to the next cross-section.
7. Minimum width was 2 metres.
8. Non-diluted.
9. Mineral resources that are not mineral reserves do not have demonstrated economic viability.
10. Mineral resource estimate prepared by Doug Roy, M.A.Sc., P.Eng.; base case denoted by “*”.
11. Specific gravity was calculated based on zinc and lead content. There are no other sulphides or dense minerals that are present in significant quantities.
12. Inverse distance weighting, power of "2" ("ID2") was used for estimating block grades.
13. Indicated mineral resources identified where sample intercept spacing was 40 metres or less (based on variography).
14. No Measured mineral resources or mineral reserves of any category were identified.
15. Zinc-equivalency for lead was calculated based on relative metal prices, demonstrated processing recoveries (86% & 84 % for lead and zinc, respectively), estimated smelter returns 95% & 85 % for lead and zinc) and demonstrated concentration factors (75% & 65% for lead and zinc).

The Getty deposit is located 1700 meters west of the Scotia Mine mill and zinc-lead mineralization hosted by carbonate bank dolomite has been shown through drilling to be present continuously in the sub-surface between the two deposits. However, comparison of Scotia Mine reserve and resource figures with Getty deposit resource figures presented in this report shows that substantially higher metal grades are present at Scotia Mine.

Approximately 1.5 kilometres to the southwest of the Getty deposit, on adjacent exploration claims also held by Acadian, the Carrolls Farm zinc-lead prospect was recently discovered by Acadian in dolomitized carbonate bank lithologies. The historic Carrolls Corner zinc–lead prospect occurs in a comparable geological setting 700 meters further to the west and in combination, these may reflect a continuously mineralized trend extending from Scotia Mine, through the Getty deposit and then to the Carrolls Farm and Carrolls Corner areas. The latter two areas have not been investigated in detail and do not have associated mineral resources. However, they present good potential for future delineation of mineral resources and require additional investigation.

15.0 Mineral Processing and Metallurgical Testing

No mineral processing or metallurgical studies have been carried out to date by Selwyn or Acadian on Getty deposit material and no historic studies are known to the authors. However, similarity of this deposit to that at Scotia Mine is well documented and metallurgical similarities can be assumed for purposes of general discussion. Roy et al. (2006) present results of metallurgical studies completed on the Scotia Mine deposit and these are relevant as guides with respect to the Getty deposit. At Scotia Mine lead and zinc are recovered by conventional flotation methods after crushing and grinding, with average historic recoveries of 90% for zinc at a concentrate grade of 60% zinc and 95% for lead at a concentrate of 75% lead (Roy et. al 2006).

16.0 Mineral Resource and Mineral Reserve Estimates

16.1 General

The definition of mineral resource and associated mineral resource categories used in this report are those recognized under National Instrument 43-101 and set out in the Canadian Institute of Mining, Metallurgy and Petroleum Standards on Mineral Resources and Reserves *Definitions and Guidelines* (the CIMM Standards). Assumptions, metal threshold parameters and deposit modeling methodologies associated with the current Getty resource estimate are discussed below in report sections 16.2 through 16.4.

16.2 Geological Interpretation Used In Resource Estimation

All areas of zinc-lead mineralization included in the current resource are restricted to the Getty deposit carbonate bank and occur within dolomitized Gays River Formation lithologies. For resource model purposes the Getty deposit is considered an extension of the adjacent Scotia Mine deposit and both are classified as carbonate-hosted, stratabound zinc-lead deposits of the Mississippi Valley Type (MVT). Mineralization is localized in carbonate bank lithofacies that developed above and around paleo-topographic basement highs comprised of Cambro-Ordovician Goldenville Formation greywacke and slate. By definition, Gays River Formation lithologies are laterally equivalent to laminated and thin bedded limestones of the Macumber Formation.

Zinc and lead mineralization of economic proportions is exclusively developed within dolomitized carbonate bank lithologies at Getty and is considered directly comparable to that seen on the adjacent Scotia Mine property. Sphalerite and galena are the dominant sulphide minerals present but trace amounts of marcasite/pyrite occur locally, typically as cavity-lining phases that post-date the zinc-lead mineralizing stage. Silver does not occur in economic proportions in this district but does report to Scotia Mine concentrates at levels of about one ounce per tonne. A similar presence at Getty may exist. Barite is absent from the deposit, as is celestite, but traces of fluorite have been reported (Kontak, 1998, 2000; Sangster et. al., 1998).

As noted earlier, several types of lead and zinc mineralization are represented in the related Scotia Mine and Getty deposits, the most important of which are (1) submassive to massive replacements of carbonate bank lithofacies by sphalerite and galena, typically along steeply dipping carbonate bank front intervals that face the open paleo-basin, (2) disseminated, replacement and porosity filling phases within various carbonate bank lithologies adjacent to and within bank-front intervals, and (3) in rare vein and irregular vug settings or as matrix mineralization between greywacke clasts or boulders in a basal breccia unit that typically separates carbonate bank lithologies from basement greywacke. The dominant type of mineralization in the Getty deposit is disseminated in nature.

16.3 Methodology of Resource Estimation

16.3.1 Overview of 2011 Estimation Procedure

The Getty mineral resource estimate is based on a three dimensional block model developed using Surpac © Version 6.0.3 modeling software and the validated project drill hole database. The database includes results from 181 historic diamond drill holes completed by Getty as well as 4 holes completed by Esso and 138 diamond drill holes completed by Acadian in 2007-2008. The current resource outline includes 84 historic holes and 94 Acadian holes, although additional holes from both sources occur adjacent to the outline and were used for geological and block model peripheral constraint definition purposes.

The first step in development of the resource model was creation of a set of interpreted geological cross sections presenting lithocoded rock types interpreted from drill logs as well as lead and zinc core sample assay interval data. These served to establish an understanding of carbonate bank geometry and grade distribution trends present in the deposit and were later augmented by contour plans depicting overburden depth, dolomite thickness and basement surface configurations. Sections were created using the local project grid at a nominal spacing of 50 meters, with adjustment of this spacing made as necessary to provide complete coverage of the deposit. Geological and grade distribution models developed from the sections were used to guide and assess subsequently developed versions of the three-dimensional block model.

Assay results from the validated project database were initially assessed through calculation of distribution statistics for both zinc and lead populations after compositing to a common 1.0 meter support base. In total, 1672 composites were created from analytical results for 1794 original core samples. Frequency distribution and probability plots for the composite data set were also prepared and results were interpreted as showing that the few high grade samples present were reflections of valid mineralization styles for which block-scale correlations could be reasonably expected. This assertion reflects observations made during underground mining of high grade portions of the adjacent Scotia Mine deposit. Composites showing high zinc and lead grades occur in several areas along the north-facing bank front of the Getty deposit, as is the case at Scotia Mine, but these are typically lower in grade, thinner and spatially less extensive than similar high grade areas at Scotia Mine. On the basis of combined factors, no requirement for high grade capping of assay results in the Getty data set was established.

The Getty deposit model was developed within a three-dimensional, peripheral constraint (or solid) created in Gemcom Surpac® Version 6.0.3 initially based on a combination of two contributing parameters, these being (1) a minimum grade % (zinc plus lead) value of 1.00% with a minimum down-hole intercept length of 3.0 meters, and (2) lateral limits to the deposit solid defined on the basis of midpoints between mineralized and non-mineralized drill holes or a maximum 25 meter projection from a mineralized hole where no other constraining hole was present. The grade cut-off was assigned as a reflection of the deposit's near-surface location and associated potential for open pit development.

While not as complex as that at Scotia Mine, the carbonate bank front configuration at Getty is irregular and the solid developed for deposit modelling purposes is characterised by numerous promontories and re-entrants. This is particularly true along north-facing bank front intervals that show spatial association with areas of best zinc and lead mineralization. This configuration approximates a series of variably-oriented panels of dipping mineralization that, although correlative, show strike and dip changes along the length of the deposit. The current peripheral deposit constraint solid for the block model reflects this variation and is based on that developed for the earlier Acadian resource estimate (Cullen et al., 2007). However, it differs from the earlier constraint by accommodating the new drill holes by Acadian and being comprised of 26 sub-domains reflecting areas of common mineralized zone orientation. As detailed later in this report, block grade interpolation was separately carried out in each sub-domain using unique search ellipse orientations.

Spatial variability of mineralized zone trends at Getty prevented development of experimental variograms for the lead and zinc data set that reflected continuity of the mineralized zone to the degree seen in the original geological cross section model. This issue was addressed by Roy et al. (2006) at the Scotia Mine deposit through three-dimensional transformation of their deposit model that "unfolded" the various mineralized segments to a common surface. Transformed data supported acceptable variogram models and these were subsequently used to establish parameters for grade interpolation into their block model.

In contrast to the method used at Scotia Mine, mineralized trend variability along the Getty deposit was addressed in the current model through development of the 26 orientation domain solids within which grade interpolation was constrained. Composite populations within individual domains typically did not provide an adequate number of sample pairs to create well developed experimental variograms. However, useful variogram models for the largest northwest trending sub-domain were initially developed and these were augmented by variogram models calculated for the entire composite population occurring within the peripheral deposit constraint. In the latter case it was recognized that geometric aspects of the deposit could factor negatively in the evaluative process. Based on combined results of the two approaches, the strike and dip directions of the mineralized zones were determined to show the highest degrees of grade correlation at longest range values. This directly supported earlier qualitative geological assessment of the grade trends. Geometric aspects of the mineralized zones were used in conjunction with variogram results to select interpolation ellipse axial ranges, with common ranges used in all sub-domains in conjunction with unique assigned orientation parameters. Block grades were assigned to the 26 deposit sub-domains using inverse distance squared (ID^2) interpolation methodology.

Results of the grade interpolation process were initially checked against geological cross sections to assess conformity and to provide primary validation of the final deposit block model. A further check on the resource model was completed using Nearest Neighbour grade interpolation methodology on the deposit solid. Resource figures reflecting ID2 interpolation and a range of minimum grade cutoff values, beginning at 2.0% (zinc + lead), constitute the final resource estimate documented in this report.

Report subsections 16.3.2 through 16.3.10 below provide specific additional information regarding estimation procedures and parameters summarized above.

16.3.2 Capping of High Grade Assay Values

Zinc and lead grades for all drill core samples were reviewed and descriptive statistics calculated for both the raw data set and that reflecting 1 meter composite support. The latter are presented below in Table 16 and include only those holes that intercept the deposit solid. Distribution and probability plots were also prepared for this data set and are included in Appendix 3 along with similar plots for the block model.

Table 16: Descriptive Statistics: 1 Meter Drill Core Composites In Resource Solid

Parameter	**Zinc**	**Lead**
Mean	1.46%	1.00%
Variance	1.94	2.53
Standard Deviation	1.39	1.59
Coefficient of Variation	0.948	1.580
Maximum	11.30	18.54
Minimum	0.00	0.00
Number	1961	1961

Maximum zinc and lead grades at 1 meter composite support are 11.30% and 18.54% respectively and reflect zones of higher grade mineralization that are considered spatially coherent and correlative at block scale within the deposit. These form a meaningful part of the grade distribution spectrum of the deposit and are associated with valid geological domains. On this basis, high grade lead and zinc values were not capped for use in the current resource estimate.

16.3.3 Compositing of Drill Hole Data

One meter down-hole composites of raw core sample assay values were created for each drill hole, with this length representing the dominant sample interval used by Acadian in the 2007-2008 drilling program. Historic drilling program sample length statistics for all holes are presented in Table 17. A review of associated rank and percentile figures shows that 99 percent of the historic samples measure less than 2.0 meters in length, 75 percent measure 1.52 meters or less in length and 39 percent measure less than 1.0 meter in length. Average length of historic samples is 1.15 meters.

Table 17: Core Sample Length Descriptive Statistics

Parameter	**Historic Core Sample Length (m)**	**Acadian Core Sample Length (m)**
Mean	1.15	1.00
Variance	0.222	0.063
Standard Deviation	0.47	0.25
Coefficient of Variation	0.411	0.250
Maximum	4.26	6
Minimum	0.02	0.38
Number	855	939

With respect to Acadian sampling, associated rank and percentile figures show that 95 percent of samples measure 1.0 meter or less in length and 99% of samples measure 2.0 meters or less in length in length. Average length of Acadian core samples is 1.00 meters. Sampling of high grade intervals in historic drill holes was typically carried out based on geological contacts with no minimum sample length parameters applied. This may in part be reflected in samples from historic programs with lengths of less than 0.5 meters.

In total, 1672 assay composites at 1.0 meter support were calculated within the resource estimation solids from the combined historic drill hole and Acadian drill hole data set. A listing of these composites plus calculated sub-samples that occur within the solid is included in Appendix 3, along with a listing of intercepts used in the Nearest Neighbour interpolation check model.

16.3.4 Calculation of Equivalent Zinc

The previous Mercator resource estimate for the Getty deposit reported by Cullen et al. (2008) presented a zinc equivalent parameter of zinc equivalent = (zinc% + lead %). Riddell (1976) also used a zinc% + lead% factor to define resource cutoff values and included the parameter in the associated resource estimate. Use of zinc% + lead% to define cutoff values was not retained for the current estimate.

Market conditions at the effective date of this report have changed since the 2008 resource estimate. Based on (1) review of London Metal Exchange 27 month forward contract pricing for lead and zinc, (2) consideration of current and future market pricing projections prepared for Selwyn (Brook Hunt, 2010), (3) availability of 2007-2008 milling recovery data from Scotia Mine, and (4) provision of relevant smelter return factors, the authors have chosen to redefine zinc equivalent for current purposes. Zinc Equivalent % (Zn Eq.%) for this report is defined as Zn % + (Pb % x 1.18), based on mill recoveries of 89.3% for zinc and 89.5% for lead, $US1.10/lb Zn and $US1.15/lb Pb metal pricing and smelter returns of 85% for Zn and 95% for Pb. A 2.00% Zn Eq. resource statement cutoff value was used and reflects open pit development potential.

16.3.5 Variography

As reported by Cullen et al. (2008), an initial assessment of variography for the deposit area was carried out for historic drill hole data by creation of experimental variograms for combined zinc plus lead (zinc + lead) values for the largest northwest trending sub-domain of the deposit that corresponds with mineralization developed along the contact between overlying evaporite and extending southwest into the dolomitized bank proper. Further details pertaining to deposit sub-domains are presented below in report section 16.3.6. In plan projection the selected sub-domain measures approximately 700 meters in length by 200 meters in average width and forms a broad corridor of northwest striking, flat-lying to northeast-dipping mineralized carbonate that shows restriction of most mineralization to a relatively narrow, 150 meter elevation interval. Local irregularities of the mineralized carbonate’s trend are present in this corridor and take the form of promontories and re-entrants that have associated variations in strike and dip components.

Experimental variograms for the selected sub-domain were calculated at various lags and bearings within a horizontal reference plane and resulted in selection of spherical variogram models for major and semi-major axes of continuity in orientations that correspond to the dominant geological strike and dip directions within the sub-domain. Representative variogram models for these two axial components are presented in Figures 18 and 19 and show ranges of 75 meters and 100 meters respectively. Experimental variograms were also calculated in the same horizontal reference plane for the entire composite data set occurring within the deposit peripheral constraint and these provided definition of spherical variogram models showing similar major and semi-major axis orientations as those calculated for the northwest sub-domain, but with higher degrees of complexity resulting from combination of data from the various orientation sub-domains present within the deposit. Selected examples of variogram models based on the entire deposit data set are included in Appendix 3.

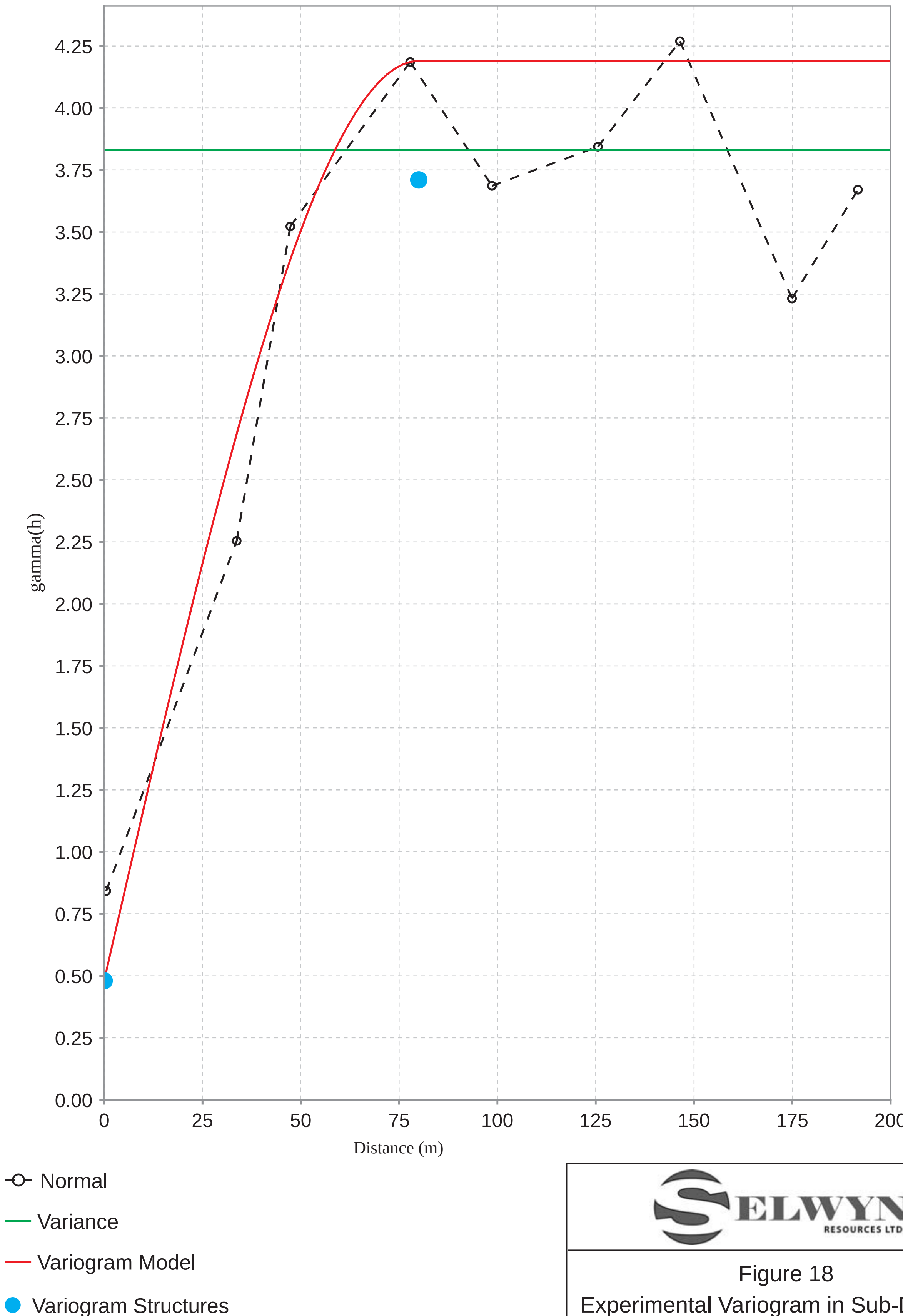

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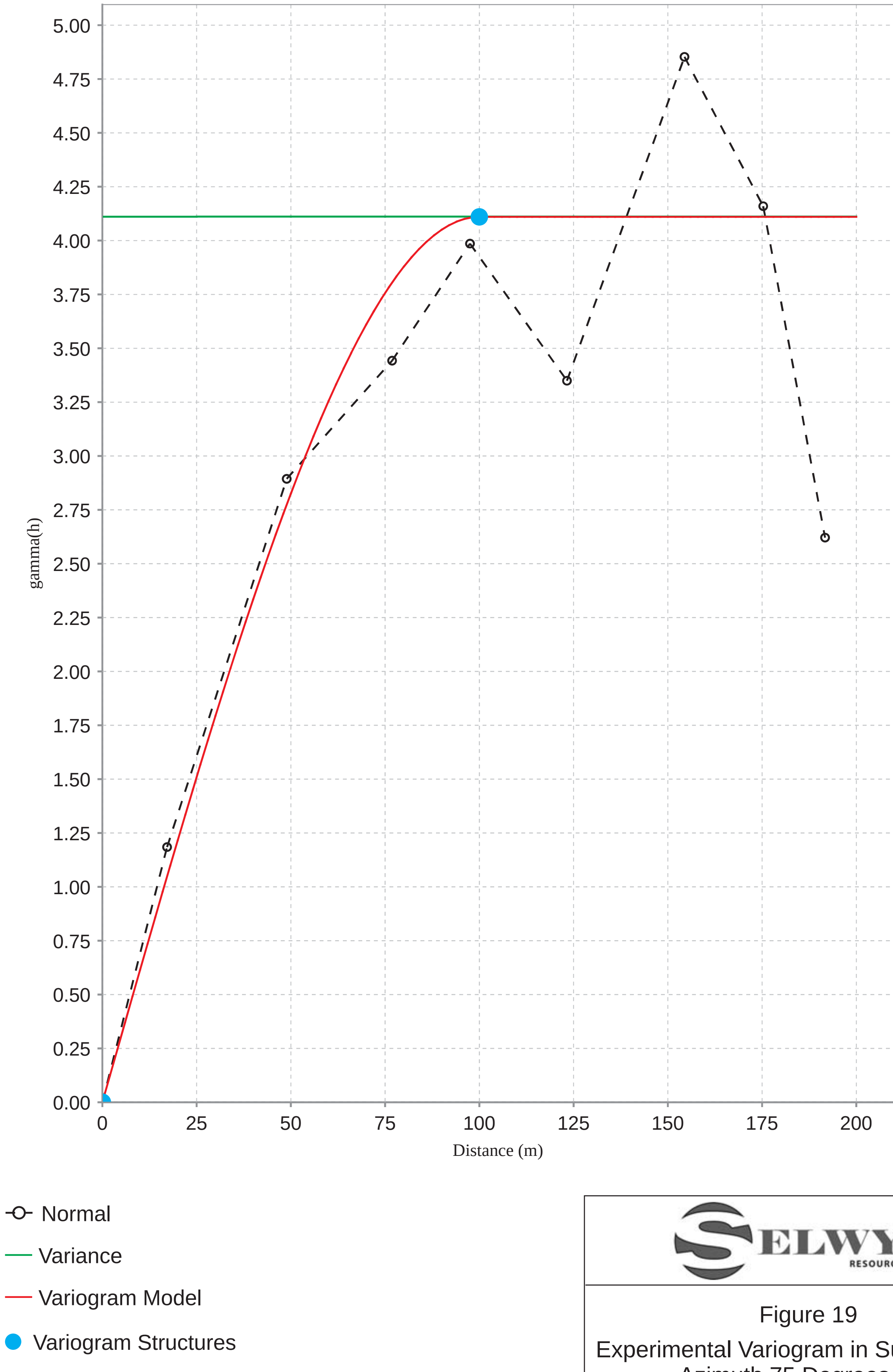
Figure 18
Experimental Variogram in Sub-Domain 1
Azimuth 150 Degrees Grid
Getty Deposit

Date: April 2011

mercator GEOLOGICAL SERVICES



SELWYN RESOURCES LTD.

Figure 19

Experimental Variogram in Sub-Domain 1
Azimuth 75 Degrees Grid
Getty Deposit

Date: April 2011

mercator GEOLOGICAL SERVICES

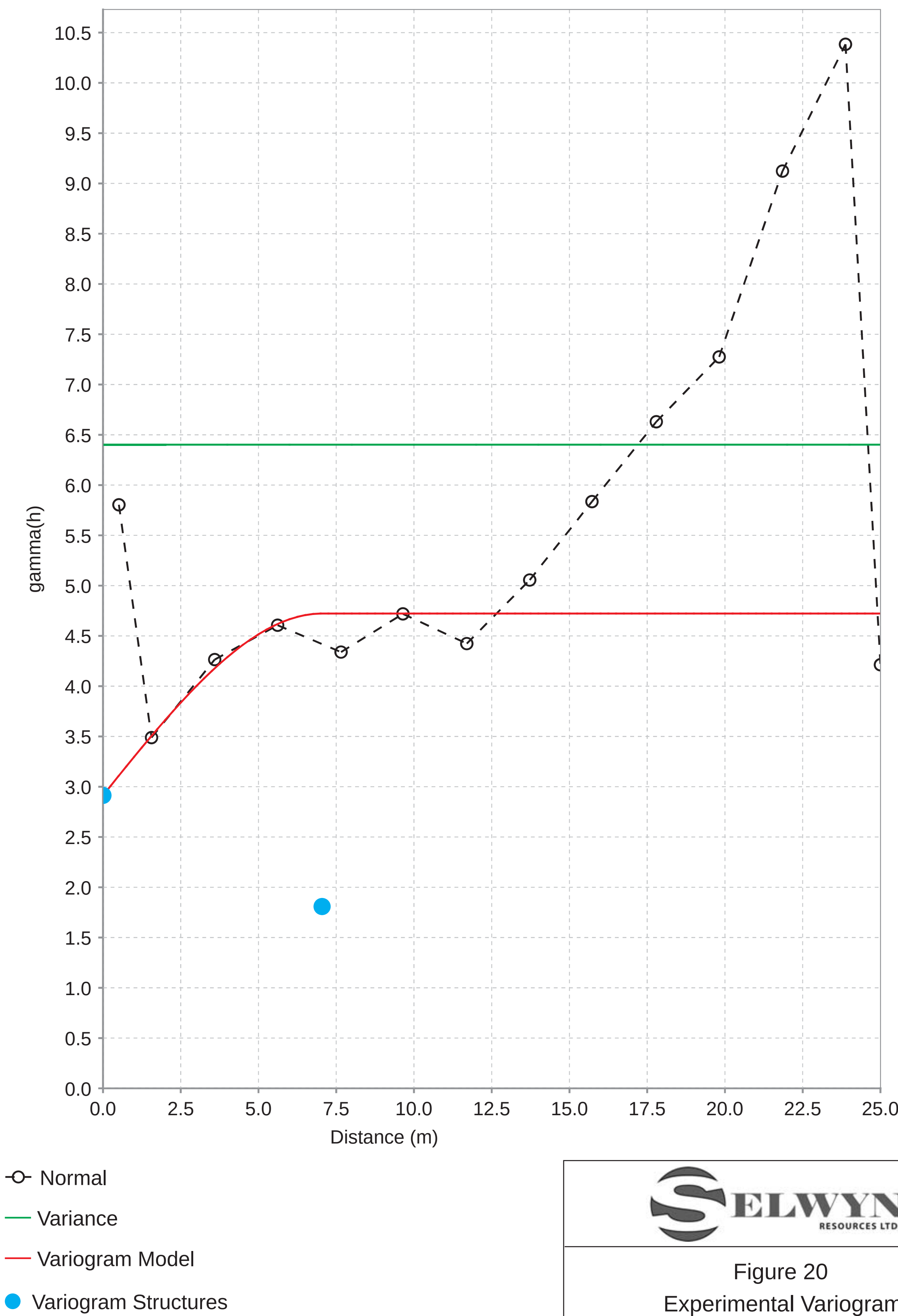


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Figure 20
Experimental Variogram
Downhole
Getty Deposit

Date: April 2011

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Down hole experimental variograms and spherical model variograms were also prepared to assess grade continuity and correlation trends vertically within the dolostone unit that hosts the deposit. Figure 20 presents the best resulting down-hole variogram model and supports a range of 7.5 meters at a lag of 2 meters. This range is interpreted as reflecting the average mineralized thickness of the host carbonate within the deposit peripheral constraint and was considered during selection of a minor axis range value for the grade interpolation search ellipse.

Ranges for variograms defined for the main northwest trending sub-domain were assumed to be applicable in the other deposit sub-domains, based on (1) correlation of the modeled continuity trends with local geological strike and dip directions and (2) independent confirmation of grade continuity based on systematic review and interpretation of multiple geological and assay cross sections through the deposit. In combination, these assumptions largely reflect the recognized stratabound character of the zinc and lead mineralization within the Gays River Formation host sequence in the Getty deposit area.

16.3.6 Setup of 2011 Three Dimensional Block Model

Block model total extents were defined in local grid coordinates as being from 6000 meters East to 7145 meters East and from 6300 meters North to 7150 meters North. The model extends in elevation from 150 meters to 700 meters relative to the Scotia Mine local grid that has a datum of mean sea level plus 500.11 meters. The nominal topographic surface in the Getty deposit area occurs between the 550 meter and 520 meter local grid elevations and all resource solids respect the bedrock/overburden surface defined by the resource drill hole data set. As noted earlier, all drill holes in the Getty resource database are coordinated to both the Scotia Mine local grid and to UTM Zone 20 (NAD83) and collar coordinates for the local grid are reported in Appendix 2. The local grid closely reflects the 3º Modified Transverse Mercator (MTM) projection for Nova Scotia (ATS 77 datum) and transformation details appear in Appendix 2.

A standard block size for the model was established at 2.50 meters x 2.50 meters x 2.50 meters, with no sub-blocking. Descretization within blocks was 1 x 1x 1 and no block rotation was applied. The chosen block size reasonably reflects the character of mineralization within the deposit and also provides approximation of a mining unit size that could be applicable in development of this style of base metal deposit.

The major lithologic units incorporated in the deposit geological model were discussed in report section 6.0 and all historic drill holes were lithocoded using the lithocode system originally established by Westminer for the Scotia Mine deposit. This system was also being used in the Getty deposit drilling program by Acadian and a listing of lithocodes and descriptions appears in Appendix 2.

Resource estimation was completely constrained within a peripheral deposit solid developed from wireframing of mineralized envelope limits on geological cross sections cut through the deposit. A minimum 1.0% (zinc + lead) value over a minimum 3.0 meter down hole sample length was used initially to define wire-framed mineralized envelope limits for a peripheral deposit constraint, with slight modifications made locally as required after inspection of the resultant solid. Lateral or down-dip deposit limits were typically created at midpoints between holes that mark the mineralized zone to non-mineralized zone transition or at a distance of 25 meters from a mineralized drill hole, the lesser distance being utilized.

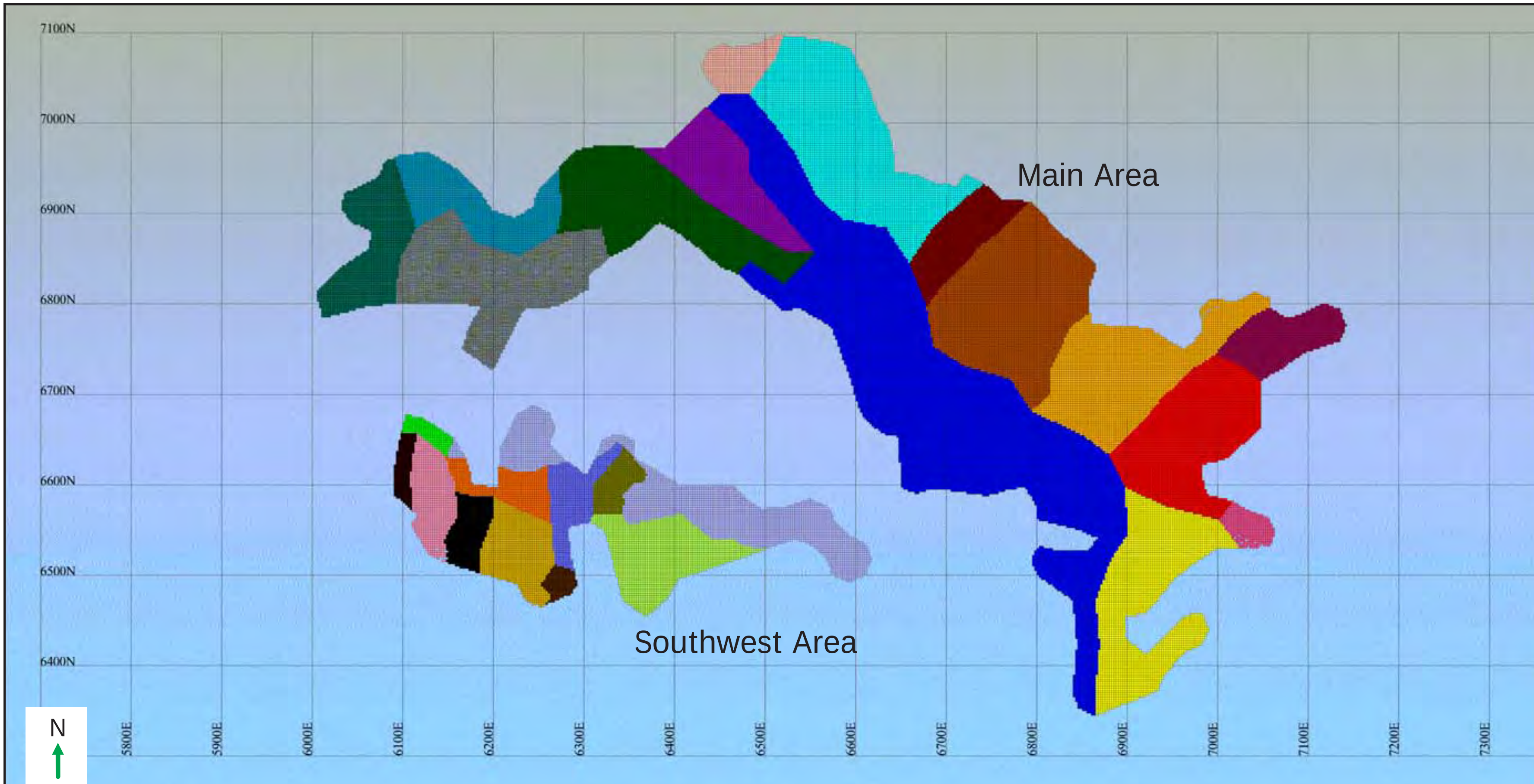
To properly accommodate deposit geometry during modelling, twenty-six grade interpolation sub-domains were established within the block model peripheral constraint and these are illustrated in (Figure 21). Sub-domains reflect areas of common geometric orientation of the mineralized carbonate and were established as discrete three dimensional constraints within which block grade interpolation could be carried out. Contributing composites for block grade interpolation were not constrained within the sub-domains, to ensure that modeling allowed grade continuity to exist across sub-domains boundaries. Fifteen sub-domains occur contiguously within the main northwest trending deposit outline and the remaining 11 occur contiguously within the southwest zone of the deposit that, at the minimum cut-off used in this report, has been modeled as a separate mineralized area immediately adjacent to the main deposit (Figure 21).

16.3.7 Assignment of Resource Estimate Cutoff Values

A minimum cutoff value of 2.0 % zinc equivalent was used for reporting the current mineral resource estimate. This value was selected to reflect recognized potential for open pit development of the deposit and processing of ore at the adjacent Scotia Mine milling complex.

16.3.8 Material Densities

No historic collection of Specific Gravity (SG) data for either the Scotia Mine or Getty deposits was identified in historic records. However, during the course of the 2007-2008 drilling program, Mercator selected 120 dolostone and basal breccia pulp samples representing the grade range within the deposit and submitted these to ALS Chemex in Sudbury, ON for the purpose of Specific Gravity (SG) determination. Pyncometer and methanol laboratory methodology was utilized as set out in the ALS Chemex OA-GRA-



LEGEND

Interpolation Domains with Identifiers

Main Area	Southwest Area
M1	S1
M2	S2
M3	S3
M4	S4
M5	S5
M6	S6
M7	S7
M8	S8
M9	S9
M10	S10
M11	S11
M12	
M13	
M14	
M15	

0 100 200

metres

SELWYN RESOURCES LTD.

Figure 21

Plan View of Getty Deposit
Grade Interpolation Sub-Domains

Date: April 2011

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08b laboratory protocol. Analytical results for zinc and lead had previously been received for all of the samples submitted for SG determination. No porosity factor was used in the specific gravity calculations.

Specific gravity (SG) values for the block model were assigned by calculation based on a base dolostone SG value of 2.82 g/cm3 and application of the formula set out below that assigns SG values based on zinc and lead block grades plus the base dolostone value. Zinc is assumed to be present as sphalerite and lead to be present as galena. This approach is consistent with methodology used for the previous Getty deposit resource estimate by Mercator (Cullen et al., 2008) and follows the earlier example of Minetech International Limited (Roy et al., 2006) for calculation of mineral resources and reserves supporting the recent feasibility study for Acadian's adjacent Scotia Mine project.

The 120 SG determinations from the Acadian drilling program were used to assess the assignment equation and results correlated sufficiently well to maintain its use. However, the equation was modified through increase of the original base dolostone SG value of 2.7 g/cm^3 to 2.82g/cm3. SG values calculated for each block were multiplied by corresponding block volumes and results summed according to applied cutoff parameters to obtain tonnage values for the deposit model. For purpose of review, descriptive statistics for calculated block density values used in the current deposit model are presented in Table 18. A tabulation of SG values for all analysed samples appears in Appendix 3.

Table 18: Descriptive Statistics: Block Model Density Values

Parameter	**Value**
Mean	2.86
Variance	0.001
Standard Deviation	0.028
Coefficient of Variation	0.010
Maximum	3.27
Minimum	2.82
Number	209757

16.3. 9 Interpolation Ellipsoid and Resource Estimation

Inverse Distance Squared (ID^2) grade interpolation was used to assign block model metal grades, with blocks being fully constrained by limits of the 26 separate resource domain solids described earlier in report section 16.3.6. Variogram models, previously discussed in report section 16.3.5, were used in conjunction with geological model attributes to guide assignment of major, semi-major and minor axis range values for interpolation ellipses used in the current model. Unique search ellipse orientation parameters were developed that reflect local geological strike and dip components for mineralized carbonate in each of the 26 interpolation domains and axial orientations were assigned to conform to this geometry.

Major and semi-major axial range values for the ellipsoids were set at 75.00 meters for each domain and in no case exceeded the maximum major and semi-major range values indicated by the selected assay composite variogram models. The 75.00 meter range in both major and semi-major orientations was considered sufficient to insure block grade interpolation from 3 contributing drill holes in a 25 meter spaced drill pattern. Minor axis ranges of 37.5 meters were assigned to ensure full exposure to the thickness of stratabound mineralization within all sub-domains. This value exceeds the down-hole variogram range mentioned above and is fifty percent of the selected major and semi-major axis range values. Minor axis range selection was weighted on the basis of the deposit geological model to ensure inclusion of the full host sequence stratigraphic thickness in all sub-domains. Orientation parameters pertaining to the 26 grade interpolation sub-domains appear in Table 19 and Figure 22 presents a graphic representation of the various search ellipses superimposed on the block model.

Table 19: Search Ellipse Parameters for Interpolation Domains

Interpolation Domain Name	Azimuth (Degrees)	Plunge (Degrees)	Dip (Degrees)
Main 1	0	0	0
Main 2	0	0	0
Main 3	306	-22.5	-33.5
Main 4	306	-20.5	37
Main 5	0	-24	0
Main 6	250	-25	-18
Main 7	295	-33	0
Main 8	47	-31	35
Main 9	36	-20	-27
Main 10	33	-23	-10
Main 11	43	-15	30
Main 12	132	-24	15
Main 13	43	-8.5	-10
Main 14	0	0	0
Main 15	58	23	0
South 1	103	0	0
South 2	90	-5	-31.5
South 3	190	10	-20
South 4	176	26	16
South 5	108	0	-30
South 6	307	0	22
South 7	184	41	4
South 8	180	41	-45
South 9	193	44	7
South 10	194	38	-24
South 11	197	41	42

A maximum of 12 included sample composites was established for estimation of individual block grades, with no more than 4 composites allowed from a single drill hole. These parameters ensured both multiple drill hole inclusion in block grade estimations and lateral grade projection between drill holes in dip and strike orientations. Single passes of ID^2 grade interpolation were separately completed for the zinc and lead data sets within each of the 26 interpolation sub-domains and results were initially reported at grade cut-offs of 1.50%, 2.00%, 2.50% and 3.00% (zinc equivalent).

Grade distribution within the block model was assessed against vertical geological and grade cross sections cut through the deposit at nominal spacings of 50 to 70 meters and also against horizontal sections cut through the model at 10 meter elevation intervals. Metal distribution trends observed in the sections were considered acceptable against the geological model. Figures 23 though 26 present perspective views of block model grade distribution trends at specified cut-off values.

16.3.10 Resource Category Definitions

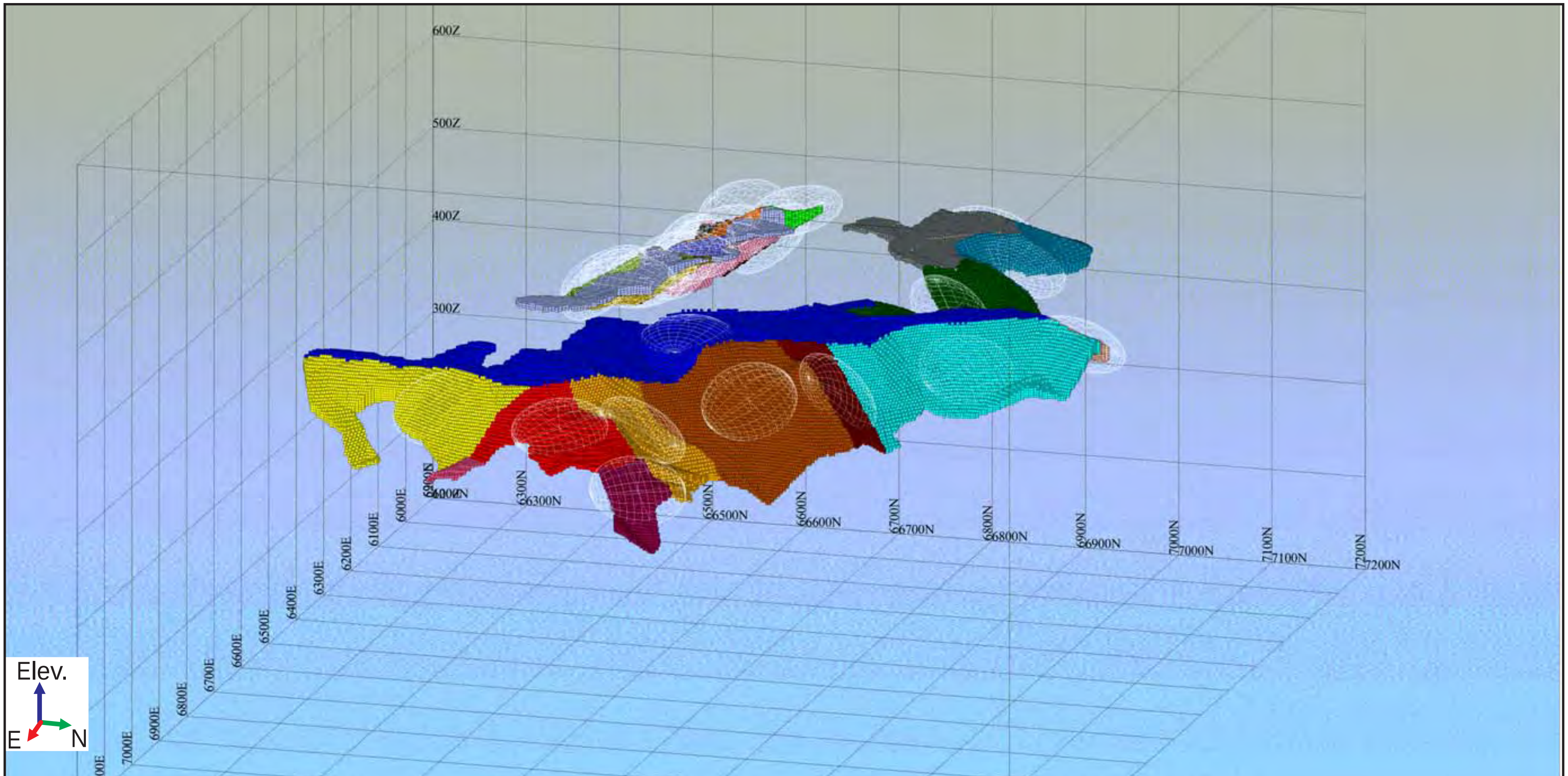
Definitions of mineral resource and associated mineral resource categories used in this report are those recognized under National Instrument 43-101 and set out in the Canadian Institute of Mining, Metallurgy and Petroleum Standards On Mineral Resources and Reserves *Definitions and Guidelines* (the CIMM Standards). These are defined below:

Mineral Resource

A “Mineral Resource” is a concentration or occurrence of natural, solid, inorganic or fossilized organic material in or on the earth’s crust in such form and quantity and of such a grade or quality that it has reasonable prospects for economic extraction. The location, quantity, grade, geological characteristics and continuity of a Mineral Resource are known, estimated or interpreted from specific geological evidence and knowledge.

Inferred Mineral Resource

An “Inferred Mineral Resource” is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics, can be estimated on the basis of geological evidence and limited sampling and reasonably assumed, but not verified, geological and grade continuity. The estimate is based on limited information and sampling gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes.



LEGEND

Interpolation Domains with Identifiers

Main Area	Southwest Area
M1	S1
M2	S2
M3	S3
M4	S4
M5	S5
M6	S6
M7	S7
M8	S8
M9	S9
M10	S10
M11	S11
M12	
M13	
M14	
M15	

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Figure 22
View of Grade Interpolation for Getty Block Model Looking Southwest

Date: April 2011

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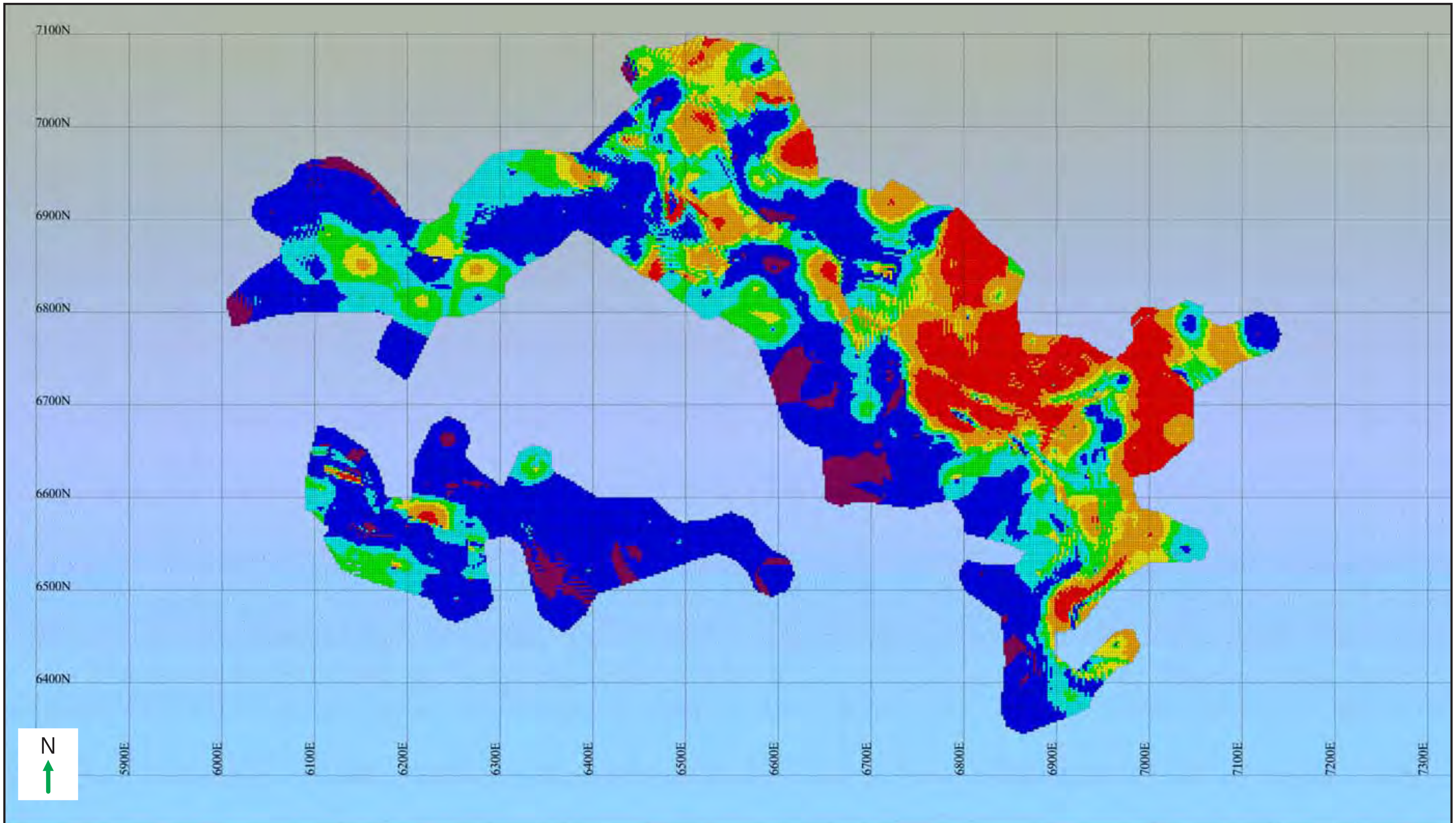

LEGEND

Zn% + Pb% Cut-off

(grey)	Undefined
(purple)	0.01 - 1.00
(blue)	1.00 - 2.00
(cyan)	2.00 - 2.50
(green)	2.50 - 3.00
(yellow)	3.00 - 3.50
(orange)	3.50 - 5.00
(red)	5.00 - 99.00

0 100 200
metres

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Figure 23

Plan View of Getty Deposit Block Model

Date: April 2011

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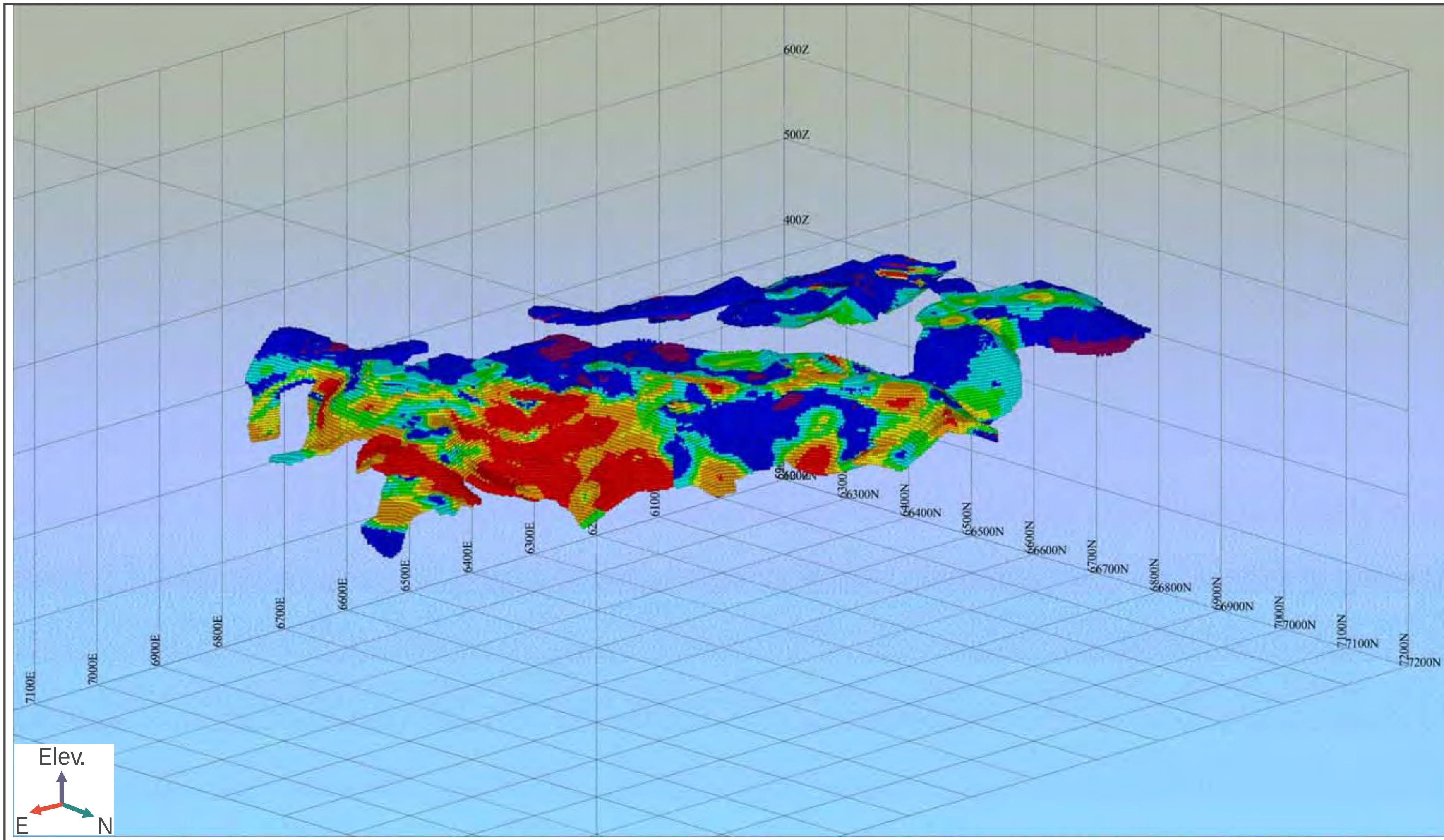

LEGEND

Zn% + Pb% Cut-off

Undefined	
0.01 - 1.00	
1.00 - 2.00	
2.00 - 2.50	
2.50 - 3.00	
3.00 - 3.50	
3.50 - 5.00	
5.00 - 99.00	

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Figure 24
Perspective View of Getty Deposit
Grade Distribution
Looking Southwest

Date: April 2011

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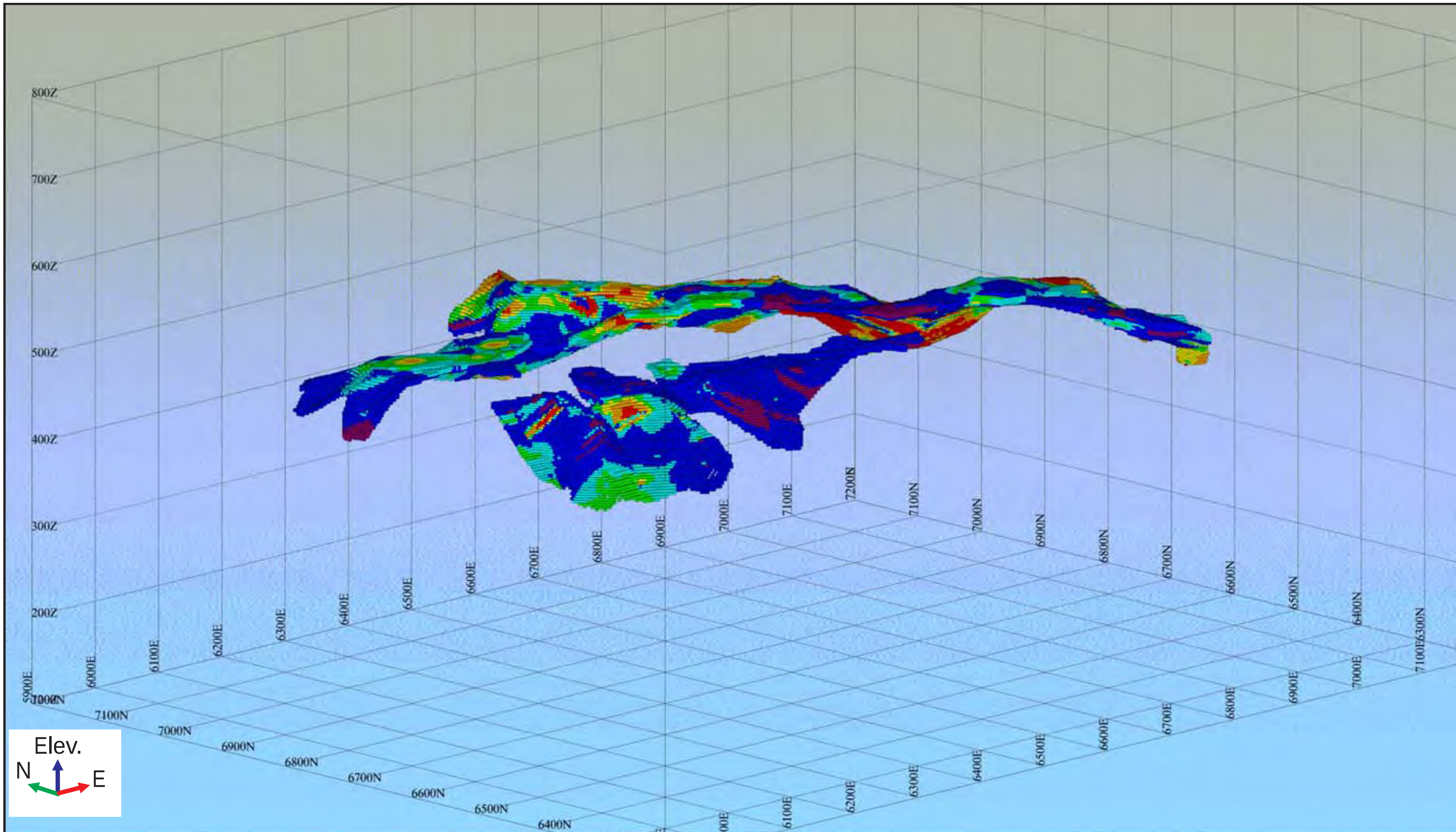

LEGEND

Zn% + Pb% Cut-off

(grey)	Undefined
(purple)	0.01 - 1.00
(blue)	1.00 - 2.00
(cyan)	2.00 - 2.50
(green)	2.50 - 3.00
(yellow)	3.00 - 3.50
(orange)	3.50 - 5.00
(red)	5.00 - 99.00

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Figure 25
Perspective View of Getty Deposit
Grade Distribution
Looking Northeast

Date: April 2011

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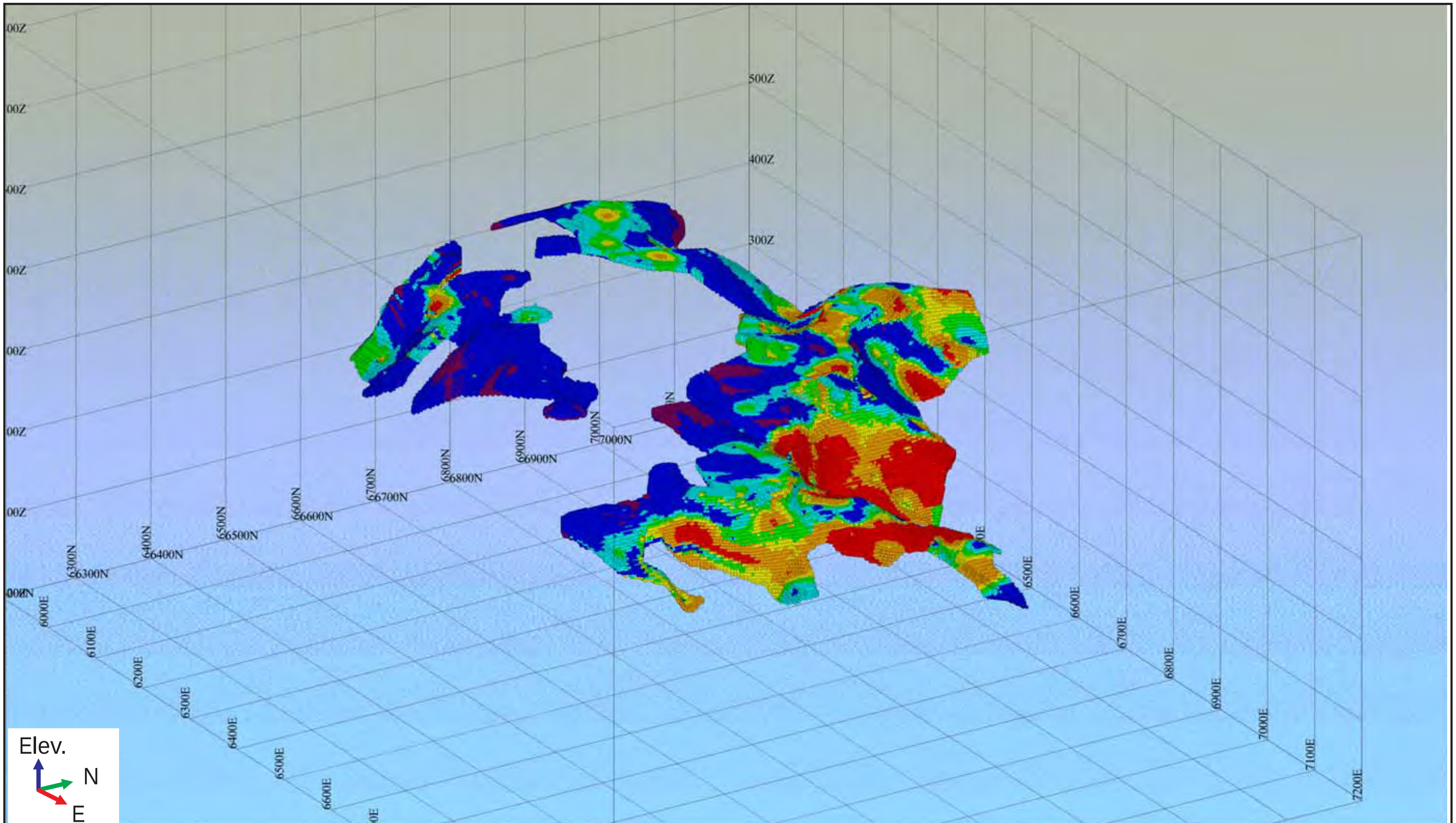

LEGEND

Undefined	Zn% + Pb% Cut-off
0.01 - 1.00	
1.00 - 2.00	
2.00 - 2.50	
2.50 - 3.00	
3.00 - 3.50	
3.50 - 5.00	
5.00 - 99.00	

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Figure 26
Perspective View of Getty Deposit
Grade Distribution
Looking Northwest

Date: April 2011

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Indicated Mineral Resource

An "Indicated Mineral Resource" is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters to support mine planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings, and drill holes, that are spaced closely enough for geological and grade continuity to be reasonably assumed.

Measured Mineral Resource

A "Measured Mineral Resource" is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters, to support production planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings, and drill holes, that are spaced closely enough to confirm both geological and grade continuity.

16.3.11 Resource Classification

Mineral resources presented in the current estimate have been assigned Inferred, Indicated and Measured resource categories that reflect increasing levels of confidence with respect to spatial configuration or resources and corresponding grade assignment within the deposit. Several factors were considered in defining resource category assignments, including drill hole spacing, geological interpretations and integrity of supporting data sets. Results of the 2007-2008 core drilling program by Acadian provided the most important upgrading factor to the deposit data set in comparison to the 2007 resource estimate which previously reported Inferred mineral resource. The new Acadian drill holes provided a nominal drill hole spacing of approximately 50 meters by 50 meters over much of the deposit area and constituted a major degree of infilling with respect to more broadly spaced historic drill holes that supported the previous estimate. The increased drill hole density factor was augmented by additional QA/QC program results associated with twinning of 10 historic drill holes during the 2007-2008 Acadian drill program and also by re-logging and sampling of 10 historic drill holes for which archived core was available. Positive results from all noted programs served to upgrade overall confidence in the project data set and justified definition of higher category resources.

Definition parameters for each resource category specified in the current Getty estimate are set out below and Figure 27 illustrates distribution of categories in plan view.

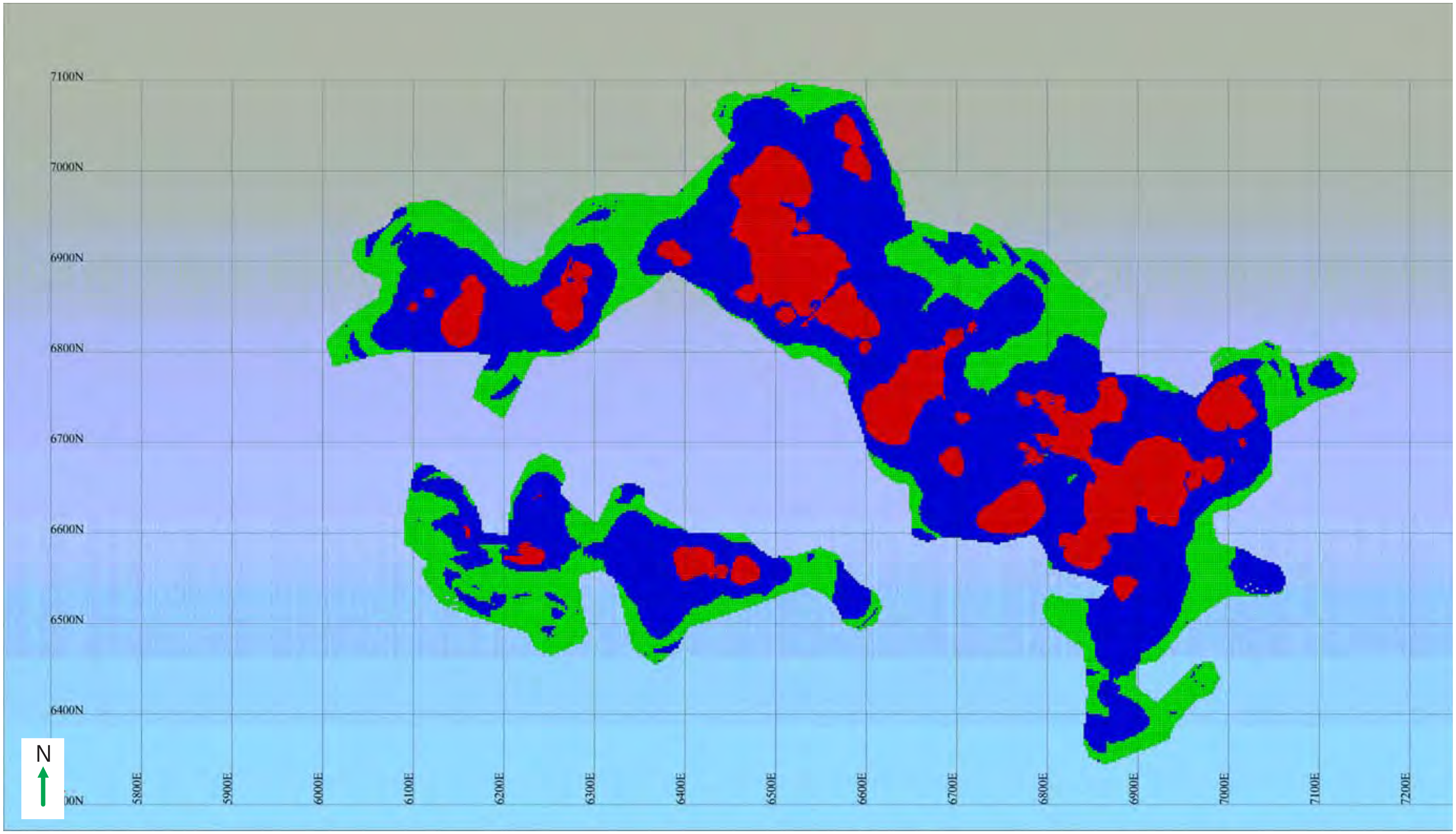
Measured Resources: All blocks with grades based on three drill holes and a minimum of 9 included samples, with not more than 4 composites from a single drill hole, for which the averaged distance to included samples was 28 meters or less with no sample greater than 50% of the major axis range (37.5m) from the block were categorized as Measured mineral resources.

Indicated Resources: All blocks with grades based on two or more drill holes and a minimum of 5 included samples, with not more than 4 composites from a single drill hole, for which the averaged distance to included samples was 40 meters or less with no sample greater than 75% of the major axis range (56.5m) from the block were categorized as Indicated mineral resources.

Inferred Resources: All blocks present within the deposit solid that did not meet other resource category requirements and for which interpolated grades were present were categorized as Inferred mineral resources.

16.3.12 Statement of Mineral Resource Estimate at Effective Date

Table 20 presents a statement of the updated mineral resource estimate for the Getty zinc-lead deposit supported by content of this technical report. The estimate is considered to be compliant with both the CIM Standards and disclosure requirements of NI-43-101. The effective date of the estimate is deemed to be March 30, 2011. All parameters utilized in the 2008 resource estimate were applied to this revised estimate with the exception of the Zinc Equivalent % calculation factor. For the current resource estimate Zinc Equivalent % (Zn Eq %) has been defined as Zn % + (Pb % x 1.18) and is based on mill recoveries of 89.3% for zinc and 89.5% for lead, $US1.10/lb Zn and $US1.15/lb Pb metal pricing and smelter returns of 85% for Zn and 95% for Pb.



Legend

- Measured Resource
- Indicated Resource
- Inferred Resource

0 100 200
metres

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Figure 27
Plan View of Getty Deposit
Resource Categories

Date: April 2011

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Table 20: Mineral Resource Estimate for Getty Deposit- March 30, 2011.

Getty Deposit - Resource Statement - Zn Eq. % * Cut-off					
Resource Category	**Zn Eq. % Cut-off**	**Tonnes (Rounded)**	**Zinc %**	**Lead %**	**Zinc Eq %***
Measured	1.50	1,930,000	1.81	1.26	3.30
Indicated	1.50	3,790,000	1.62	1.21	3.05
Indicated + Measured	***1.50***	***5,720,000***	***1.68***	***1.23***	***3.13***
Inferred	***1.50***	***1,350,000***	***1.52***	***1.31***	***3.06***
Measured	***2.00**	**1,550,000**	**1.97**	**1.45**	**3.68**
Indicated	***2.00**	**2,810,000**	**1.82**	**1.44**	**3.51**
Indicated + Measured	****2.00***	***4,360,000***	***1.87***	***1.44***	***3.57***
Inferred	****2.00***	***960,000***	***1.73***	***1.59***	***3.60***
Measured	2.50	1,180,000	2.14	1.68	4.12
Indicated	2.50	1,950,000	2.06	1.70	4.07
Indicated + Measured	***2.50***	***3,130,000***	***2.09***	***1.69***	***4.09***
Inferred	***2.50***	***680,000***	***1.95***	***1.88***	***4.16***
Measured	3.00	860,000	2.34	1.95	4.64
Indicated	3.00	1,300,000	2.35	2.03	4.74
Indicated + Measured	***2.50***	***2,160,000***	***2.35***	***2.00***	***4.70***
Inferred	***3.00***	***460,000***	***2.21***	***2.23***	***4.85***

Notes: ***(1) Zinc Equivalent % (Zn Eq.%) = Zn % + (Pb % x 1.18) and is based on mill recoveries of 89.3% for zinc and 89.5% for lead, $US1.10/lb Zn and $US1.15/lb Pb metal pricing and smelter returns of 85% for Zn and 95% for Pb, (2) * denotes the 2.00% Zn Eq. resource statement cutoff value that reflects open pit development potential***

16.3.13 Validation of Model

Comparison to Geological Sections

Results of block modeling were compared on a section by section basis with corresponding interpreted geological and grade distribution sections prepared prior to block model development. This showed that block model grade patterns show good correlation with those interpreted from the geological sections and that the stratabound character of the mineralization was being properly represented. Results of visual inspection are interpreted as showing an acceptable degree of consistency between the block model and the independently derived sectional interpretation, thusly providing a measure of validation against the geological model developed for the deposit.

Comparison of Composite Database and Block Model Grades

Descriptive statistics were calculated for those portions of the drill hole composite population falling within the total deposit peripheral constraint and these figures were compared to corresponding values calculated for the resource estimate block model. Results of the comparison are tabulated in Table 21 below. Mean drill hole assay composite grades for zinc and lead compare closely with corresponding zinc and lead grades calculated for the entire block model and provide a check on bias within the model with respect to the underlying total assay composite population.

Table 21: Comparison of Drill Hole Assay Composite and Block Model Grades

Parameter	***Total Model Grade (Zn%)**	***Total Model Grade (Pb%)**	**Composites Grade (Zn%)**	**Composites Grade (Pb%)**
Mean	1.43	1.01	1.46	1.00
Variance	0.86	0.99	1.94	2.53
Standard Deviation	0.93	1.00	1.39	1.59
Coef. of Variation	0.648	0.990	0.948	1.580
Maximum	10.27	14.52	11.30	18.54
Minimum	0.00	0.00	0.00	0.00
Number	209,757	209,757	1961	1961

**Defined as all blocks having interpolated grades within the deposit peripheral constraint*

Comparison of With Nearest Neighbour Grade Interpolation Model

The ID^2 block model was checked using Nearest Neighbour (NN) grade interpolation methodology within the same resource solids used for the ID^2 method and associated weighted average drill hole intercepts appear in Appendix 2. Assigned block resource categories were constant between models as were metal cut-off values. Results of the NN estimation appear in Table 22 and Figure 28 provides a comparison to ID2 model results.

Table 22: Results of Nearest Neighbour Block Model Estimate

Cutoff: Pb%+Zn%	**Resource Category**	**Tonnes (Rounded)**	**Pb %**	**Zn%**	**Pb%+Zn%**
2.00	Measured	1,480,000	1.44	1.90	3.34
2.00	Indicated	2,320,000	1.51	1.96	3.47
2.00	*Indicated Plus Measured*	*3,800,000*	*1.48*	*1.94*	*3.42*
2.00	Inferred	880,000	1.58	1.81	3.39
2.50	Measured	1,050,000	1.75	2.07	3.82
2.50	Indicated	1,490,000	1.90	2.27	4.17
2.50	*Indicated Plus Measured*	*2,540,000*	*1.84*	*2.19*	*4.03*
2.50	Inferred	530,000	2.05	2.15	4.20
3.00	Measured	700,000	2.07	2.31	4.38
3.00	Indicated	1,080,000	2.19	2.56	4.75
3.00	*Indicated Plus Measured*	*1,780,000*	*2.14*	*2.46*	*4.60*
3.00	Inferred	410,000	2.24	2.41	4.64

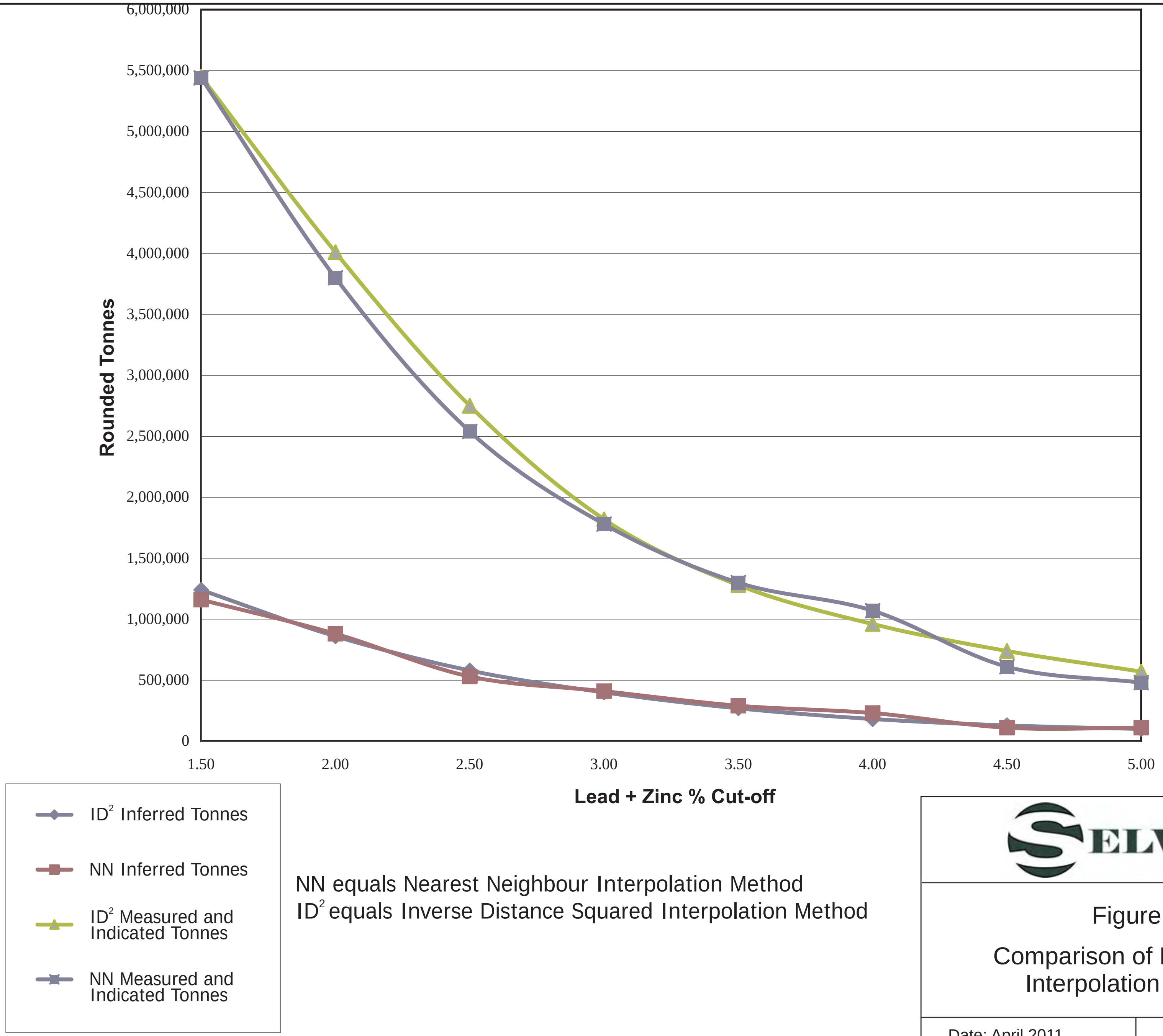

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Figure 28

Comparison of Block Model Interpolation Methods

Date: April 2011

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Grade and tonnage figures for the two block models correlate well at all cutoff values and are interpreted as providing an acceptable check of the ID2 model.

16.4 Comments on Previous Resource or Reserve Estimates

Three historic mineral resource estimates were reviewed for purposes of this report and these were referenced previously in section 5.2. The first was prepared in 1976 for Getty by MPH Consulting Limited (Riddell, 1976) and apparently followed earlier in-house estimates by Getty. Subsequently, an in-house assessment was prepared by Esso (MacLeod, 1980) and in 1992 Westminer also completed an estimate (Hudgins and Lamb, 1992). Results of these programs are presented in Table 23 below and, as noted earlier, all are historic in nature, pre-date NI 43-101 and are not compliant with current CIMM Standards. As such, they should not be relied upon.

Table 23: Historic Tonnage and Grade Estimates for Getty Deposit
(Estimates Are Not Compliant With NI 43-101 or CIMM Standards)

Reference	Cutoff	Tonnes	Pb %	Zn %	Zn + Pb %
Riddell (1976)	2% Zn + Pb	4,005,000	1.84	1.87	3.02
*MacLeod (1980)	1.5% Zn +Pb	3,078,000	1.37	1.60	2.97
**Hudgins and Lamb (1992)	**1.5% Zn Eq.	4,500,000	1.33	1.87	3.20

** Diluted and Minable;*
***Zn Eq. = Zn% + 0.60 x Pb%*
Notes: *With regard to the historic mineral resource estimates stated above 1) a qualified person has not done sufficient work to classify the historical estimate as current mineral resources or mineral reserves; 2) the issuer is not treating the historical estimate as current mineral resources or mineral reserves as defined in sections 1.2 and 1.3 of NI43-101; and 3) the historical estimate should not be relied upon.*

Support documents provided for the historic estimates showed that those of Getty and Esso were based on drill-hole-centered polygonal methods with tonnage weighting to establish final deposit grade. A single density factor of 11.5 cubic feet per ton (~2.78g/cm3) was used in the Riddell (1976) estimate and this appears to have been used by MacLeod (1980) before application of a 10% tonnage reduction factor to drill hole intercepts. Westminer employed a cross-sectional method using Surpac® mining software to determine resource area limits and volume and used a single density factor of 2.75 g/cm3 to estimate tonnage. Deposit grade was calculated as the length-weighted average of all drill hole intercepts, but spatial distribution of grade within the deposit was not specifically addressed.

A summary review of supporting file information for the historic estimates was completed for current purposes and it is apparent that the noticeably lower tonnage figure quoted by Esso reflects exclusion of certain drill holes based on the report's development potential assumptions. The higher lead grade in the MPH estimate is also notable but main contributing factors were not clearly identified.

Riddell (1976) completed a preliminary economic assessment for open pit development of a 3.6 million ton (3.3 million tonne) portion of the deposit at a diluted grade of 1.28% Pb and 1.74% Zn. Modeling parameters included options of a stand-alone mill, custom milling of ore at Esso's adjacent Gays River site and development of a jointly-owned mill complex in association with Esso. Analysis showed that a 20 year model producing at 182,000 tons per year with a dedicated mill was uneconomic. However, 10 year projects producing at 375,000 tons per year were financially attractive in both the custom milling and jointly owned mill models.

In 1980 Esso reported on economic aspects of developing the deposit based on an insitu tonnage and grade model of 3.1 million diluted tons (2.8 million tonnes) grading 1.37% Pb and 1.60% Zn (MacLeod, 1980). This study concluded that mining the deposit through open-pit methods as an ore supplement to the Gays River deposit was economically viable, provided that important operating assumptions were met. Positive Net Present Value figures at 15% discounting were returned for 1000 and 1250 ton per day production rates, with the Gays River operation absorbing certain operating and capital cost components. George (1985) again reviewed deposit economics for Getty and used economic analysis applied to tonnage and grade curves to show that a deposit size of approximately 8 million tons was necessary to justify stand-alone profitable development at realizable metal grades. The earlier MPH work was also reviewed and some of the economic models updated. None of the work indicated that profitable stand-alone development of the deposit could be expected under existing market conditions of the time.

Hudgins and Lamb (1992) reported on preliminary economic analysis of a 3.9 million tonne portion of the total resource at their assigned grade and concluded that a positive economic case could be made for development of the property as a "top-up" source of feed for the Gays River concentrator. Assumptions included sharing of various operating costs with the Gays River operation and that the full 1500 tonne per day capacity of the Gays River concentrator would not be required for underground production.

In review, each of the historic estimates reflects specific assumptions considered appropriate at the time of preparation. This includes exclusion of certain historic drill holes, establishment of different maximum depth criteria and use of differing minimum grade and width cut off values. The current estimate does not directly reflect any of the parameter sets used in the early programs and results are therefore different. However, all historic programs model the Getty deposit as a relatively low grade accumulation of lead and zinc having potential for open pit development. From the grade and tonnage perspective the earlier estimates are generally consistent with results of the current estimate and provide relevant views of the deposit under historic market conditions.

The first NI 43-101 compliant Getty resource estimate completed by Mercator for Acadian (Cullen et al. 2007) was based solely on historical drilling and the entire resource was assigned to the Inferred resource category. Inferred designation reflected drill hole spacing and historical nature of the supporting database. The associated block model provided a well developed view of geological and grade trends within the deposit area and also highlighted the need to carry out a substantial amount of infill drilling before higher category resources could be defined for the deposit. Table 24 presents results of the Cullen et al. (2007) resource estimate, which, on a total tonnage basis, is approximately 19% smaller than total tonnage at the same cutoff value for the 2008 resource at comparable average grades.

Table 24:*Getty Deposit Mineral Resource Estimate - December 2007

Resource Category	**Zn Equivalent % Threshold****	**Tonnes (Rounded)**	**Lead %**	**Zinc %**	**Zinc% + Lead %**
Inferred	2.00	4,160,000	1.40%	1.81%	3.21%
Inferred	2.50	2,860,000	1.60%	2.06%	3.66%
Inferred	3.00	1,970,000	1.82%	2.26%	4.08%
Inferred	3.50	1,300,000	2.09%	2.42%	4.51%

Notes: Estimate is compliant with NI 43-101 and CIM Standards; ** Zn Equivalent calculated as Zn Equivalent = (Zn% + Pb %)*

Completion of infill drilling was recommended and ultimately carried out during the 2007-2008 Acadian drilling campaign that totalled 138 holes in the deposit area. Addition of results for the 138 drill holes is the principal difference between the 2008 resource data set and that used in the 2007 estimate, with the designation of higher category resources in reflecting increased confidence in deposit geology and grade distribution models (Cullen et al., 2008). The NI 43-101 compliant 2008 estimate is summarized in Table 25.

Table 25:*Getty Deposit Mineral Resource Estimate – November 2008

Resource Category	**Zinc% +Lead% Threshold****	**Tonnes (Rounded)**	**Lead %**	**Zinc %**	**Zinc% + Lead %**
Measured	2.00	1,470,000	1.48	2.02	3.50
Indicated	2.00	2,540,000	1.48	1.91	3.39
Indicated Plus Measured	***2.00***	***4,010,000***	***1.48***	***1.95***	***3.43***
Inferred	2.00	860,000	1.65	1.82	3.48
Measured	2.50	1,070,000	1.74	2.22	3.97
Indicated	2.50	1,680,000	1.78	2.21	3.99
Indicated Plus Measured	***2.50***	***2,750,000***	***1.76***	***2.21***	***3.98***
Inferred	2.50	580,000	1.98	2.09	4.07

Resource Category	Zinc% +Lead% Threshold**	Tonnes (Rounded)	Lead %	Zinc %	Zinc% + Lead %
Measured	3.00	740,000	2.04	2.47	4.52
Indicated	3.00	1,080,000	2.13	2.54	4.67
Indicated Plus Measured	***3.00***	***1,820,000***	***2.09***	***2.51***	***4.61***
Inferred	3.00	400,000	2.34	2.37	4.71

** Estimate is compliant with NI 43-101 and CIM Standards; ** Zn Equivalent calculated as Zn Equivalent = (Zn% + Pb %)*

A portion of this tonnage increase is directly attributable to change in base SG value for the block model, from 2.7 g/cm^3 in 2007 to 2.82 g/cm^3 in 2008. The remaining change is attributed to incremental extension of local deposit limits on the basis of 2007-2008 drilling program results.

17.0 Other Relevant Data and Information

17.1 Environmental and Surface Title Liabilities

The Getty deposit underlies an area of predominantly cleared land with limited peripheral forest cover that is being actively used for agricultural purposes. This primarily reflects one dairy farming operation with associated infrastructure. No obvious environmental liabilities with respect to current land use in the deposit area deposit were known to the authors at the report date and no such liabilities had been communicated by Acadian or Selwyn personnel. However, this comment does not constitute a professional opinion with respect to environmental status of the property. Presence of the Gays River watercourse along a portion of the deposit's eastern margin has required enhanced diligence with respect to surface exploration activities such as drilling and the authors surmise that proximity to the river will remain an important consideration in any development evaluation or planning efforts.

In addition to the above, status and details of surface rights, titles and land access agreements were not reviewed by the authors for purposes of this report. However, Acadian advised that no difficulties exist to date on this front and that the company has established access agreements to allow work programs to be carried out. On a related point, surface rights holders in Nova Scotia typically hold title to gypsum and limestone occurring on their lands. In some instances gypsum and/or limestone rights have been severed from the surface title or legal agreements have been made that bear on their ownership. While current status of gypsum title was not investigated by the authors for report purposes, this point is noted as being relevant to assessment of future development options for the deposit. As in the preceding case, a professional opinion is not being provided with respect to surface or mineral right titles.

18.0 Interpretation and Conclusions

The Getty zinc lead deposit is a carbonate hosted, stratabound lead – zinc deposit of the Mississippi Valley Type (MVT) that exists as an extension to the Scotia Mine zinc-lead deposit located immediately to the southeast. Both occur in carbonate bank lithologies of the Gays River Formation that are situated along discrete paleo-topographic highs consisting of Cambro-Ordovician Goldenville Formation greywacke. Bank morphology in the Getty area differs from that at Scotia Mine by having generally shallower bank-front slopes. The Scotia Mine deposit has higher overall lead and zinc resource grades than Getty and these reflect higher proportions of submassive to massive sphalerite and galena along moderate to steeply dipping (40º o to 70º) bank-front intervals.

During 2007-2008 Acadian completed 138 new drill holes in the Getty deposit area and addition of associated results to the previously validated historic drill hole database provided the basis for the current updated resource estimate. In comparison to an earlier estimate prepared by Mercator for Acadian (Cullen et al., 2007) overall deposit size has increased at generally comparable zinc and lead grade levels. This increase is predominantly attributable to incremental extension and/or infilling of the deposit outline based on the new drill hole data set. A lesser influence is attributable to modification of the specific gravity assignment factor used in the block model. The 2007-2008 drill program also effectively defined the limits of the deposit at the cutoff grades used in the updated resource estimate. Upgrading of the deposit database through addition of the new drilling program results has increased confidence in geological and grade distribution models for the deposit and provided support for definition of Measured, Indicated and Inferred category resources.

Table 26 presents the updated mineral resource statement, which is considered compliant with both the CIM Standards and disclosure requirements of NI-43-101. All parameters utilized in the 2008 resource estimate were applied to this revised estimate with the exception of the Zinc Equivalent % factor which was re-defined for current purposes.

Table 26: Mineral Resource Estimate for Getty Deposit- March 2011.

Getty Deposit - Resource Statement - Zn Eq. % * Cut-off					
Resource Category	**Zn Eq. % Cut-off**	**Tonnes (Rounded)**	**Zinc %**	**Lead %**	**Zinc Eq %***
Measured	1.50	1,930,000	1.81	1.26	3.30
Indicated	1.50	3,790,000	1.62	1.21	3.05
Indicated + Measured	***1.50***	***5,720,000***	***1.68***	***1.23***	***3.13***
Inferred	***1.50***	***1,350,000***	***1.52***	***1.31***	***3.06***
Measured	***2.00**	**1,550,000**	**1.97**	**1.45**	**3.68**
Indicated	***2.00**	**2,810,000**	**1.82**	**1.44**	**3.51**
Indicated + Measured	****2.00***	***4,360,000***	***1.87***	***1.44***	***3.57***
Inferred	****2.00***	***960,000***	***1.73***	***1.59***	***3.60***
Measured	2.50	1,180,000	2.14	1.68	4.12
Indicated	2.50	1,950,000	2.06	1.70	4.07
Indicated + Measured	***2.50***	***3,130,000***	***2.09***	***1.69***	***4.09***
Inferred	***2.50***	***680,000***	***1.95***	***1.88***	***4.16***
Measured	3.00	860,000	2.34	1.95	4.64
Indicated	3.00	1,300,000	2.35	2.03	4.74
Indicated + Measured	***2.50***	***2,160,000***	***2.35***	***2.00***	***4.70***
Inferred	***3.00***	***460,000***	***2.21***	***2.23***	***4.85***

Notes: *(1) Zinc Equivalent % (Zn Eq.%) = Zn % + (Pb % x 1.18) and is based on mill recoveries of 89.3% for zinc and 89.5% for lead, $US1.10/lb Zn and $US1.15/lb Pb metal pricing and smelter returns of 85% for Zn and 95% for Pb, (2) * denotes the 2.00% Zn Eq. resource statement cutoff value that reflects open pit development potential*

19.0 Recommendations

Based on results of the resource estimation program described in this report, the following recommendations are provided with respect to future work on the Getty deposit. Estimated budget figures for recommended work are not included because detailed planning and execution of such programs should only be undertaken after full coordination with advancement of the adjacent Scotia Mine project is possible.

1. A preliminary economic assessment of the deposit should be completed to establish an initial structured assessment of its future development potential.

2. Additional infill drilling should be carried out in areas of Inferred resources, particularly those present in the southeast half of the deposit, where generally higher metal grades are present. Infill drill hole spacing of at least 50 meters by 50 meters should be completed to allow upgrading of resources. The anticipated result of such drilling would be to increase Indicated mineral resources within the deposit limit.

3. A preliminary metallurgical testing program should be carried out on selected core sample reject materials or on new representative drill core samples from the deposit. Results of this work should identify basic processing attributes and provide input data for more advanced assessments of development potential.

19.1 Estimated Budget

Based on the results of this report the following Phase 1 budget is recommended (Table 27).

Table 27: Estimated Phase 1 Budget

Task	**Estimated Cost**
Preliminary Economic Assessment	$50,000
Contingency 10%	$5,000
Total	**$55,000**

The following Phase 2 budget is contingent on the outcome of the Phase 1 recommendations (Table 28).

Table 28: Estimated Phase 2 Budget

Task	**Estimated Cost**
Infill drilling 2,500m	$500,000
Metallurgical Testing	$100,000
Contingency 10%	$60,000
Total	**$660,000**

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21.0 Date and Signature Page

The effective date of this report is March 30, 2011.

Respectfully submitted,

[Original signed and sealed by]

____

Michael P. Cullen, M.Sc. (Geol.), P. Geo.
Senior Geologist

[Original signed and sealed by]

____

Chrystal Kennedy, B.Sc. (Geol.), P. Geo.
Senior Project Geologist

[Original signed by]

____

Matthew Harrington, B.Sc. (Geol.)
Geologist

Appendix 1: Statements of Qualifications and Consent Letters

CERTIFICATE of AUTHOR

I, Michael P. Cullen, *P. Geo.* do hereby certify that:

1. I am currently employed as a Senior Geologist by:

   Mercator Geological Services Limited
   65 Queen St
   Dartmouth, Nova Scotia, Canada
   B2Y 1GA

2. I graduated with a Masters Degree in Science (Geology) from Dalhousie University in 1984. In addition, I obtained a Bachelor of Science degree (Honours, Geology) in 1980 from Mount Allison University.

3. I am a registered member in good standing of the following professional associations: (1) Association of Professional Geoscientists of Nova Scotia, registration number 064, Professional Engineers and Geologists of Newfoundland and Labrador, registration number 05058 and Association of Professional Engineers and Geoscientists of New Brunswick, registration number L4333.

4. I have worked as a geologist in Canada and internationally since graduation from university.

5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101

6. I am one of the qualified person responsible for preparation of the technical report entitled:

   TECHNICAL REPORT ON AN
   UPDATED MINERAL RESOURCE ESTIMATE
   GETTY ZINC - LEAD DEPOSIT
   GAYS RIVER AREA
   HALIFAX COUNTY, NOVA SCOTIA
   CANADA
   NTS 11E03B
   Effective Date: March 30, 2011

7. I have visited the Getty Property on numerous occasions since September, 2006 and most recently visited the property on September 17th, 2008 at which time diamond drill core was examined and Acadian's core logging facility at the Scotia Mine site was also visited. Since September, 2006 I

have participated in numerous meetings with Mercator and Acadian staff regarding Getty deposit geology.

8. I am responsible for supervision of all aspects of report preparation and specifically responsible for report sections 1, 6, 7, 8, 16, 17, 18 and 19.

9. I previously reviewed and reported on historic Getty deposit drilling results on behalf of Savage Zinc Inc., this work being carried out by Mercator Geological Services Limited on a fee for service basis in 2001. I am also a co-author of a previously disclosed National Instrument 43-101 compliant mineral resource estimate for the Getty deposit, having an effective date of September 9th, 2008, that was completed by Mercator for Acadian Mining.

10. I have extensive experience in the Carboniferous stratigraphy and zinc lead mineralization within Nova Scotia having worked and managed drilling programs within the Gays River area and other areas of Nova Scotia over my 30 year career.

11. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.

12. I am independent of the issuer applying all of the tests in section 1.5 of National Instrument 43-101.

13. I have read National Instrument 43-101 and Form 43-101F1, and believe that this Technical Report has been prepared in compliance with that instrument and form.

14. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 26th Day of April, 2011

[Original signed and sealed by]

Michael P. Cullen, M. Sc., P. Geo.
Senior Geologist
Mercator Geological Services Limited

CERTIFICATE of AUTHOR

I, Chrystal Kennedy, B.Sc. (Geol.), P. Geo. do hereby certify that:

1. I am currently employed as a Senior Geologist by:

   Mercator Geological Services Limited
   65 Queen St
   Dartmouth, Nova Scotia, Canada
   B2Y 1GA

2. I graduated with a Bachelor of Science Degree (Adv. Major Geology) from Dalhousie University in 1996. In addition, I obtained a Bachelor of Science degree (Honours, Biology) in 1993 from Dalhousie University.

3. I am a registered member in good standing of the Association of Professional Geoscientists of Nova Scotia, registration number 105.

4. I have worked as a geologist in Canada since 1996.

5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101

6. I am one of the qualified persons responsible for preparation of the technical report entitled:

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7. I have visited the Getty Property on numerous occasions since September, 2006 and most recently visited the property on April 11, 2011. I was responsible for supervision of a diamond drilling program carried out on the Getty property by Acadian Mining Corp. during 2007 and 2008 I have examined core logging and sampling facilities at Acadian's Scotia Mine site and have participated in numerous meetings with Mercator and Acadian staff regarding Getty deposit geology.

8. I am responsible for preparation of report sections 2, 3, 4, 9, 10, 11, 12, 15, and 20 and contributed to sections 5, 6, 7, 8, 16, 18 and 19.

9. I am a co-author of a previously disclosed National Instrument 43-101 compliant mineral resource estimate for the Getty deposit (Cullen et al., 2007), having an effective date of September 9th, 2008, and Cullen et al 2008, having and effective date of November 12, 2008 that was completed by Mercator for Acadian Mining.

10. I have extensive experience in the Carboniferous stratigraphy and zinc lead mineralization within Nova Scotia having worked and managed drilling programs within the Gays River area.

11. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.

12. I am independent of the issuer applying all of the tests in section 1.5 of National Instrument 43-101.

13. I have read National Instrument 43-101 and Form 43-101F1, and believe that this Technical Report has been prepared in compliance with that instrument and form.

14. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 26th Day of April, 2011

[Original signed and sealed by]

____

Chrystal Kennedy, B. Sc. (Geol.), P. Geo.
Senior Project Geologist
Mercator Geological Services Limited

CERTIFICATE of AUTHOR

I, Matthew Harrington, B.Sc. (Geol.), do hereby certify that:

1. I currently reside in Halifax, Nova Scotia Canada and am employed as a Geologist by:

   Mercator Geological Services Limited
   65 Queen St
   Dartmouth, Nova Scotia, Canada
   B2Y 1GA

2. I graduated with a Bachelor of Science (Geol.) degree from Dalhousie University in Halifax, Nova Scotia, Canada in 2003.

3. I have worked as a geologist in Canada for 4 years since graduation from university and have been employed by Mercator geological Services since 2003.

4. I participated in preparation of the Getty deposit mineral resource estimate and three dimension block model described in the technical report named below. My participation was supervised by Mr. Michael P. Cullen, P. Geo. and Ms. Chrystal Kennedy, P. Geo.

TECHNICAL REPORT ON AN
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5. I have visited the property that is the subject of this Technical Report. I am a co-author of a previously disclosed National Instrument 43-101 compliant mineral resource estimate for the Getty deposit (Cullen et al., 2007), having an effective date of September 9th, 2008, and (Cullen et al, 2008) having an effective date of November 12, 2008 that was completed by Mercator for Acadian Mining.

6. I specifically contributed to report sections 16, 18 and 19.

7. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.

8. I am independent of the issuer applying all of the tests in section 1.5 of National Instrument 43-101.

9. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 26th Day of April, 2011

[Original signed by]

Matthew Harrington, B. Sc. (Geol.)
Geologist
Mercator Geological Services Limited

CONSENT of AUTHOR

TO: Selwyn Resources Ltd., Alberta Securities Commission, Manitoba Securities Commission, Ontario Securities Commission, Nova Scotia Securities Commission, New Brunswick Securities Commission, Securities Commission of Newfoundland and Labrador, TSX Venture Exchange and Toronto Stock Exchange and British Columbia Securities Commission

I, Michael P. Cullen, M. Sc., P. Geo. do hereby consent to the filing, with the regulatory authorities referred to above, of the technical report entitled

TECHNICAL REPORT ON AN
UPDATED MINERAL RESOURCE ESTIMATE
GETTY ZINC - LEAD DEPOSIT
GAYS RIVER AREA
HALIFAX COUNTY, NOVA SCOTIA
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NTS 11E03B
Effective Date: March 30, 2011

(the "Technical Report") and to the written disclosure of the Technical Report and of extracts from or a summary of the Technical Report in the written disclosure in the news release of Acadian Mining Corporation being filed.

I also certify that I have read the written disclosure being filed and I do not have any reason to believe that there are any misrepresentations in the information derived from the Technical Report or that the written disclosure in the news release of Selwyn Resources Ltd., dated March 30, 2011, contains any misrepresentation of the information contained in the Technical Report.

Dated this 26th Day of April, 2011

[Original signed and sealed by]

____
Signature of Qualified Person

Michael P. Cullen, M. Sc., P. Geo.
Senior Geologist
Mercator Geological Services Limited

CONSENT of AUTHOR

TO: Selwyn Resources Ltd., Alberta Securities Commission, Manitoba Securities Commission, Ontario Securities Commission, Nova Scotia Securities Commission, New Brunswick Securities Commission, Securities Commission of Newfoundland and Labrador, TSX Venture Exchange and Toronto Stock Exchange and British Columbia Securities Commission

I, Chrystal Kennedy, B. Sc. (Geol.), P. Geo., do hereby consent to the filing, with the regulatory authorities referred to above, of the technical report entitled:

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UPDATED MINERAL RESOURCE ESTIMATE
GETTY ZINC - LEAD DEPOSIT
GAYS RIVER AREA
HALIFAX COUNTY, NOVA SCOTIA
CANADA
NTS 11E03B
Effective Date: March 30, 2011

(the "Technical Report") and to the written disclosure of the Technical Report and of extracts from or a summary of the Technical Report in the written disclosure in the news release of Acadian Mining Corporation being filed.

I also certify that I have read the written disclosure being filed and I do not have any reason to believe that there are any misrepresentations in the information derived from the Technical Report or that the written disclosure in the news release of Selwyn Resources Ltd., dated March 30, 2011, contains any misrepresentation of the information contained in the Technical Report.

Dated this 26th Day of April, 2011

[Original signed and sealed by]

Signature of Qualified Person

Chrystal Kennedy, B. Sc. (Geol.), P. Geo.
Senior Project Geologist
Mercator Geological Services Limited

CONSENT of AUTHOR

TO: Selwyn Resources Ltd., Alberta Securities Commission, Manitoba Securities Commission, Ontario Securities Commission, Nova Scotia Securities Commission, New Brunswick Securities Commission, Securities Commission of Newfoundland and Labrador, TSX Venture Exchange and Toronto Stock Exchange and British Columbia Securities Commission

I, Matthew Harrington, B. Sc. (Geol.), do hereby consent to the filing, with the regulatory authorities referred to above, of the technical report entitled:

TECHNICAL REPORT ON
UPDATED MINERAL RESOURCE ESTIMATE
GETTY ZINC - LEAD DEPOSIT
GAYS RIVER AREA
HALIFAX COUNTY, NOVA SCOTIA
CANADA
NTS 11E03B
Effective Date: March 30, 2011

(the "Technical Report") and to the written disclosure of the Technical Report and of extracts from or a summary of the Technical Report in the written disclosure in the news release of Acadian Mining Corporation being filed.

I also certify that I have read the written disclosure being filed and I do not have any reason to believe that there are any misrepresentations in the information derived from the Technical Report or that the written disclosure in the news release of Selwyn Resources Ltd., dated March 30, 2011, contains any misrepresentation of the information contained in the Technical Report.

Dated this 26th Day of April, 2011

[Original signed by]

Signature of Qualified Person

Matthew Harrington, B. Sc. (Geol.)
Geologist
Mercator Geological Services Limited

Appendix 2: Drilling Related Dcouments

Listing of 1 Meter Assay Composites in Resource Solid
Listing of Nearest Neighbour Drill Hole Intercepts
Acadian Lithocode Descriptions
Laboratory Procedure Summaries

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR018	56.65	57.65	0.28	3.53	3.81	6654	6984	478
GGR018	57.65	58.65	0.18	4.21	4.39	6654	6984	477
GGR018	58.65	59.65	2.45	7.63	10.08	6654	6984	476
GGR019	47.87	48.87	0.21	1.41	1.62	6659	6877	495
GGR019	48.87	49.87	0.13	1.82	1.95	6659	6877	494
GGR019	49.87	50.87	0.04	2.27	2.31	6659	6877	493
GGR019	50.87	51.87	0.41	3.87	4.29	6659	6877	492
GGR019	51.87	52.87	0.63	4.75	5.38	6659	6877	491
GGR019	52.87	53.87	0.89	5.82	6.71	6659	6877	490
GGR019	53.87	54.87	2.86	6.32	9.19	6659	6877	489
GGR019	54.87	55.87	2.05	5.25	7.30	6659	6877	488
GGR019	55.87	56.87	0.40	3.42	3.82	6659	6877	487
GGR019	56.87	57.87	0.13	1.35	1.48	6659	6877	486
GGR019	57.87	58.87	0.09	1.01	1.10	6659	6877	485
GGR021	28.96	29.96	0.01	1.35	1.36	6629	6756	520
GGR021	29.96	30.96	0.01	1.34	1.35	6629	6756	519
GGR021	30.96	31.96	0.01	1.33	1.34	6629	6756	518
GGR021	31.96	32.96	0.01	1.79	1.80	6629	6756	517
GGR021	32.96	33.96	0.02	1.35	1.37	6629	6756	516
GGR021	33.96	34.96	0.04	0.72	0.76	6629	6756	515
GGR021	34.96	35.96	0.12	0.98	1.10	6629	6756	514
GGR021	35.96	36.96	0.16	1.21	1.37	6629	6756	513
GGR021	36.96	37.96	0.22	1.54	1.76	6629	6756	512
GGR021	37.96	38.96	0.05	2.12	2.17	6629	6756	511
GGR021	38.96	39.96	0.14	1.93	2.06	6629	6756	510
GGR021	39.96	40.96	0.37	1.33	1.70	6629	6756	509
GGR021	40.96	41.96	0.23	0.48	0.72	6629	6756	508
GGR021	41.96	42.96	0.22	0.31	0.53	6629	6756	507
GGR021	42.96	43.96	0.28	0.42	0.70	6629	6756	506
GGR021	43.96	44.96	0.89	0.71	1.59	6629	6756	505
GGR021	44.96	45.96	0.38	0.29	0.67	6629	6756	504
GGR021	45.96	46.96	0.05	0.04	0.09	6629	6756	503
GGR021	46.96	47.96	0.61	0.56	1.17	6629	6756	502
GGR021	47.96	48.96	1.50	1.39	2.89	6629	6756	501
GGR021	48.96	49.96	0.61	1.69	2.30	6629	6756	500
GGR022	44.82	45.82	0.18	0.82	1.00	6641	6931	494
GGR022	45.82	46.82	0.60	1.30	1.90	6641	6931	493
GGR022	46.82	47.82	1.06	1.82	2.88	6641	6931	492
GGR022	47.82	48.82	0.33	1.37	1.70	6641	6931	491
GGR022	48.82	49.82	0.35	1.63	1.98	6641	6931	490
GGR022	49.82	50.82	0.43	2.01	2.44	6641	6931	489
GGR022	50.82	51.82	0.46	2.09	2.55	6641	6931	488
GGR022	51.82	52.82	0.39	1.80	2.19	6641	6931	487
GGR022	52.82	53.82	0.27	1.32	1.59	6641	6931	486
GGR022	53.82	54.82	0.12	1.21	1.33	6641	6931	485
GGR022	54.82	55.82	0.07	1.00	1.07	6641	6931	484

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR022	55.82	56.82	0.02	0.60	0.62	6641	6931	483
GGR022	56.82	57.82	0.01	1.44	1.45	6641	6931	482
GGR022	57.82	58.82	0.01	1.64	1.65	6641	6931	481
GGR024	70.12	71.12	6.41	3.76	10.17	6766	7014	456
GGR024	71.12	72.12	4.41	2.58	7.00	6766	7014	455
GGR025A	121.21	122.21	1.68	0.01	1.69	6768	6875	421
GGR025A	122.21	123.21	4.68	0.11	4.78	6768	6875	420
GGR025A	123.21	124.21	6.49	0.29	6.78	6768	6875	419
GGR025A	124.21	125.21	6.51	0.13	6.64	6768	6875	418
GGR025A	125.21	126.21	6.48	0.14	6.62	6768	6875	417
GGR025A	126.21	127.21	8.18	0.15	8.33	6768	6875	416
GGR025A	127.21	128.21	10.98	0.01	10.99	6768	6875	415
GGR025A	128.21	129.21	4.64	0.01	4.65	6768	6875	414
GGR025A	129.21	130.21	1.52	0.01	1.53	6768	6875	413
GGR026	71.34	72.34	3.16	1.55	4.71	6759	6761	476
GGR026	72.34	73.34	2.28	1.20	3.48	6759	6761	475
GGR026	73.34	74.34	4.79	3.02	7.81	6759	6761	474
GGR026	74.34	75.34	3.38	3.74	7.12	6759	6761	473
GGR026	75.34	76.34	2.16	2.84	5.00	6759	6761	472
GGR026	76.34	77.34	0.33	1.67	2.00	6759	6761	471
GGR026	77.34	78.34	0.09	0.58	0.67	6759	6761	470
GGR026	78.34	79.34	0.10	1.10	1.20	6759	6761	469
GGR026	79.34	80.34	0.17	2.14	2.31	6759	6761	468
GGR026	80.34	81.34	0.17	2.14	2.31	6759	6761	467
GGR027	34.15	35.15	0.32	0.88	1.20	6755	6636	520
GGR027	35.15	36.15	0.26	0.70	0.96	6755	6636	519
GGR027	36.15	37.15	0.20	0.51	0.71	6755	6636	518
GGR027	37.15	38.15	0.64	0.85	1.49	6755	6636	517
GGR027	38.15	39.15	0.60	0.89	1.48	6755	6636	516
GGR027	39.15	40.15	0.39	0.82	1.21	6755	6636	515
GGR027	40.15	41.15	0.22	0.77	0.98	6755	6636	514
GGR027	41.15	42.15	3.89	1.88	5.77	6755	6636	513
GGR027	42.15	43.15	4.22	1.52	5.74	6755	6636	512
GGR027	43.15	44.15	1.28	0.77	2.05	6755	6636	511
GGR027	44.15	45.15	0.67	0.80	1.46	6755	6636	510
GGR032	91.80	92.80	0.26	0.60	0.87	6776	7117	421
GGR032	92.80	93.80	0.95	0.10	1.05	6776	7117	420
GGR032	93.80	94.80	2.38	0.02	2.40	6776	7117	419
GGR035A	87.50	88.50	0.21	1.54	1.75	7005	6602	458
GGR035A	88.50	89.50	0.12	1.42	1.53	7005	6602	457
GGR035A	89.50	90.50	0.02	0.70	0.72	7005	6602	456
GGR036	39.94	40.94	1.27	0.65	1.92	6884	6634	510
GGR036	40.94	41.94	0.54	0.25	0.80	6884	6634	509
GGR036	41.94	42.94	1.26	0.53	1.79	6884	6634	508
GGR036	42.94	43.94	2.61	1.04	3.65	6884	6634	507
GGR036	43.94	44.94	0.63	0.75	1.38	6884	6634	506

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR036	44.94	45.94	0.51	0.49	0.99	6884	6634	505
GGR036	45.94	46.94	0.41	0.27	0.67	6884	6634	504
GGR036	46.94	47.94	0.71	0.59	1.30	6884	6634	503
GGR037	40.50	41.50	1.11	2.37	3.47	6997	6511	512
GGR037	41.50	42.50	5.71	2.20	7.92	6997	6511	511
GGR037	42.50	43.50	5.81	1.67	7.48	6997	6511	510
GGR037	43.50	44.50	2.08	1.95	4.03	6997	6511	509
GGR037	44.50	45.50	3.20	3.75	6.95	6997	6511	508
GGR037	45.50	46.50	1.91	2.17	4.08	6997	6511	507
GGR037	46.50	47.50	3.42	2.66	6.07	6997	6511	506
GGR037	47.50	48.50	2.89	2.01	4.90	6997	6511	505
GGR037	48.50	49.50	1.10	1.25	2.35	6997	6511	504
GGR037	49.50	50.50	0.55	0.71	1.26	6997	6511	503
GGR037	50.50	51.50	0.49	0.67	1.16	6997	6511	502
GGR037	51.50	52.50	0.44	0.83	1.27	6997	6511	501
GGR037	52.50	53.50	0.87	1.21	2.08	6997	6511	500
GGR037	53.50	54.50	3.79	1.49	5.28	6997	6511	499
GGR037	54.50	55.50	1.95	1.11	3.06	6997	6511	498
GGR037	55.50	56.50	0.93	0.95	1.88	6997	6511	497
GGR037	56.50	57.50	1.16	1.12	2.28	6997	6511	496
GGR037	57.50	58.50	0.54	0.83	1.36	6997	6511	495
GGR037	58.50	59.50	0.38	0.69	1.07	6997	6511	494
GGR037	59.50	60.50	0.42	0.50	0.92	6997	6511	493
GGR037	60.50	61.50	0.35	0.17	0.53	6997	6511	492
GGR038	56.40	57.40	0.40	2.07	2.47	6889	6509	500
GGR038	57.40	58.40	0.28	1.59	1.87	6889	6509	499
GGR038	58.40	59.40	0.14	1.05	1.19	6889	6509	498
GGR038	59.40	60.40	0.05	0.13	0.17	6889	6509	497
GGR038	60.40	61.40	0.14	0.55	0.70	6889	6509	496
GGR038	61.40	62.40	0.27	1.20	1.46	6889	6509	495
GGR038	62.40	63.40	0.21	1.14	1.35	6889	6509	494
GGR038	63.40	64.40	0.11	0.54	0.65	6889	6509	493
GGR038	64.40	65.40	0.11	0.59	0.70	6889	6509	492
GGR038	65.40	66.40	0.38	2.31	2.69	6889	6509	491
GGR038	66.40	67.40	4.62	4.00	8.62	6889	6509	490
GGR038	67.40	68.40	2.86	2.70	5.56	6889	6509	489
GGR038	68.40	69.40	0.33	0.83	1.16	6889	6509	488
GGR039A	58.54	59.54	5.82	2.28	8.10	6987	6433	494
GGR039A	59.54	60.54	4.21	1.99	6.20	6987	6433	493
GGR039A	60.54	61.54	1.72	1.42	3.14	6987	6433	492
GGR039A	61.54	62.54	1.36	1.43	2.79	6987	6433	491
GGR039A	62.54	63.54	0.76	1.06	1.82	6987	6433	490
GGR039A	63.54	64.54	1.25	0.63	1.88	6987	6433	489
GGR039A	64.54	65.54	1.74	1.99	3.72	6987	6433	488
GGR039A	65.54	66.54	1.99	2.69	4.68	6987	6433	487
GGR039A	66.54	67.54	1.21	0.41	1.62	6987	6433	486

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR039A	67.54	68.54	0.91	0.89	1.80	6987	6433	485
GGR039A	68.54	69.54	0.66	1.28	1.94	6987	6433	484
GGR039A	69.54	70.54	0.44	1.17	1.61	6987	6433	483
GGR039A	70.54	71.54	0.39	1.29	1.68	6987	6433	482
GGR039A	71.54	72.54	0.34	1.41	1.75	6987	6433	481
GGR039A	72.54	73.54	0.73	0.39	1.12	6987	6433	480
GGR039A	73.54	74.54	0.57	0.62	1.19	6987	6433	479
GGR039A	74.54	75.54	1.27	0.40	1.67	6987	6433	478
GGR039A	75.54	76.54	0.36	0.21	0.57	6987	6433	477
GGR039A	76.54	77.54	0.79	0.41	1.20	6987	6433	476
GGR039A	77.54	78.54	2.03	1.19	3.22	6987	6433	475
GGR039A	78.54	79.54	2.15	0.51	2.67	6987	6433	474
GGR039A	79.54	80.54	1.70	0.31	2.01	6987	6433	473
GGR039A	80.54	81.54	0.87	0.12	0.99	6987	6433	472
GGR039A	81.54	82.54	0.40	0.10	0.50	6987	6433	471
GGR039A	82.54	83.54	0.28	0.09	0.36	6987	6433	470
GGR039A	83.54	84.54	0.22	0.06	0.28	6987	6433	469
GGR039A	84.54	85.54	0.46	0.45	0.91	6987	6433	468
GGR039A	85.54	86.54	0.64	0.55	1.20	6987	6433	467
GGR039A	86.54	87.54	0.96	0.54	1.50	6987	6433	466
GGR039A	87.54	88.54	1.50	0.95	2.45	6987	6433	465
GGR039A	88.54	89.54	1.60	1.11	2.71	6987	6433	464
GGR039A	89.54	90.54	1.25	1.20	2.45	6987	6433	463
GGR039A	90.54	91.54	1.51	1.24	2.75	6987	6433	462
GGR039A	91.54	92.54	1.88	1.52	3.40	6987	6433	461
GGR039A	92.54	93.54	3.19	2.88	6.07	6987	6433	460
GGR039A	94.54	95.54	1.90	0.45	2.35	6987	6433	458
GGR039A	95.54	96.54	1.03	0.31	1.34	6987	6433	457
GGR039A	96.54	97.54	0.43	0.22	0.65	6987	6433	456
GGR039A	97.54	98.54	1.79	0.02	1.81	6987	6433	455
GGR040	71.55	72.55	0.99	0.50	1.49	6882	6762	474
GGR040	72.55	73.55	0.85	0.33	1.18	6882	6762	473
GGR040	73.55	74.55	1.18	0.53	1.71	6882	6762	472
GGR040	74.55	75.55	0.82	0.69	1.51	6882	6762	471
GGR040	75.55	76.55	0.08	0.75	0.83	6882	6762	470
GGR040	76.55	77.55	0.06	0.70	0.76	6882	6762	469
GGR040	77.55	78.55	0.32	0.56	0.88	6882	6762	468
GGR040	78.55	79.55	0.57	0.44	1.01	6882	6762	467
GGR046	73.48	74.48	0.25	0.80	1.05	6899	6393	476
GGR046	74.48	75.48	0.32	0.86	1.18	6899	6393	475
GGR046	75.48	76.48	0.40	0.92	1.32	6899	6393	474
GGR046	76.48	77.48	0.04	1.05	1.09	6899	6393	473
GGR046	77.48	78.48	0.09	1.12	1.21	6899	6393	472
GGR046	78.48	79.48	0.18	1.20	1.38	6899	6393	471
GGR046	79.48	80.48	0.10	0.85	0.94	6899	6393	470
GGR046	80.48	81.48	0.07	1.01	1.07	6899	6393	469

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR046	81.48	82.48	0.03	1.33	1.36	6899	6393	468
GGR046	82.48	83.48	0.27	1.40	1.67	6899	6393	467
GGR046	83.48	84.48	0.31	1.41	1.72	6899	6393	466
GGR079	27.37	28.37	1.19	0.04	1.23	6878	6271	508
GGR079	28.37	29.37	0.37	0.63	1.01	6878	6271	507
GGR079	29.37	30.37	0.20	0.44	0.64	6878	6271	506
GGR079	30.37	31.37	1.26	0.93	2.19	6878	6271	505
GGR079	31.37	32.37	2.09	1.51	3.60	6878	6271	504
GGR079	32.37	33.37	1.32	1.03	2.35	6878	6271	503
GGR081	28.32	29.32	2.42	0.07	2.49	6868	6180	511
GGR081	29.32	30.32	0.91	0.17	1.08	6868	6180	510
GGR081	30.32	31.32	1.76	0.42	2.18	6868	6180	509
GGR081	31.32	32.32	1.93	0.52	2.45	6868	6180	508
GGR081	32.32	33.32	2.21	0.90	3.11	6868	6180	507
GGR081	33.32	34.32	1.25	0.62	1.87	6868	6180	506
GGR081	34.32	35.32	0.94	0.57	1.51	6868	6180	505
GGR081	35.32	36.32	0.77	0.66	1.43	6868	6180	504
GGR081	36.32	37.32	0.53	0.73	1.27	6868	6180	503
GGR081	37.32	38.32	0.45	0.76	1.21	6868	6180	502
GGR087	16.86	17.86	1.36	0.17	1.53	6758	6187	515
GGR087	17.86	18.86	1.62	0.41	2.03	6758	6187	514
GGR087	18.86	19.86	0.30	0.14	0.44	6758	6187	513
GGR087	19.86	20.86	0.45	0.39	0.84	6758	6187	512
GGR112	71.63	72.63	0.86	0.74	1.60	6941	6457	480
GGR112	72.63	73.63	0.61	0.90	1.51	6941	6457	479
GGR112	73.63	74.63	0.72	0.28	1.01	6941	6457	478
GGR112	74.63	75.63	0.67	0.20	0.87	6941	6457	477
GGR112	75.63	76.63	0.38	0.35	0.73	6941	6457	476
GGR112	76.63	77.63	0.94	0.33	1.28	6941	6457	475
GGR112	77.63	78.63	0.64	0.20	0.83	6941	6457	474
GGR112	78.63	79.63	0.01	0.01	0.02	6941	6457	473
GGR112	79.63	80.63	0.11	0.01	0.12	6941	6457	472
GGR112	80.63	81.63	0.09	0.02	0.12	6941	6457	471
GGR112	81.63	82.63	0.04	0.05	0.09	6941	6457	470
GGR112	82.63	83.63	0.02	0.49	0.52	6941	6457	469
GGR112	83.63	84.63	0.02	1.02	1.04	6941	6457	468
GGR112	84.63	85.63	0.03	0.92	0.95	6941	6457	467
GGR112	85.63	86.63	0.08	0.30	0.39	6941	6457	466
GGR112	86.63	87.63	0.14	0.72	0.87	6941	6457	465
GGR112	87.63	88.63	0.10	0.75	0.86	6941	6457	464
GGR112	88.63	89.63	0.22	0.84	1.05	6941	6457	463
GGR112	89.63	90.63	0.32	1.51	1.83	6941	6457	462
GGR113A	76.26	77.26	0.83	0.39	1.22	6952	6315	466
GGR113A	77.26	78.26	0.70	0.47	1.17	6952	6315	465
GGR113A	78.26	79.26	0.60	0.55	1.15	6952	6315	464
GGR113A	79.26	80.26	3.13	2.71	5.83	6952	6315	463

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR113A	80.26	81.26	0.60	0.94	1.54	6952	6315	462
GGR116	65.53	66.53	1.43	0.52	1.95	7063	6455	478
GGR116	66.53	67.53	2.92	1.20	4.12	7063	6455	477
GGR116	67.53	68.53	3.49	1.98	5.47	7063	6455	476
GGR116	68.53	69.53	0.15	0.33	0.48	7063	6455	475
GGR116	69.53	70.53	0.20	0.33	0.53	7063	6455	474
GGR116	70.53	71.53	0.37	0.37	0.74	7063	6455	473
GGR116	71.53	72.53	0.13	0.48	0.61	7063	6455	472
GGR116	72.53	73.53	0.12	0.35	0.46	7063	6455	471
GGR116	73.53	74.53	0.14	0.11	0.25	7063	6455	470
GGR116	74.53	75.53	0.35	0.39	0.74	7063	6455	469
GGR116	75.53	76.53	0.56	0.69	1.25	7063	6455	468
GGR116	76.53	77.53	2.00	0.89	2.89	7063	6455	467
GGR116	77.53	78.53	1.52	0.63	2.15	7063	6455	466
GGR116	78.53	79.53	0.84	0.29	1.13	7063	6455	465
GGR117	78.67	79.67	0.92	0.51	1.43	7064	6577	466
GGR117	79.67	80.67	1.10	1.01	2.11	7064	6577	465
GGR117	80.67	81.67	0.92	0.75	1.67	7064	6577	464
GGR117	81.67	82.67	1.05	0.57	1.62	7064	6577	463
GGR118	73.15	74.15	2.25	0.90	3.15	6942	6578	480
GGR118	74.15	75.15	2.47	1.31	3.78	6942	6578	479
GGR118	75.15	76.15	2.80	1.18	3.98	6942	6578	478
GGR118	76.15	77.15	0.46	0.30	0.76	6942	6578	477
GGR118	77.15	78.15	0.18	0.35	0.53	6942	6578	476
GGR118	78.15	79.15	0.90	0.30	1.20	6942	6578	475
GGR124	122.71	123.71	3.94	0.01	3.95	6817	6833	424
GGR124	123.71	124.71	4.09	0.02	4.11	6817	6833	423
GGR124	124.71	125.71	0.55	0.01	0.56	6817	6833	422
GGR125	44.20	45.20	0.41	1.60	2.01	6696	6938	495
GGR125	45.20	46.20	0.27	1.44	1.71	6696	6938	494
GGR125	46.20	47.20	0.38	1.13	1.51	6696	6938	493
GGR125	47.20	48.20	0.37	0.47	0.83	6696	6938	492
GGR125	48.20	49.20	0.34	1.68	2.02	6696	6938	491
GGR125	49.20	50.20	0.33	3.37	3.70	6696	6938	490
GGR125	50.20	51.20	0.47	2.67	3.14	6696	6938	489
GGR125	51.20	52.20	0.12	2.58	2.71	6696	6938	488
GGR125	52.20	53.20	0.70	2.99	3.69	6696	6938	487
GGR125	53.20	54.20	4.41	1.69	6.10	6696	6938	486
GGR125	54.20	55.20	1.13	1.75	2.88	6696	6938	485
GGR125	55.20	56.20	1.11	2.71	3.83	6696	6938	484
GGR125	56.20	57.20	0.32	0.57	0.89	6696	6938	483
GGR125	57.20	58.20	1.19	0.79	1.98	6696	6938	482
GGR125	58.20	59.20	0.83	1.08	1.92	6696	6938	481
GGR125	59.20	60.20	0.63	1.20	1.83	6696	6938	480
GGR125	60.20	61.20	1.78	1.24	3.02	6696	6938	479
GGR125	61.20	62.20	1.58	1.06	2.64	6696	6938	478

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR125	62.20	63.20	1.15	0.93	2.09	6696	6938	477
GGR125	63.20	64.20	1.37	0.57	1.95	6696	6938	476
GGR126	44.10	45.10	0.43	1.75	2.19	6818	6695	504
GGR126	45.10	46.10	0.85	1.92	2.77	6818	6695	503
GGR126	46.10	47.10	0.05	0.72	0.77	6818	6695	502
GGR126	47.10	48.10	0.43	1.62	2.05	6818	6695	501
GGR126	48.10	49.10	0.20	0.96	1.16	6818	6695	500
GGR126	49.10	50.10	0.28	1.39	1.67	6818	6695	499
GGR126	50.10	51.10	0.10	1.54	1.65	6818	6695	498
GGR126	51.10	52.10	0.06	1.58	1.64	6818	6695	497
GGR129	80.07	81.07	3.33	4.36	7.69	6702	6816	468
GGR129	81.07	82.07	4.10	3.97	8.08	6702	6816	467
GGR129	82.07	83.07	2.96	2.52	5.47	6702	6816	466
GGR129	83.07	84.07	0.78	1.77	2.55	6702	6816	465
GGR129	84.07	85.07	0.66	1.34	2.01	6702	6816	464
GGR129	85.07	86.07	0.07	0.57	0.64	6702	6816	463
GGR129	86.07	87.07	0.05	1.43	1.48	6702	6816	462
GGR130	42.46	43.46	1.82	1.40	3.22	6826	6576	515
GGR130	43.46	44.46	1.64	1.53	3.18	6826	6576	514
GGR130	44.46	45.46	1.29	1.56	2.84	6826	6576	513
GGR130	45.46	46.46	1.31	1.45	2.77	6826	6576	512
GGR130	46.46	47.46	1.36	1.42	2.78	6826	6576	511
GGR130	47.46	48.46	1.50	2.05	3.55	6826	6576	510
GGR130	48.46	49.46	5.54	3.95	9.49	6826	6576	509
GGR130	49.46	50.46	4.71	4.84	9.56	6826	6576	508
GGR130	50.46	51.46	1.43	3.74	5.17	6826	6576	507
GGR130	51.46	52.46	1.38	1.97	3.36	6826	6576	506
GGR133	34.75	35.75	0.01	2.27	2.28	6694	6697	517
GGR133	35.75	36.75	0.01	2.50	2.51	6694	6697	516
GGR133	36.75	37.75	0.01	2.94	2.95	6694	6697	515
GGR133	37.75	38.75	0.02	3.30	3.32	6694	6697	514
GGR133	38.75	39.75	0.03	2.22	2.25	6694	6697	513
GGR133	39.75	40.75	0.06	1.12	1.18	6694	6697	512
GGR133	40.75	41.75	0.05	1.01	1.06	6694	6697	511
GGR133	41.75	42.75	0.01	1.01	1.02	6694	6697	510
GGR133	42.75	43.75	0.01	1.07	1.08	6694	6697	509
GGR133	43.75	44.75	0.01	1.01	1.03	6694	6697	508
GGR133	44.75	45.75	0.02	0.78	0.80	6694	6697	507
GGR133	45.75	46.75	0.03	1.42	1.44	6694	6697	506
GGR133	46.75	47.75	0.03	1.43	1.45	6694	6697	505
GGR133	47.75	48.75	0.01	0.61	0.62	6694	6697	504
GGR133	48.75	49.75	0.01	1.07	1.08	6694	6697	503
GGR133	49.75	50.75	0.01	1.21	1.22	6694	6697	502
GGR133	50.75	51.75	0.01	1.36	1.37	6694	6697	501
GGR135	26.00	27.00	2.50	0.53	3.03	6812	6216	511
GGR135	27.00	28.00	4.20	0.99	5.19	6812	6216	510

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR135	28.00	29.00	1.62	0.50	2.12	6812	6216	509
GGR135	29.00	30.00	0.72	0.35	1.06	6812	6216	508
GGR135	30.00	31.00	0.46	0.32	0.78	6812	6216	507
GGR135	31.00	32.00	0.70	0.34	1.04	6812	6216	506
GGR135	32.00	33.00	0.43	0.51	0.94	6812	6216	505
GGR135	33.00	34.00	0.43	0.51	0.94	6812	6216	504
GGR135	34.00	35.00	0.43	0.51	0.94	6812	6216	503
GGR135	35.00	36.00	0.79	0.75	1.54	6812	6216	502
GGR135	36.00	37.00	0.60	0.66	1.26	6812	6216	501
GGR135	37.00	38.00	0.50	0.58	1.08	6812	6216	500
GGR135	38.00	39.00	2.59	1.29	3.88	6812	6216	499
GGR136	25.60	26.60	0.97	0.35	1.32	6814	6092	505
GGR136	26.60	27.60	1.42	0.57	1.98	6814	6092	504
GGR136	27.60	28.60	1.92	0.81	2.73	6814	6092	503
GGR136	28.60	29.60	1.14	0.34	1.48	6814	6092	502
GGR146	45.11	46.11	1.49	0.03	1.52	6940	6098	487
GGR146	46.11	47.11	1.01	0.04	1.05	6940	6098	486
GGR146	47.11	48.11	0.49	0.05	0.54	6940	6098	485
GGR146	48.11	49.11	1.13	0.02	1.15	6940	6098	484
GGR157	43.28	44.28	1.97	6.82	8.79	6576	6943	494
GGR157	44.28	45.28	0.96	4.36	5.32	6576	6943	493
GGR157	45.28	46.28	0.05	0.46	0.50	6576	6943	492
GGR157	46.28	47.28	0.25	1.58	1.83	6576	6943	491
GGR157	47.28	48.28	0.52	3.42	3.94	6576	6943	490
GGR158	21.52	22.52	0.01	1.80	1.81	6575	6817	524
GGR158	22.52	23.52	0.01	1.15	1.16	6575	6817	523
GGR158	23.52	24.52	0.01	0.86	0.87	6575	6817	522
GGR158	24.52	25.52	0.01	1.12	1.13	6575	6817	521
GGR158	25.52	26.52	0.01	1.22	1.23	6575	6817	520
GGR158	26.52	27.52	0.01	1.27	1.28	6575	6817	519
GGR158	27.52	28.52	0.01	1.12	1.13	6575	6817	518
GGR158	28.52	29.52	0.33	6.44	6.77	6575	6817	517
GGR158	29.52	30.52	0.01	0.50	0.51	6575	6817	516
GGR158	30.52	31.52	0.23	0.83	1.06	6575	6817	515
GGR158	31.52	32.52	0.80	1.67	2.47	6575	6817	514
GGR158	32.52	33.52	1.15	2.11	3.25	6575	6817	513
GGR158	33.52	34.52	1.03	1.96	2.99	6575	6817	512
GGR158	34.52	35.52	0.26	0.97	1.23	6575	6817	511
GGR158	35.52	36.52	0.20	0.91	1.11	6575	6817	510
GGR158	36.52	37.52	0.16	0.91	1.07	6575	6817	509
GGR158	37.52	38.52	0.12	1.01	1.13	6575	6817	508
GGR166	23.10	24.10	1.00	0.51	1.51	6821	6152	513
GGR166	24.10	25.10	1.18	2.00	3.18	6821	6152	512
GGR166	25.10	26.10	1.26	0.67	1.93	6821	6152	511
GGR167	26.21	27.21	1.12	0.04	1.16	6851	6152	513
GGR167	27.21	28.21	2.73	0.31	3.04	6851	6152	512

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR167	28.21	29.21	4.54	0.61	5.15	6851	6152	511
GGR167	29.21	30.21	4.42	0.51	4.93	6851	6152	510
GGR167	30.21	31.21	2.17	0.74	2.90	6851	6152	509
GGR167	31.21	32.21	3.30	1.00	4.30	6851	6152	508
GGR167	32.21	33.21	2.20	0.63	2.83	6851	6152	507
GGR167	33.21	34.21	2.15	0.82	2.97	6851	6152	506
GGR167	34.21	35.21	1.90	0.77	2.67	6851	6152	505
GGR167	35.21	36.21	1.56	0.59	2.15	6851	6152	504
GGR167	36.21	37.21	1.07	0.64	1.72	6851	6152	503
GGR167	37.21	38.21	0.79	0.67	1.46	6851	6152	502
GGR168	30.18	31.18	0.59	1.02	1.61	6906	6155	506
GGR168	31.18	32.18	0.61	0.82	1.43	6906	6155	505
GGR168	32.18	33.18	0.45	0.86	1.31	6906	6155	504
GGR168	33.18	34.18	0.68	0.90	1.58	6906	6155	503
GGR168	34.18	35.18	0.73	0.87	1.60	6906	6155	502
GGR168	35.18	36.18	0.27	0.51	0.78	6906	6155	501
GGR168	36.18	37.18	0.89	0.44	1.33	6906	6155	500
GGR168	37.18	38.18	1.27	0.39	1.66	6906	6155	499
GGR168	38.18	39.18	0.93	0.34	1.27	6906	6155	498
GGR168	39.18	40.18	1.01	0.32	1.34	6906	6155	497
GGR168	40.18	41.18	1.06	0.31	1.37	6906	6155	496
GGR168	41.18	42.18	0.53	0.23	0.76	6906	6155	495
GGR168	42.18	43.18	0.41	0.21	0.63	6906	6155	494
GGR168	43.18	44.18	0.30	0.20	0.50	6906	6155	493
GGR168	44.18	45.18	0.63	0.37	1.00	6906	6155	492
GGR171	26.40	27.40	1.25	0.61	1.85	6815	6275	511
GGR171	27.40	28.40	1.07	0.69	1.77	6815	6275	510
GGR171	28.40	29.40	1.50	0.78	2.28	6815	6275	509
GGR172	28.38	29.38	2.06	1.69	3.75	6845	6275	509
GGR172	29.38	30.38	1.27	1.51	2.78	6845	6275	508
GGR172	30.38	31.38	1.95	1.65	3.60	6845	6275	507
GGR172	31.38	32.38	4.31	1.18	5.49	6845	6275	506
GGR172	32.38	33.38	3.43	1.84	5.27	6845	6275	505
GGR172	33.38	34.38	2.31	2.03	4.34	6845	6275	504
GGR173	32.61	33.61	0.96	0.60	1.56	6907	6275	504
GGR173	33.61	34.61	0.97	0.56	1.53	6907	6275	503
GGR173	34.61	35.61	0.98	0.51	1.49	6907	6275	502
GGR173	35.61	36.61	1.51	1.17	2.68	6907	6275	501
GGR173	36.61	37.61	1.44	1.04	2.48	6907	6275	500
GGR173	37.61	38.61	1.31	0.81	2.12	6907	6275	499
GGR176	65.44	66.44	1.05	1.36	2.41	6883	6482	490
GGR176	66.44	67.44	1.25	0.73	1.97	6883	6482	489
GGR176	67.44	68.44	0.93	0.77	1.70	6883	6482	488
GGR176	68.44	69.44	0.57	0.83	1.40	6883	6482	487
GGR176	69.44	70.44	2.54	1.77	4.31	6883	6482	486
GGR176	70.44	71.44	0.11	0.95	1.06	6883	6482	485

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR176	71.44	72.44	0.36	0.86	1.22	6883	6482	484
GGR176	72.44	73.44	0.53	0.81	1.34	6883	6482	483
GGR176	73.44	74.44	0.77	0.84	1.61	6883	6482	482
GGR176	74.44	75.44	0.38	0.42	0.80	6883	6482	481
GGR176	75.44	76.44	0.10	0.16	0.25	6883	6482	480
GGR176	76.44	77.44	0.03	0.77	0.80	6883	6482	479
GGR176	77.44	78.44	0.03	1.80	1.83	6883	6482	478
GGR176	78.44	79.44	0.06	1.17	1.23	6883	6482	477
GGR176	79.44	80.44	0.07	1.36	1.43	6883	6482	476
GGR176	80.44	81.44	0.07	1.62	1.70	6883	6482	475
GGR176	81.44	82.44	0.15	1.70	1.85	6883	6482	474
GGR176	82.44	83.44	0.13	2.24	2.36	6883	6482	473
GGR176	83.44	84.44	0.11	2.71	2.82	6883	6482	472
GGR177	47.55	48.55	0.07	1.18	1.25	6913	6484	508
GGR177	48.55	49.55	0.07	1.03	1.10	6913	6484	507
GGR177	49.55	50.55	0.05	0.30	0.35	6913	6484	506
GGR177	50.55	51.55	1.13	1.67	2.80	6913	6484	505
GGR177	51.55	52.55	1.00	2.29	3.30	6913	6484	504
GGR177	52.55	53.55	17.94	4.83	22.77	6913	6484	503
GGR177	53.55	54.55	1.54	1.45	2.99	6913	6484	502
GGR177	54.55	55.55	1.22	1.52	2.73	6913	6484	501
GGR177	55.55	56.55	1.15	1.60	2.75	6913	6484	500
GGR177	56.55	57.55	1.56	1.88	3.44	6913	6484	499
GGR177	57.55	58.55	1.22	1.25	2.47	6913	6484	498
GGR177	58.55	59.55	0.97	0.92	1.89	6913	6484	497
GGR177	59.55	60.55	0.46	1.08	1.54	6913	6484	496
GGR177	60.55	61.55	0.37	0.75	1.12	6913	6484	495
GGR177	61.55	62.55	0.30	0.50	0.80	6913	6484	494
GGR177	62.55	63.55	0.30	0.30	0.60	6913	6484	493
GGR177	63.55	64.55	0.47	0.71	1.18	6913	6484	492
GGR177	64.55	65.55	0.63	1.07	1.69	6913	6484	491
GGR177	65.55	66.55	1.86	1.55	3.41	6913	6484	490
GGR177	66.55	67.55	6.03	1.88	7.91	6913	6484	489
GGR177	67.55	68.55	2.58	1.30	3.88	6913	6484	488
GGR177	68.55	69.55	0.84	1.42	2.26	6913	6484	487
GGR178	41.45	42.45	0.02	1.08	1.10	6943	6483	514
GGR178	42.45	43.45	0.03	0.73	0.76	6943	6483	513
GGR178	43.45	44.45	1.41	1.31	2.72	6943	6483	512
GGR178	44.45	45.45	3.40	2.18	5.58	6943	6483	511
GGR178	45.45	46.45	1.60	1.55	3.14	6943	6483	510
GGR178	46.45	47.45	1.16	1.69	2.85	6943	6483	509
GGR178	47.45	48.45	0.82	2.10	2.92	6943	6483	508
GGR178	48.45	49.45	1.61	1.71	3.32	6943	6483	507
GGR178	49.45	50.45	1.70	1.41	3.11	6943	6483	506
GGR178	50.45	51.45	1.55	0.92	2.47	6943	6483	505
GGR178	51.45	52.45	1.63	1.92	3.54	6943	6483	504

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR178	52.45	53.45	1.55	2.06	3.61	6943	6483	503
GGR178	53.45	54.45	1.28	1.72	3.00	6943	6483	502
GGR178	54.45	55.45	1.73	1.15	2.88	6943	6483	501
GGR178	55.45	56.45	1.78	0.94	2.72	6943	6483	500
GGR178	56.45	57.45	1.36	0.91	2.27	6943	6483	499
GGR178	57.45	58.45	0.77	0.59	1.35	6943	6483	498
GGR179	40.75	41.75	0.30	0.88	1.18	6972	6482	514
GGR179	41.75	42.75	0.51	1.66	2.18	6972	6482	513
GGR179	42.75	43.75	0.75	2.55	3.30	6972	6482	512
GGR179	43.75	44.75	1.51	1.93	3.44	6972	6482	511
GGR179	44.75	45.75	2.78	2.48	5.27	6972	6482	510
GGR179	45.75	46.75	0.73	1.74	2.46	6972	6482	509
GGR179	46.75	47.75	1.55	2.20	3.75	6972	6482	508
GGR179	47.75	48.75	2.29	1.80	4.08	6972	6482	507
GGR179	48.75	49.75	1.72	1.52	3.24	6972	6482	506
GGR179	49.75	50.75	0.62	1.13	1.75	6972	6482	505
GGR179	50.75	51.75	1.65	2.35	4.00	6972	6482	504
GGR179	51.75	52.75	1.60	2.04	3.64	6972	6482	503
GGR179	52.75	53.75	1.10	0.91	2.01	6972	6482	502
GGR179	53.75	54.75	0.85	0.56	1.41	6972	6482	501
GGR179	54.75	55.75	0.75	0.63	1.38	6972	6482	500
GGR179	55.75	56.75	0.65	1.03	1.68	6972	6482	499
GGR179	56.75	57.75	0.52	1.29	1.82	6972	6482	498
GGR179	57.75	58.75	0.46	1.18	1.64	6972	6482	497
GGR179	58.75	59.75	0.41	0.51	0.92	6972	6482	496
GGR181	39.01	40.01	0.97	0.66	1.63	7032	6482	511
GGR181	40.01	41.01	0.61	0.66	1.27	7032	6482	510
GGR181	41.01	42.01	0.20	0.67	0.87	7032	6482	509
GGR181	42.01	43.01	0.43	0.93	1.35	7032	6482	508
GGR181	43.01	44.01	0.54	0.71	1.25	7032	6482	507
GGR181	44.01	45.01	0.68	0.39	1.07	7032	6482	506
GGR181	45.01	46.01	0.77	0.39	1.16	7032	6482	505
GGR181	46.01	47.01	0.50	0.31	0.81	7032	6482	504
GGR181	47.01	48.01	0.03	0.18	0.21	7032	6482	503
GGR181	48.01	49.01	0.26	0.32	0.58	7032	6482	502
GGR181	49.01	50.01	0.53	0.36	0.89	7032	6482	501
GGR181	50.01	51.01	1.01	0.39	1.40	7032	6482	500
GGR181	51.01	52.01	1.03	0.54	1.58	7032	6482	499
GGR181	52.01	53.01	1.03	0.61	1.64	7032	6482	498
GGR181	53.01	54.01	0.99	0.70	1.69	7032	6482	497
GGR182	42.98	43.98	0.02	0.97	0.98	6847	6483	511
GGR182	43.98	44.98	0.04	0.99	1.03	6847	6483	510
GGR182	44.98	45.98	0.34	3.36	3.70	6847	6483	509
GGR182	45.98	46.98	0.96	2.44	3.40	6847	6483	508
GGR182	46.98	47.98	0.62	1.90	2.52	6847	6483	507
GGR182	47.98	48.98	1.25	3.68	4.93	6847	6483	506

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR182	48.98	49.98	4.36	5.76	10.11	6847	6483	505
GGR183	40.52	41.52	6.46	4.28	10.74	6897	6538	517
GGR183	41.52	42.52	0.52	3.27	3.79	6897	6538	516
GGR183	42.52	43.52	0.33	2.80	3.13	6897	6538	515
GGR183	43.52	44.52	1.82	2.84	4.65	6897	6538	514
GGR183	44.52	45.52	9.91	3.46	13.37	6897	6538	513
GGR183	45.52	46.52	2.88	3.30	6.18	6897	6538	512
GGR183	46.52	47.52	0.70	2.19	2.89	6897	6538	511
GGR183	47.52	48.52	3.81	4.24	8.04	6897	6538	510
GGR183	48.52	49.52	1.54	3.11	4.65	6897	6538	509
GGR183	49.52	50.52	0.37	2.35	2.72	6897	6538	508
GGR183	50.52	51.52	1.13	3.26	4.39	6897	6538	507
GGR183	51.52	52.52	1.96	2.85	4.81	6897	6538	506
GGR183	52.52	53.52	0.73	0.79	1.52	6897	6538	505
GGR183	53.52	54.52	2.20	1.90	4.10	6897	6538	504
GGR183	54.52	55.52	1.79	1.40	3.19	6897	6538	503
GGR183	55.52	56.52	0.94	0.53	1.48	6897	6538	502
GGR183	56.52	57.52	1.40	1.48	2.88	6897	6538	501
GGR183	57.52	58.52	1.55	1.62	3.17	6897	6538	500
GGR183	58.52	59.52	1.99	1.63	3.62	6897	6538	499
GGR183	59.52	60.52	2.06	1.41	3.47	6897	6538	498
GGR184	39.78	40.78	0.80	3.68	4.48	6919	6556	516
GGR184	40.78	41.78	0.18	2.31	2.49	6919	6556	515
GGR184	41.78	42.78	0.20	1.58	1.77	6919	6556	514
GGR184	42.78	43.78	0.64	1.95	2.58	6919	6556	513
GGR184	43.78	44.78	0.54	1.38	1.92	6919	6556	512
GGR184	44.78	45.78	1.25	0.42	1.67	6919	6556	511
GGR184	45.78	46.78	1.12	0.53	1.65	6919	6556	510
GGR184	46.78	47.78	0.93	0.70	1.63	6919	6556	509
GGR190	32.80	33.80	0.03	1.08	1.12	6731	6614	522
GGR190	33.80	34.80	0.01	1.81	1.82	6731	6614	521
GGR190	34.80	35.80	0.01	1.62	1.63	6731	6614	520
GGR190	35.80	36.80	0.01	1.68	1.69	6731	6614	519
GGR190	36.80	37.80	0.01	0.17	0.18	6731	6614	518
GGR190	37.80	38.80	0.01	0.13	0.14	6731	6614	517
GGR190	38.80	39.80	0.70	0.89	1.59	6731	6614	516
GGR190	39.80	40.80	1.10	1.34	2.44	6731	6614	515
GGR191	31.39	32.39	0.01	1.46	1.47	6776	6656	522
GGR191	32.39	33.39	0.04	1.29	1.33	6776	6656	521
GGR191	33.39	34.39	0.07	1.10	1.17	6776	6656	520
GGR191	34.39	35.39	0.08	1.51	1.59	6776	6656	519
GGR191	35.39	36.39	0.08	1.33	1.41	6776	6656	518
GGR191	36.39	37.39	0.08	1.06	1.14	6776	6656	517
GGR191	37.39	38.39	0.10	1.22	1.32	6776	6656	516
GGR191	38.39	39.39	0.12	1.59	1.71	6776	6656	515
GGR191	39.39	40.39	0.97	3.30	4.27	6776	6656	514

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR191	40.39	41.39	0.98	2.65	3.62	6776	6656	513
GGR191	41.39	42.39	0.21	1.01	1.22	6776	6656	512
GGR191	42.39	43.39	0.01	0.67	0.68	6776	6656	511
GGR191	43.39	44.39	0.06	0.65	0.71	6776	6656	510
GGR191	44.39	45.39	0.11	0.62	0.73	6776	6656	509
GGR191	45.39	46.39	0.12	0.88	1.00	6776	6656	508
GGR191	46.39	47.39	0.15	0.87	1.01	6776	6656	507
GGR191	47.39	48.39	0.18	0.84	1.02	6776	6656	506
GGR192	29.50	30.50	0.01	1.24	1.25	6797	6678	521
GGR192	30.50	31.50	0.01	2.49	2.50	6797	6678	520
GGR192	31.50	32.50	0.01	3.99	4.00	6797	6678	519
GGR192	32.50	33.50	0.52	2.66	3.18	6797	6678	518
GGR192	33.50	34.50	2.30	5.25	7.55	6797	6678	517
GGR192	34.50	35.50	0.87	4.10	4.98	6797	6678	516
GGR192	35.50	36.50	0.19	3.03	3.22	6797	6678	515
GGR192	36.50	37.50	0.13	2.11	2.24	6797	6678	514
GGR192	37.50	38.50	0.31	2.26	2.57	6797	6678	513
GGR192	38.50	39.50	0.35	1.92	2.27	6797	6678	512
GGR192	39.50	40.50	0.36	1.56	1.92	6797	6678	511
GGR192	40.50	41.50	0.35	2.43	2.78	6797	6678	510
GGR192	41.50	42.50	1.45	5.02	6.48	6797	6678	509
GGR192	42.50	43.50	0.64	3.22	3.86	6797	6678	508
GGR192	43.50	44.50	0.13	1.81	1.94	6797	6678	507
GGR192	44.50	45.50	0.15	0.83	0.98	6797	6678	506
GGR192	45.50	46.50	0.32	1.52	1.84	6797	6678	505
GGR192	46.50	47.50	0.41	1.88	2.29	6797	6678	504
GGR192	47.50	48.50	0.16	0.50	0.67	6797	6678	503
GGR192	48.50	49.50	0.16	0.59	0.75	6797	6678	502
GGR192	49.50	50.50	0.14	0.80	0.93	6797	6678	501
GGR192	50.50	51.50	0.01	0.75	0.76	6797	6678	500
GGR192	51.50	52.50	0.01	0.92	0.93	6797	6678	499
GGR192	52.50	53.50	0.01	1.01	1.02	6797	6678	498
GGR192	53.50	54.50	0.01	1.08	1.09	6797	6678	497
GGR192	54.50	55.50	0.01	0.89	0.90	6797	6678	496
GGR192	55.50	56.50	0.01	1.17	1.18	6797	6678	495
GGR192	56.50	57.50	0.01	1.80	1.81	6797	6678	494
GGR192	57.50	58.50	0.01	2.08	2.09	6797	6678	493
GGR192	58.50	59.50	0.01	1.65	1.66	6797	6678	492
GGR192	59.50	60.50	0.01	1.13	1.14	6797	6678	491
GGR193	38.10	39.10	2.24	1.34	3.58	6842	6719	509
GGR193	39.10	40.10	3.11	2.98	6.09	6842	6719	508
GGR193	40.10	41.10	1.80	2.35	4.15	6842	6719	507
GGR193	41.10	42.10	0.40	0.59	1.00	6842	6719	506
GGR193	42.10	43.10	0.40	0.62	1.03	6842	6719	505
GGR193	43.10	44.10	0.50	0.79	1.29	6842	6719	504
GGR193	44.10	45.10	1.81	0.54	2.35	6842	6719	503

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR193	45.10	46.10	1.96	0.51	2.47	6842	6719	502
GGR193	46.10	47.10	1.96	0.51	2.47	6842	6719	501
GGR193	47.10	48.10	1.96	0.51	2.47	6842	6719	500
GGR193	48.10	49.10	0.83	0.41	1.24	6842	6719	499
GGR193	49.10	50.10	0.73	1.60	2.33	6842	6719	498
GGR193	50.10	51.10	2.17	3.94	6.11	6842	6719	497
GGR193	51.10	52.10	1.29	2.65	3.93	6842	6719	496
GGR193	52.10	53.10	2.17	3.29	5.47	6842	6719	495
GGR193	53.10	54.10	2.83	3.69	6.52	6842	6719	494
GGR193	54.10	55.10	1.86	1.50	3.36	6842	6719	493
GGR193	55.10	56.10	3.82	3.73	7.54	6842	6719	492
GGR193	56.10	57.10	2.42	4.16	6.58	6842	6719	491
GGR193	57.10	58.10	0.58	1.25	1.83	6842	6719	490
GGR193	58.10	59.10	0.17	0.64	0.81	6842	6719	489
GGR193	59.10	60.10	0.19	0.63	0.82	6842	6719	488
GGR193	60.10	61.10	0.31	0.93	1.24	6842	6719	487
GGR193	61.10	62.10	0.99	1.30	2.29	6842	6719	486
GGR193	62.10	63.10	1.01	1.13	2.14	6842	6719	485
GGR205	29.87	30.87	0.01	1.23	1.24	6610	6706	525
GGR205	30.87	31.87	0.01	1.92	1.93	6610	6706	524
GGR205	31.87	32.87	0.01	1.64	1.65	6610	6706	523
GGR205	32.87	33.87	0.01	1.24	1.25	6610	6706	522
GGR205	33.87	34.87	0.01	0.71	0.72	6610	6706	521
GGR205	34.87	35.87	0.02	0.23	0.25	6610	6706	520
GGR205	35.87	36.87	0.07	0.39	0.46	6610	6706	519
GGR205	36.87	37.87	0.54	0.92	1.46	6610	6706	518
GGR205	37.87	38.87	0.42	0.72	1.14	6610	6706	517
GGR206	31.12	32.12	0.01	2.12	2.13	6654	6779	517
GGR206	32.12	33.12	0.01	1.02	1.03	6654	6779	516
GGR206	33.12	34.12	0.03	1.21	1.25	6654	6779	515
GGR206	34.12	35.12	0.05	1.92	1.97	6654	6779	514
GGR206	35.12	36.12	0.05	2.65	2.70	6654	6779	513
GGR206	36.12	37.12	0.05	1.84	1.89	6654	6779	512
GGR206	37.12	38.12	0.05	1.07	1.12	6654	6779	511
GGR206	38.12	39.12	0.15	1.43	1.58	6654	6779	510
GGR206	39.12	40.12	0.27	1.45	1.72	6654	6779	509
GGR206	40.12	41.12	0.55	1.19	1.74	6654	6779	508
GGR206	41.12	42.12	0.31	0.74	1.05	6654	6779	507
GGR206	42.12	43.12	0.18	0.54	0.72	6654	6779	506
GGR206	43.12	44.12	0.01	0.39	0.40	6654	6779	505
GGR206	44.12	45.12	0.10	0.54	0.65	6654	6779	504
GGR206	45.12	46.12	0.12	0.70	0.83	6654	6779	503
GGR206	46.12	47.12	0.13	0.96	1.09	6654	6779	502
GGR206	47.12	48.12	0.13	0.32	0.45	6654	6779	501
GGR206	48.12	49.12	0.61	0.85	1.47	6654	6779	500
GGR206	49.12	50.12	1.03	1.20	2.23	6654	6779	499

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR206	50.12	51.12	0.71	0.19	0.90	6654	6779	498
GGR206	51.12	52.12	0.35	0.24	0.59	6654	6779	497
GGR206	52.12	53.12	0.19	0.25	0.45	6654	6779	496
GGR206	53.12	54.12	0.48	0.68	1.17	6654	6779	495
GGR206	54.12	55.12	0.53	1.21	1.74	6654	6779	494
GGR206	55.12	56.12	0.41	1.80	2.21	6654	6779	493
GGR206	56.12	57.12	0.41	2.00	2.41	6654	6779	492
GGR206	57.12	58.12	0.47	1.63	2.09	6654	6779	491
GGR206	58.12	59.12	0.57	0.91	1.48	6654	6779	490
GGR206	59.12	60.12	1.39	0.85	2.24	6654	6779	489
GGR206	60.12	61.12	1.29	0.49	1.78	6654	6779	488
GGR206	61.12	62.12	1.09	0.65	1.74	6654	6779	487
GGR206	62.12	63.12	0.63	1.12	1.75	6654	6779	486
GGR206	63.12	64.12	0.24	1.04	1.29	6654	6779	485
GGR206	64.12	65.12	0.10	1.00	1.10	6654	6779	484
GGR208	98.37	99.37	18.54	9.12	27.66	6719	6847	446
GGR208	99.37	100.37	3.74	1.51	5.25	6719	6847	445
GGR208	100.37	101.37	4.50	2.14	6.63	6719	6847	444
GGR208	101.37	102.37	0.59	0.45	1.04	6719	6847	443
GGR208	102.37	103.37	2.86	1.92	4.78	6719	6847	442
GGR208	103.37	104.37	6.30	3.53	9.83	6719	6847	441
GGR208	104.37	105.37	2.10	0.65	2.75	6719	6847	440
GGR209	110.79	111.79	4.60	2.86	7.46	6741	6869	433
GGR209	111.79	112.79	0.47	1.68	2.15	6741	6869	432
GGR209	112.79	113.79	1.95	2.94	4.89	6741	6869	431
GGR209	113.79	114.79	5.56	4.58	10.14	6741	6869	430
GGR209	114.79	115.79	1.49	0.39	1.87	6741	6869	429
GGR211	25.88	26.88	0.19	1.96	2.15	6634	6879	517
GGR211	26.88	27.88	0.34	2.56	2.90	6634	6879	516
GGR211	27.88	28.88	0.51	3.20	3.71	6634	6879	515
GGR211	28.88	29.88	1.08	1.50	2.58	6634	6879	514
GGR211	29.88	30.88	2.34	1.75	4.09	6634	6879	513
GGR211	30.88	31.88	0.59	2.61	3.20	6634	6879	512
GGR211	31.88	32.88	1.31	2.23	3.54	6634	6879	511
GGR211	32.88	33.88	1.74	1.98	3.72	6634	6879	510
GGR211	33.88	34.88	1.75	1.94	3.69	6634	6879	509
GGR211	34.88	35.88	1.58	2.03	3.61	6634	6879	508
GGR211	35.88	36.88	1.14	1.79	2.92	6634	6879	507
GGR211	36.88	37.88	0.19	1.18	1.37	6634	6879	506
GGR211	37.88	38.88	0.60	1.13	1.73	6634	6879	505
GGR211	38.88	39.88	0.70	1.15	1.86	6634	6879	504
GGR211	39.88	40.88	0.68	1.25	1.93	6634	6879	503
GGR211	40.88	41.88	0.24	1.03	1.27	6634	6879	502
GGR211	41.88	42.88	0.10	1.03	1.14	6634	6879	501
GGR211	42.88	43.88	0.19	1.35	1.54	6634	6879	500
GGR211	43.88	44.88	0.26	1.83	2.09	6634	6879	499

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR211	44.88	45.88	0.27	2.26	2.53	6634	6879	498
GGR211	45.88	46.88	0.09	3.39	3.48	6634	6879	497
GGR211	46.88	47.88	0.09	1.73	1.82	6634	6879	496
GGR211	47.88	48.88	0.09	0.81	0.90	6634	6879	495
GGR211	48.88	49.88	0.08	0.93	1.01	6634	6879	494
GGR211	49.88	50.88	0.06	1.57	1.63	6634	6879	493
GGR211	50.88	51.88	0.09	2.58	2.66	6634	6879	492
GGR211	51.88	52.88	0.84	11.30	12.14	6634	6879	491
GGR211	52.88	53.88	0.39	6.82	7.21	6634	6879	490
GGR211	53.88	54.88	0.01	2.98	2.99	6634	6879	489
GGR211	54.88	55.88	0.01	2.05	2.06	6634	6879	488
GGR211	55.88	56.88	0.01	1.86	1.87	6634	6879	487
GGR213	48.16	49.16	0.29	1.12	1.41	6675	6921	492
GGR213	49.16	50.16	1.36	3.29	4.65	6675	6921	491
GGR213	50.16	51.16	2.52	5.65	8.17	6675	6921	490
GGR213	51.16	52.16	0.29	2.93	3.22	6675	6921	489
GGR213	52.16	53.16	0.15	2.16	2.32	6675	6921	488
GGR213	53.16	54.16	0.13	1.33	1.46	6675	6921	487
GGR214	61.72	62.72	0.53	0.44	0.97	6728	6972	474
GGR214	62.72	63.72	0.31	1.03	1.34	6728	6972	473
GGR214	63.72	64.72	0.07	1.69	1.76	6728	6972	472
GGR214	64.72	65.72	0.11	2.23	2.34	6728	6972	471
GGR214	65.72	66.72	0.18	1.70	1.88	6728	6972	470
GGR214	66.72	67.72	0.27	0.95	1.22	6728	6972	469
GGR215	65.47	66.47	12.97	4.08	17.05	6750	6998	472
GGR215	66.47	67.47	0.71	1.90	2.61	6750	6998	471
GGR215	67.47	68.47	2.11	0.91	3.02	6750	6998	470
GGR216	58.83	59.83	3.92	0.01	3.93	6788	7041	458
GGR216	59.83	60.83	0.96	0.01	0.97	6788	7041	457
GGR216	60.83	61.83	0.12	0.01	0.13	6788	7041	456
GGR217	96.62	97.62	0.05	3.53	3.57	6947	6395	454
GGR217	97.62	98.62	0.07	5.93	6.00	6947	6395	453
GGR217	98.62	99.62	0.11	3.85	3.96	6947	6395	452
GGR217	99.62	100.62	0.69	1.67	2.37	6947	6395	451
GGR217	100.62	101.62	1.08	2.30	3.38	6947	6395	450
GGR217	101.62	102.62	0.47	1.31	1.78	6947	6395	449
GGR217	102.62	103.62	0.46	0.64	1.10	6947	6395	448
GGR217	103.62	104.62	0.23	0.33	0.55	6947	6395	447
GGR217	104.62	105.62	0.30	0.57	0.87	6947	6395	446
GGR217	105.62	106.62	0.52	1.13	1.65	6947	6395	445
GGR217	106.62	107.62	0.31	0.74	1.04	6947	6395	444
GGR217	107.62	108.62	0.23	0.59	0.82	6947	6395	443
GGR217	108.62	109.62	0.64	1.17	1.81	6947	6395	442
GGR217	109.62	110.62	2.79	2.68	5.47	6947	6395	441
GGR217	110.62	111.62	4.89	3.87	8.76	6947	6395	440
GGR217	111.62	112.62	3.94	2.70	6.64	6947	6395	439

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR217	112.62	113.62	2.47	1.08	3.55	6947	6395	438
GGR217	113.62	114.62	2.47	1.08	3.55	6947	6395	437
GGR217	114.62	115.62	2.27	0.81	3.08	6947	6395	436
GGR217	115.62	116.62	2.12	0.79	2.91	6947	6395	435
GGR217	116.62	117.62	2.27	1.17	3.44	6947	6395	434
GGR217	117.62	118.62	2.45	2.36	4.81	6947	6395	433
GGR217	118.62	119.62	0.62	0.50	1.12	6947	6395	432
GGR217	119.62	120.62	2.52	0.89	3.40	6947	6395	431
GGR217	120.62	121.62	4.43	1.29	5.72	6947	6395	430
GGR219	22.56	23.56	0.01	1.07	1.08	6599	6845	522
GGR219	23.56	24.56	0.03	1.57	1.59	6599	6845	521
GGR219	24.56	25.56	0.02	1.64	1.67	6599	6845	520
GGR219	25.56	26.56	0.01	1.47	1.48	6599	6845	519
GGR219	26.56	27.56	0.11	1.98	2.09	6599	6845	518
GGR219	27.56	28.56	0.12	2.06	2.18	6599	6845	517
GGR219	28.56	29.56	0.06	1.66	1.72	6599	6845	516
GGR219	29.56	30.56	0.09	1.60	1.69	6599	6845	515
GGR219	30.56	31.56	0.11	1.51	1.62	6599	6845	514
GGR219	31.56	32.56	0.12	1.20	1.32	6599	6845	513
GGR219	32.56	33.56	0.15	1.00	1.14	6599	6845	512
GGR219	33.56	34.56	0.16	0.88	1.04	6599	6845	511
GGR222	26.82	27.82	1.85	0.18	2.03	6851	6097	510
GGR222	27.82	28.82	1.02	0.22	1.23	6851	6097	509
GGR222	28.82	29.82	1.23	0.68	1.91	6851	6097	508
GGR222	29.82	30.82	1.47	0.93	2.40	6851	6097	507
GGR222	30.82	31.82	1.45	1.00	2.45	6851	6097	506
GGR222	31.82	32.82	1.63	0.72	2.35	6851	6097	505
GGR222	32.82	33.82	1.01	0.19	1.20	6851	6097	504
S0992-07	44.00	45.00	0.56	3.50	4.06	6894	6585	512
S0992-07	45.00	46.00	2.06	2.38	4.44	6894	6585	511
S0992-07	46.00	47.00	2.80	1.38	4.18	6894	6585	510
S0992-07	47.00	48.00	1.29	0.62	1.91	6894	6585	509
S0992-07	48.00	49.00	0.36	0.46	0.82	6894	6585	508
S0992-07	49.00	50.00	0.33	0.00	0.33	6894	6585	507
S0992-07	50.00	51.00	0.20	0.09	0.30	6894	6585	506
S0992-07	51.00	52.00	0.10	0.16	0.26	6894	6585	505
S0992-07	52.00	53.00	0.09	0.03	0.12	6894	6585	504
S0992-07	53.00	54.00	0.19	0.04	0.22	6894	6585	503
S0992-07	54.00	55.00	0.12	0.03	0.16	6894	6585	502
S0992-07	55.00	56.00	0.44	0.58	1.02	6894	6585	501
S0992-07	56.00	57.00	0.25	0.11	0.36	6894	6585	500
S0992-07	57.00	58.00	0.42	0.30	0.72	6894	6585	499
S0992-07	58.00	59.00	0.22	0.29	0.51	6894	6585	498
S0992-07	59.00	60.00	0.21	0.15	0.36	6894	6585	497
S0992-07	60.00	61.00	0.42	0.42	0.84	6894	6585	496
S0992-07	61.00	62.00	0.92	0.35	1.27	6894	6585	495

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S0992-07	62.00	63.00	1.13	0.39	1.52	6894	6585	494
S0992-07	63.00	64.00	0.51	0.26	0.77	6894	6585	493
S0992-07	64.00	65.00	0.69	0.41	1.10	6894	6585	492
S0993-07	80.00	81.00	0.21	0.75	0.96	6929	6618	469
S0993-07	81.00	82.00	0.20	0.97	1.17	6929	6618	468
S0993-07	82.00	83.00	0.13	2.60	2.73	6929	6618	467
S0993-07	83.00	84.00	2.50	0.68	3.18	6929	6618	466
S0994-07	41.00	42.00	0.32	2.90	3.22	6856	6555	516
S0994-07	42.00	43.00	0.07	0.51	0.58	6856	6555	515
S0994-07	43.00	44.00	0.18	0.73	0.91	6856	6555	514
S0994-07	44.00	45.00	0.06	0.38	0.44	6856	6555	513
S0994-07	45.00	46.00	0.28	1.15	1.43	6856	6555	512
S0994-07	46.00	47.00	0.37	0.66	1.03	6856	6555	511
S0994-07	47.00	48.00	1.57	1.52	3.09	6856	6555	510
S0994-07	48.00	49.00	3.30	2.06	5.36	6856	6555	509
S0994-07	49.00	50.00	1.31	1.05	2.36	6856	6555	508
S0994-07	50.00	51.00	1.28	1.20	2.48	6856	6555	507
S0994-07	51.00	52.00	1.17	1.54	2.71	6856	6555	506
S0994-07	52.00	53.00	0.25	1.01	1.26	6856	6555	505
S0994-07	53.00	54.00	0.31	0.83	1.14	6856	6555	504
S0995-07	44.00	45.00	0.34	0.87	1.21	6822	6522	511
S0995-07	45.00	46.00	0.29	1.72	2.01	6822	6522	510
S0995-07	46.00	47.00	0.30	1.68	1.98	6822	6522	509
S0995-07	47.00	48.00	1.19	2.20	3.39	6822	6522	508
S0995-07	48.00	49.00	1.22	2.70	3.92	6822	6522	507
S0995-07	49.00	50.00	1.23	2.50	3.73	6822	6522	506
S0995-07	50.00	51.00	0.15	0.43	0.58	6822	6522	505
S0995-07	51.00	52.00	0.03	0.16	0.19	6822	6522	504
S0995-07	52.00	53.00	0.13	0.43	0.56	6822	6522	503
S0995-07	53.00	54.00	0.46	0.61	1.07	6822	6522	502
S0995-07	54.00	55.00	0.69	2.36	3.05	6822	6522	501
S0995-07	55.00	56.00	1.44	2.18	3.62	6822	6522	500
S0995-07	56.00	57.00	1.84	1.97	3.81	6822	6522	499
S0995-07	57.00	58.00	2.98	1.65	4.62	6822	6522	498
S0995-07	58.00	59.00	0.98	0.70	1.68	6822	6522	497
S0995-07	59.00	60.00	0.62	0.31	0.93	6822	6522	496
S0995-07	60.00	61.00	0.86	0.50	1.36	6822	6522	495
S0996-07	40.00	41.00	0.51	1.34	1.85	6848	6596	516
S0996-07	41.00	42.00	0.09	0.16	0.25	6848	6596	515
S0996-07	42.00	43.00	0.00	0.25	0.25	6848	6596	514
S0996-07	43.00	44.00	0.00	0.58	0.58	6848	6596	513
S0996-07	44.00	45.00	0.31	1.11	1.42	6848	6596	512
S0996-07	45.00	46.00	1.60	3.10	4.70	6848	6596	511
S0996-07	46.00	47.00	0.61	0.86	1.47	6848	6596	510
S0996-07	47.00	48.00	1.08	1.29	2.37	6848	6596	509
S0996-07	48.00	49.00	3.40	1.51	4.91	6848	6596	508

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S0996-07	49.00	50.00	1.80	0.65	2.45	6848	6596	507
S0996-07	50.00	51.00	1.47	0.79	2.26	6848	6596	506
S0997-07	39.60	40.60	0.64	0.28	0.92	6931	6509	516
S0997-07	40.60	41.60	0.57	1.22	1.80	6931	6509	515
S0997-07	41.60	42.60	1.38	2.19	3.57	6931	6509	514
S0997-07	42.60	43.60	1.85	1.58	3.44	6931	6509	513
S0997-07	43.60	44.60	4.80	1.61	6.41	6931	6509	512
S0997-07	44.60	45.60	8.66	2.18	10.84	6931	6509	511
S0997-07	45.60	46.60	7.20	2.18	9.38	6931	6509	510
S0997-07	46.60	47.60	3.34	2.23	5.57	6931	6509	509
S0997-07	47.60	48.60	1.94	3.08	5.02	6931	6509	508
S0997-07	48.60	49.60	1.75	2.53	4.27	6931	6509	507
S0997-07	49.60	50.60	1.29	1.41	2.70	6931	6509	506
S0997-07	50.60	51.60	0.86	0.80	1.67	6931	6509	505
S0997-07	51.60	52.60	0.69	1.45	2.14	6931	6509	504
S0997-07	52.60	53.60	1.45	2.67	4.12	6931	6509	503
S0997-07	53.60	54.60	3.01	2.31	5.33	6931	6509	502
S0997-07	54.60	55.60	1.89	1.32	3.21	6931	6509	501
S0997-07	55.60	56.60	0.97	1.02	1.98	6931	6509	500
S0997-07	56.60	57.60	0.75	0.82	1.57	6931	6509	499
S0997-07	57.60	58.60	0.42	0.64	1.06	6931	6509	498
S0998-07	38.00	39.00	0.31	1.10	1.41	6781	6593	519
S0998-07	39.00	40.00	1.47	1.81	3.28	6781	6593	518
S0998-07	40.00	41.00	1.08	2.21	3.29	6781	6593	517
S0998-07	41.00	42.00	1.51	2.22	3.73	6781	6594	516
S0998-07	42.00	43.00	1.51	1.44	2.95	6781	6594	515
S0998-07	43.00	44.00	0.65	1.33	1.98	6781	6594	514
S0998-07	44.00	45.00	0.86	1.92	2.78	6781	6594	513
S0998-07	45.00	46.00	0.22	0.92	1.14	6781	6594	512
S0998-07	46.00	47.00	0.45	0.67	1.12	6781	6594	511
S0998-07	47.00	48.00	0.26	0.71	0.97	6781	6594	510
S0999-07	38.00	39.00	0.25	1.23	1.48	6814	6624	517
S0999-07	39.00	40.00	0.63	1.73	2.36	6814	6624	516
S0999-07	40.00	41.00	0.29	1.61	1.90	6814	6624	515
S0999-07	41.00	42.00	0.26	1.38	1.64	6814	6624	514
S0999-07	42.00	43.00	0.33	1.03	1.36	6814	6624	513
S0999-07	43.00	44.00	1.87	1.52	3.39	6814	6624	512
S0999-07	44.00	45.00	0.47	1.48	1.95	6814	6623	511
S0999-07	45.00	46.00	0.42	2.02	2.44	6814	6623	510
S0999-07	46.00	47.00	1.10	1.32	2.42	6814	6623	509
S0999-07	47.00	48.00	1.81	0.75	2.56	6814	6623	508
S0999-07	48.00	49.00	0.38	0.36	0.74	6814	6622	507
S0999-07	49.00	50.00	0.00	0.23	0.23	6814	6622	507
S0999-07	50.00	51.00	0.17	0.17	0.34	6814	6622	506
S0999-07	51.00	52.00	0.00	0.24	0.24	6814	6621	505
S0999-07	52.00	53.00	2.70	2.18	4.88	6814	6621	504

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S0999-07	53.00	54.00	0.49	0.58	1.07	6813	6621	503
S1000-07	79.00	80.00	0.00	0.95	0.95	6886	6687	466
S1000-07	80.00	81.00	0.32	1.51	1.83	6886	6687	465
S1000-07	81.00	82.00	0.00	1.20	1.20	6886	6687	464
S1001-07	34.00	35.00	1.33	1.84	3.17	6845	6659	515
S1001-07	35.00	36.00	3.20	2.35	5.55	6845	6659	514
S1001-07	36.00	37.00	1.28	4.00	5.28	6845	6659	513
S1001-07	37.00	38.00	5.00	3.60	8.60	6845	6659	512
S1001-07	38.00	39.00	1.81	2.49	4.30	6845	6659	511
S1001-07	39.00	40.00	1.16	1.45	2.61	6845	6659	510
S1001-07	40.00	41.00	2.01	1.01	3.02	6845	6659	509
S1001-07	41.00	42.00	3.50	0.95	4.45	6845	6659	508
S1001-07	42.00	43.00	2.70	0.65	3.35	6845	6659	507
S1001-07	43.00	44.00	1.30	0.31	1.61	6845	6659	506
S1001-07	44.00	45.00	2.00	0.53	2.53	6845	6659	505
S1001-07	45.00	46.00	1.18	0.33	1.51	6845	6659	504
S1001-07	46.00	47.00	0.66	0.00	0.66	6845	6659	503
S1001-07	47.00	48.00	0.33	0.00	0.33	6845	6659	502
S1001-07	48.00	49.00	1.53	0.74	2.27	6845	6659	501
S1001-07	49.00	50.00	0.59	0.68	1.27	6845	6659	500
S1004-07	33.00	34.00	0.00	1.10	1.10	6753	6685	519
S1004-07	34.00	35.00	0.00	2.37	2.37	6753	6685	518
S1004-07	35.00	36.00	0.00	1.81	1.81	6753	6685	517
S1004-07	36.00	37.00	0.00	5.20	5.20	6753	6685	516
S1004-07	37.00	38.00	0.00	5.40	5.40	6753	6685	515
S1004-07	38.00	39.00	0.00	4.70	4.70	6753	6685	514
S1004-07	39.00	40.00	0.37	2.40	2.77	6753	6685	513
S1004-07	40.00	41.00	0.00	1.83	1.83	6753	6685	512
S1004-07	41.00	42.00	0.00	1.30	1.30	6752	6685	511
S1004-07	42.00	43.00	0.00	1.78	1.78	6752	6685	510
S1004-07	43.00	44.00	0.09	0.23	0.32	6752	6685	509
S1004-07	44.00	45.00	0.00	0.84	0.84	6752	6685	508
S1004-07	45.00	46.00	0.00	1.65	1.65	6752	6685	507
S1004-07	46.00	47.00	0.00	0.46	0.46	6752	6685	506
S1004-07	47.00	48.00	0.00	4.80	4.80	6752	6685	505
S1004-07	48.00	49.00	0.00	0.47	0.47	6752	6685	504
S1004-07	49.00	50.00	0.06	0.20	0.26	6752	6685	503
S1004-07	50.00	51.00	0.00	0.57	0.57	6752	6685	502
S1004-07	51.00	52.00	0.00	0.53	0.53	6752	6685	501
S1004-07	52.00	53.00	0.00	0.59	0.59	6752	6685	500
S1004-07	53.00	54.00	0.01	0.16	0.17	6752	6685	499
S1004-07	54.00	55.00	0.00	0.19	0.19	6752	6685	498
S1004-07	55.00	56.00	0.00	3.20	3.20	6752	6685	497
S1004-07	56.00	57.00	0.00	2.06	2.06	6752	6685	496
S1004-07	57.00	58.00	0.00	1.27	1.27	6752	6685	495
S1004-07	58.00	59.00	0.00	3.10	3.10	6752	6685	494

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1004-07	59.00	60.00	0.00	1.16	1.16	6752	6685	493
S1005-07	31.00	32.00	0.00	3.60	3.60	6722	6645	523
S1005-07	32.00	33.00	0.00	1.56	1.56	6722	6645	522
S1005-07	33.00	34.00	0.00	0.81	0.81	6722	6645	521
S1005-07	34.00	35.00	0.00	0.88	0.88	6722	6645	520
S1005-07	35.00	36.00	0.00	0.55	0.55	6722	6645	519
S1005-07	36.00	37.00	0.01	0.01	0.02	6722	6645	518
S1005-07	37.00	38.00	0.02	0.19	0.22	6722	6645	517
S1005-07	38.00	39.00	0.00	0.54	0.54	6722	6645	516
S1005-07	39.00	40.00	0.00	1.94	1.94	6722	6645	515
S1005-07	40.00	41.00	0.00	3.30	3.30	6722	6645	514
S1005-07	41.00	42.00	0.00	4.00	4.00	6722	6645	513
S1005-07	42.00	43.00	0.00	2.05	2.05	6722	6645	512
S1005-07	43.00	44.00	0.00	1.72	1.72	6722	6645	511
S1005-07	44.00	45.00	0.00	3.80	3.80	6722	6645	510
S1005-07	45.00	46.00	0.00	2.22	2.22	6722	6645	509
S1006-07	39.00	40.00	0.00	2.01	2.01	6687	6626	518
S1006-07	40.00	41.00	0.00	0.92	0.92	6687	6626	517
S1006-07	41.00	42.00	0.00	1.26	1.26	6687	6626	516
S1007-07	41.00	42.00	0.00	1.01	1.01	6678	6663	514
S1007-07	42.00	43.00	0.00	1.03	1.03	6678	6663	513
S1007-07	43.00	44.00	0.00	1.21	1.21	6678	6663	512
S1010-07	35.00	36.00	0.00	1.87	1.87	6615	6667	523
S1010-07	36.00	37.00	0.00	0.60	0.60	6615	6667	522
S1010-07	37.00	38.00	0.00	0.67	0.67	6615	6667	521
S1010-07	38.00	39.00	0.00	0.52	0.52	6615	6667	520
S1010-07	39.00	40.00	0.41	0.38	0.79	6615	6667	519
S1010-07	40.00	41.00	0.00	1.20	1.20	6615	6667	518
S1010-07	41.00	42.00	0.00	0.93	0.93	6615	6667	517
S1010-07	42.00	43.00	0.00	1.29	1.29	6615	6667	516
S1011-07	40.00	41.00	0.00	1.06	1.06	6659	6708	511
S1011-07	41.00	42.00	0.00	0.80	0.80	6659	6708	510
S1011-07	42.00	43.00	0.00	1.20	1.20	6659	6708	509
S1011-07	43.00	44.00	0.00	0.93	0.93	6659	6708	508
S1011-07	44.00	45.00	0.00	1.63	1.63	6659	6708	507
S1011-07	45.00	46.00	0.00	2.27	2.27	6659	6707	506
S1011-07	46.00	47.00	0.00	2.44	2.44	6659	6707	505
S1011-07	47.00	48.00	0.35	1.35	1.70	6659	6707	504
S1011-07	48.00	49.00	2.29	2.08	4.37	6659	6707	503
S1012-07	53.00	54.00	0.30	0.36	0.66	6682	6743	495
S1012-07	54.00	55.00	0.52	1.31	1.84	6682	6743	494
S1012-07	55.00	56.00	0.53	0.44	0.97	6682	6743	493
S1017-07	28.00	29.00	0.00	1.11	1.11	6618	6792	521
S1017-07	29.00	30.00	0.00	3.00	3.00	6618	6792	520
S1017-07	30.00	31.00	0.00	2.03	2.03	6618	6792	519
S1017-07	31.00	32.00	0.00	3.90	3.90	6618	6792	518

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1017-07	32.00	33.00	0.00	3.80	3.80	6618	6792	517
S1017-07	33.00	34.00	0.00	2.50	2.50	6618	6792	516
S1017-07	34.00	35.00	0.00	2.24	2.24	6618	6792	515
S1017-07	35.00	36.00	0.00	2.20	2.20	6618	6792	514
S1017-07	36.00	37.00	1.06	3.60	4.66	6618	6792	513
S1017-07	37.00	38.00	0.48	2.70	3.18	6618	6792	512
S1017-07	38.00	39.00	1.76	3.80	5.56	6618	6792	511
S1017-07	39.00	40.00	1.29	2.21	3.50	6618	6792	510
S1017-07	40.00	41.00	0.95	1.84	2.79	6618	6792	509
S1017-07	41.00	42.00	0.46	0.68	1.14	6618	6792	508
S1017-07	42.00	43.00	1.33	2.09	3.42	6618	6792	507
S1017-07	43.00	44.00	0.55	1.28	1.83	6618	6792	506
S1018-07	31.00	32.00	0.00	1.50	1.50	6610	6750	520
S1018-07	32.00	33.00	0.00	1.67	1.67	6610	6750	519
S1018-07	33.00	34.00	0.00	1.11	1.11	6610	6750	518
S1018-07	34.00	35.00	0.00	0.94	0.94	6610	6750	517
S1018-07	35.00	36.00	0.48	0.97	1.45	6610	6750	516
S1019-07	55.50	56.50	3.65	4.28	7.93	6717	6770	492
S1019-07	56.50	57.50	1.07	6.93	8.00	6717	6770	491
S1019-07	57.50	58.50	2.13	8.85	10.98	6717	6770	490
S1019-07	58.50	59.50	2.76	8.40	11.16	6717	6770	489
S1019-07	59.50	60.50	1.90	7.65	9.55	6717	6770	488
S1019-07	60.50	61.50	0.20	4.30	4.50	6717	6770	487
S1019-07	61.50	62.50	0.14	6.50	6.64	6717	6770	486
S1019-07	62.50	63.50	2.04	9.45	11.49	6717	6770	485
S1019-07	63.50	64.50	2.56	7.30	9.86	6717	6770	484
S1019-07	64.50	65.50	1.42	3.92	5.34	6717	6770	483
S1019-07	65.50	66.50	1.68	2.13	3.80	6717	6770	482
S1019-07	66.50	67.50	1.06	2.02	3.07	6717	6770	481
S1019-07	67.50	68.50	0.41	2.27	2.68	6717	6769	480
S1019-07	68.50	69.50	0.70	2.24	2.94	6717	6769	479
S1020-07	65.00	66.00	2.80	6.50	9.30	6686	6840	480
S1020-07	66.00	67.00	1.03	10.50	11.53	6686	6840	479
S1020-07	67.00	68.00	2.00	7.40	9.40	6686	6840	478
S1020-07	68.00	69.00	2.23	1.87	4.10	6686	6840	477
S1020-07	69.00	70.00	0.62	1.15	1.77	6686	6840	476
S1020-07	70.00	71.00	6.30	5.50	11.80	6686	6840	475
S1020-07	71.00	72.00	0.00	1.36	1.36	6686	6840	474
S1020-07	72.00	73.00	0.00	1.03	1.03	6686	6840	473
S1020-07	73.00	74.00	0.92	2.50	3.42	6686	6840	472
S1020-07	74.00	75.00	0.64	2.44	3.08	6686	6840	471
S1020-07	75.00	76.00	0.48	4.40	4.88	6686	6840	470
S1021-07	32.79	33.79	0.01	0.06	0.07	6731	6615	522
S1021-07	33.79	34.79	0.02	0.03	0.05	6731	6615	521
S1021-07	34.79	35.79	0.01	0.02	0.03	6731	6615	520
S1021-07	35.79	36.79	0.00	0.01	0.01	6731	6615	519

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1023-07	50.20	51.20	1.76	5.00	6.76	6682	6794	498
S1023-07	51.20	52.20	4.50	5.98	10.48	6682	6794	497
S1023-07	52.20	53.20	4.10	6.22	10.32	6682	6794	496
S1023-07	53.20	54.20	0.77	3.82	4.59	6682	6794	495
S1023-07	54.20	55.20	0.24	1.52	1.76	6682	6794	494
S1023-07	55.20	56.20	0.19	0.14	0.33	6682	6794	493
S1023-07	56.20	57.20	0.99	0.72	1.71	6682	6794	492
S1023-07	57.20	58.20	1.21	1.15	2.36	6682	6794	491
S1023-07	58.20	59.20	0.47	0.37	0.84	6682	6794	490
S1023-07	59.20	60.20	0.76	0.46	1.23	6682	6794	489
S1023-07	60.20	61.20	2.02	1.57	3.59	6682	6794	488
S1023-07	61.20	62.20	1.74	3.54	5.28	6682	6794	487
S1023-07	62.20	63.20	0.53	5.46	5.99	6682	6794	486
S1023-07	63.20	64.20	0.70	2.66	3.36	6682	6794	485
S1023-07	64.20	65.20	1.15	1.62	2.77	6682	6794	484
S1023-07	65.20	66.20	1.99	1.90	3.90	6682	6794	483
S1023-07	66.20	67.20	5.82	4.06	9.88	6682	6794	482
S1023-07	67.20	68.20	0.25	2.21	2.46	6682	6794	481
S1023-07	68.20	69.20	0.00	3.36	3.36	6682	6794	480
S1023-07	69.20	70.20	0.00	3.20	3.20	6682	6794	479
S1024-07	100.60	101.60	15.20	2.90	18.10	6727	6815	446
S1024-07	101.60	102.60	9.86	3.44	13.30	6727	6815	445
S1024-07	102.60	103.60	4.62	2.65	7.27	6727	6815	444
S1024-07	103.60	104.60	1.95	2.80	4.74	6727	6815	443
S1024-07	104.60	105.60	1.73	3.46	5.19	6727	6815	442
S1024-07	105.60	106.60	1.47	3.26	4.73	6727	6815	441
S1024-07	106.60	107.60	2.89	1.97	4.86	6727	6815	440
S1024-07	107.60	108.60	4.26	1.14	5.40	6727	6815	439
S1024-07	108.60	109.60	5.98	0.44	6.42	6727	6815	438
S1024-07	109.60	110.60	4.48	0.00	4.48	6727	6815	437
S1024-07	110.60	111.60	1.10	0.00	1.10	6727	6815	436
S1024-07	111.60	112.60	2.10	0.00	2.10	6727	6815	435
S1025-07	49.00	50.00	0.90	0.64	1.54	6651	6898	492
S1025-07	50.00	51.00	1.47	0.48	1.95	6651	6898	491
S1025-07	51.00	52.00	3.10	1.80	4.90	6651	6898	490
S1025-07	52.00	53.00	1.17	7.70	8.87	6651	6898	489
S1025-07	53.00	54.00	1.08	6.40	7.48	6651	6898	488
S1025-07	54.00	55.00	0.00	1.93	1.93	6651	6898	487
S1025-07	55.00	56.00	0.00	1.28	1.28	6651	6898	486
S1025-07	56.00	57.00	0.00	1.69	1.69	6651	6898	485
S1025-07	57.00	58.00	0.00	1.90	1.90	6651	6898	484
S1026-07	45.00	46.00	0.00	0.96	0.96	6622	6932	494
S1026-07	46.00	47.00	0.78	1.97	2.75	6622	6932	493
S1026-07	47.00	48.00	1.00	2.80	3.80	6622	6932	492
S1026-07	48.00	49.00	0.71	2.08	2.79	6622	6932	491
S1026-07	49.00	50.00	0.26	1.75	2.01	6622	6932	490

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1026-07	50.00	51.00	0.00	1.61	1.61	6622	6932	489
S1027-07	29.00	30.00	0.49	0.51	1.00	6597	6897	512
S1027-07	30.00	31.00	0.72	1.92	2.64	6597	6897	511
S1027-07	31.00	32.00	0.46	1.15	1.61	6597	6897	510
S1027-07	32.00	33.00	2.30	2.01	4.31	6597	6897	509
S1027-07	33.00	34.00	1.64	2.33	3.97	6597	6897	508
S1027-07	34.00	35.00	3.20	1.73	4.93	6597	6897	507
S1027-07	35.00	36.00	0.80	0.94	1.74	6597	6897	506
S1027-07	36.00	37.00	0.50	0.44	0.94	6597	6897	505
S1028-07	26.00	27.00	0.03	1.36	1.39	6628	6864	517
S1028-07	27.00	28.00	0.03	0.92	0.95	6628	6864	516
S1028-07	28.00	29.00	0.01	2.41	2.42	6628	6863	515
S1028-07	29.00	30.00	0.18	2.28	2.46	6628	6863	514
S1028-07	30.00	31.00	0.34	2.70	3.04	6628	6863	513
S1028-07	31.00	32.00	0.70	4.00	4.70	6628	6863	512
S1028-07	32.00	33.00	0.34	5.40	5.74	6628	6863	511
S1028-07	33.00	34.00	0.18	1.29	1.47	6628	6863	510
S1028-07	34.00	35.00	0.03	0.73	0.76	6628	6863	509
S1028-07	35.00	36.00	0.06	0.51	0.57	6628	6863	508
S1028-07	36.00	37.00	0.65	1.53	2.18	6628	6863	507
S1028-07	37.00	38.00	0.78	1.06	1.84	6628	6863	506
S1028-07	38.00	39.00	0.14	1.35	1.49	6628	6863	505
S1028-07	39.00	40.00	0.36	1.73	2.09	6628	6863	504
S1028-07	40.00	41.00	0.33	2.34	2.67	6628	6863	503
S1028-07	41.00	42.00	0.22	2.42	2.64	6628	6863	502
S1028-07	42.00	43.00	0.61	1.07	1.68	6628	6863	501
S1028-07	43.00	44.00	0.61	0.49	1.10	6628	6863	500
S1029-07	64.10	65.10	2.03	4.98	7.01	6696	6897	478
S1029-07	65.10	66.10	4.32	7.68	12.00	6696	6897	477
S1029-07	66.10	67.10	0.01	1.55	1.56	6696	6897	476
S1029-07	67.10	68.10	0.09	4.82	4.91	6696	6897	475
S1029-07	68.10	69.10	0.63	4.74	5.37	6696	6897	474
S1029-07	69.10	70.10	0.35	2.54	2.89	6696	6897	473
S1029-07	70.10	71.10	1.37	3.65	5.02	6696	6897	472
S1029-07	71.10	72.10	2.07	2.34	4.41	6696	6897	471
S1029-07	72.10	73.10	0.44	1.55	1.99	6696	6897	470
S1029-07	73.10	74.10	1.18	0.60	1.78	6696	6897	469
S1030-07	25.30	26.30	0.01	1.83	1.84	6565	6857	518
S1030-07	26.30	27.30	0.00	1.62	1.62	6565	6857	517
S1030-07	27.30	28.30	0.00	2.33	2.33	6565	6857	516
S1030-07	28.30	29.30	0.00	1.97	1.97	6565	6857	515
S1030-07	29.30	30.30	0.00	2.92	2.92	6565	6857	514
S1030-07	30.30	31.30	0.00	2.64	2.65	6565	6857	513
S1030-07	31.30	32.30	0.06	2.65	2.72	6565	6857	512
S1030-07	32.30	33.30	0.20	1.55	1.75	6565	6857	511
S1030-07	33.30	34.30	0.17	0.87	1.04	6565	6857	510

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1030-07	34.30	35.30	0.07	1.05	1.12	6565	6857	509
S1030-07	35.30	36.30	0.01	1.20	1.21	6565	6857	508
S1030-07	36.30	37.30	0.01	0.40	0.41	6565	6857	507
S1030-07	37.30	38.30	0.01	0.37	0.38	6565	6857	506
S1030-07	38.30	39.30	0.47	0.76	1.24	6565	6857	505
S1030-07	39.30	40.30	1.12	1.48	2.60	6565	6857	504
S1030-07	40.30	41.30	0.03	0.34	0.37	6565	6857	503
S1030-07	41.30	42.30	0.06	0.86	0.92	6565	6857	502
S1030-07	42.30	43.30	0.16	1.32	1.48	6565	6857	501
S1031-07	88.75	89.75	3.30	7.10	10.40	6750	6795	458
S1031-07	89.75	90.75	2.30	9.28	11.57	6750	6795	457
S1031-07	90.75	91.75	0.90	5.13	6.02	6750	6795	456
S1031-07	91.75	92.75	2.31	1.67	3.98	6750	6795	455
S1031-07	92.75	93.75	0.84	1.41	2.24	6750	6795	454
S1031-07	93.75	94.75	0.89	0.84	1.72	6750	6795	453
S1031-07	94.75	95.75	0.93	0.31	1.24	6750	6795	452
S1032-07	20.80	21.80	0.11	2.09	2.20	6546	6901	519
S1032-07	21.80	22.80	0.41	1.25	1.66	6546	6901	518
S1032-07	22.80	23.80	2.03	2.45	4.48	6546	6901	517
S1032-07	23.80	24.80	0.48	1.01	1.49	6546	6901	516
S1032-07	24.80	25.80	0.90	1.21	2.11	6546	6901	515
S1032-07	25.80	26.80	1.67	3.71	5.39	6546	6901	514
S1032-07	26.80	27.80	0.36	1.18	1.54	6547	6901	513
S1032-07	27.80	28.80	0.00	0.44	0.44	6547	6901	512
S1032-07	28.80	29.80	0.00	0.43	0.43	6547	6901	511
S1032-07	29.80	30.80	0.00	0.64	0.64	6547	6901	510
S1032-07	30.80	31.80	0.05	0.49	0.54	6547	6901	509
S1032-07	31.80	32.80	0.08	0.19	0.27	6547	6901	508
S1032-07	32.80	33.80	0.02	0.27	0.29	6547	6901	507
S1032-07	33.80	34.80	0.39	3.02	3.41	6547	6901	506
S1032-07	34.80	35.80	0.74	1.72	2.46	6547	6901	505
S1032-07	35.80	36.80	0.16	3.77	3.93	6547	6901	504
S1032-07	36.80	37.80	0.00	1.89	1.89	6547	6901	503
S1032-07	37.80	38.80	0.00	1.08	1.08	6547	6901	502
S1032-07	38.80	39.80	0.00	1.26	1.26	6547	6901	501
S1033-07	26.00	27.00	0.01	1.24	1.25	6654	6851	518
S1033-07	27.00	28.00	0.03	2.12	2.15	6654	6851	517
S1033-07	28.00	29.00	0.06	1.18	1.24	6654	6851	516
S1033-07	29.00	30.00	1.94	4.00	5.94	6654	6851	515
S1033-07	30.00	31.00	0.74	1.55	2.29	6654	6851	514
S1033-07	31.00	32.00	2.60	1.65	4.25	6654	6851	513
S1033-07	32.00	33.00	0.72	1.09	1.81	6654	6851	512
S1033-07	33.00	34.00	0.26	1.40	1.66	6654	6851	511
S1033-07	34.00	35.00	2.60	2.21	4.81	6654	6851	510
S1033-07	35.00	36.00	5.50	2.60	8.10	6654	6851	509
S1033-07	36.00	37.00	0.42	0.93	1.35	6654	6851	508

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1033-07	37.00	38.00	0.10	0.16	0.26	6654	6851	507
S1033-07	38.00	39.00	0.20	0.22	0.41	6654	6851	506
S1033-07	39.00	40.00	1.09	0.83	1.92	6654	6851	505
S1033-07	40.00	41.00	0.25	0.34	0.59	6654	6851	504
S1033-07	41.00	42.00	0.77	1.33	2.10	6654	6851	503
S1033-07	42.00	43.00	0.41	0.29	0.70	6654	6851	502
S1033-07	43.00	44.00	1.77	2.07	3.84	6654	6851	501
S1033-07	44.00	45.00	1.62	2.39	4.01	6654	6851	500
S1033-07	45.00	46.00	3.00	1.25	4.25	6654	6851	499
S1033-07	46.00	47.00	1.27	0.42	1.69	6654	6851	498
S1033-07	47.00	48.00	1.98	1.44	3.42	6654	6851	497
S1033-07	48.00	49.00	1.19	0.93	2.12	6654	6850	496
S1033-07	49.00	50.00	1.19	0.93	2.12	6654	6850	495
S1033-07	50.00	51.00	1.19	0.93	2.12	6654	6850	494
S1033-07	51.00	52.00	0.61	1.29	1.90	6654	6850	493
S1033-07	52.00	53.00	0.14	1.01	1.15	6654	6850	492
S1033-07	53.00	54.00	0.16	0.81	0.97	6654	6850	491
S1033-07	54.00	55.00	1.60	1.76	3.36	6654	6850	490
S1033-07	55.00	56.00	3.40	2.90	6.30	6654	6850	489
S1033-07	56.00	57.00	1.10	1.40	2.50	6654	6850	488
S1033-07	57.00	58.00	0.26	0.75	1.01	6654	6850	487
S1033-07	58.00	59.00	0.13	1.58	1.71	6654	6850	486
S1034-07	114.40	115.40	6.88	1.45	8.33	6775	6838	430
S1034-07	115.40	116.40	8.20	2.70	10.90	6775	6838	429
S1034-07	116.40	117.40	8.20	2.70	10.90	6775	6838	428
S1034-07	117.40	118.40	6.44	2.36	8.80	6775	6838	427
S1034-07	118.40	119.40	3.80	1.86	5.66	6775	6838	426
S1035-07	101.00	102.00	2.50	6.60	9.10	6721	6897	441
S1035-07	102.00	103.00	2.80	5.90	8.70	6721	6897	440
S1035-07	103.00	104.00	0.14	0.74	0.88	6721	6897	439
S1037-07	94.00	95.00	0.10	1.37	1.47	6751	6930	445
S1037-07	95.00	96.00	0.01	0.29	0.30	6751	6930	444
S1037-07	96.00	97.00	11.10	5.10	16.20	6751	6930	443
S1037-07	97.00	98.00	0.96	4.30	5.26	6751	6930	442
S1037-07	98.00	99.00	7.90	4.00	11.90	6751	6930	441
S1037-07	99.00	100.00	3.64	1.82	5.46	6751	6930	440
S1037-07	100.00	101.00	3.20	0.63	3.83	6751	6930	439
S1037-07	101.00	102.00	3.80	1.40	5.20	6751	6930	438
S1037-07	102.00	103.00	0.38	0.21	0.59	6751	6930	437
S1041-07	50.00	51.00	0.00	0.70	0.70	6671	6963	487
S1041-07	51.00	52.00	0.00	1.11	1.11	6671	6963	486
S1041-07	52.00	53.00	0.00	0.89	0.89	6671	6963	485
S1042-07	53.00	54.00	0.27	3.00	3.27	6673	7032	476
S1042-07	55.00	56.00	0.99	3.60	4.59	6673	7032	474
S1042-07	56.00	57.00	3.30	1.38	4.68	6673	7032	473
S1043-07	62.50	63.50	5.00	8.25	13.25	6744	6997	469

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1043-07	63.50	64.50	6.10	8.35	14.45	6744	6997	468
S1043-07	64.50	65.50	4.63	5.66	10.28	6744	6997	467
S1043-07	65.50	66.50	1.03	2.18	3.21	6744	6997	466
S1044-07	39.00	40.00	0.03	1.06	1.09	6965	6534	515
S1044-07	40.00	41.00	0.50	1.40	1.90	6965	6534	514
S1044-07	41.00	42.00	0.94	1.56	2.50	6965	6534	513
S1044-07	42.00	43.00	0.90	1.41	2.31	6965	6534	512
S1044-07	43.00	44.00	0.05	1.12	1.17	6965	6534	511
S1044-07	44.00	45.00	0.17	0.93	1.10	6965	6534	510
S1044-07	45.00	46.00	1.24	2.03	3.27	6965	6534	509
S1044-07	46.00	47.00	1.71	2.17	3.88	6965	6533	508
S1044-07	47.00	48.00	1.58	0.87	2.45	6965	6533	507
S1044-07	48.00	49.00	1.26	0.38	1.64	6965	6533	506
S1044-07	49.00	50.00	0.47	0.51	0.98	6965	6533	505
S1044-07	50.00	51.00	0.12	0.14	0.26	6965	6533	504
S1044-07	51.00	52.00	0.33	0.27	0.60	6965	6533	503
S1044-07	52.00	53.00	0.12	0.19	0.31	6965	6533	502
S1044-07	53.00	54.00	0.08	0.06	0.14	6965	6533	501
S1044-07	54.00	55.00	0.20	0.18	0.38	6965	6533	500
S1044-07	55.00	56.00	0.16	0.13	0.28	6965	6533	499
S1044-07	56.00	57.00	0.75	0.33	1.08	6965	6533	498
S1044-07	57.00	58.00	1.09	0.58	1.67	6965	6533	497
S1044-07	58.00	59.00	0.42	0.07	0.49	6965	6533	496
S1044-07	59.00	60.00	0.85	0.16	1.01	6965	6533	495
S1044-07	60.00	61.00	1.06	0.65	1.71	6965	6533	494
S1044-07	61.00	62.00	1.44	0.50	1.94	6965	6533	493
S1044-07	62.00	63.00	1.70	1.00	2.70	6965	6533	492
S1044-07	63.00	64.00	1.38	0.61	1.99	6965	6533	491
S1044-07	64.00	65.00	0.48	0.35	0.83	6965	6533	490
S1044-07	65.00	66.00	0.11	0.07	0.19	6965	6533	489
S1044-07	66.00	67.00	0.37	0.17	0.54	6965	6533	488
S1044-07	67.00	68.00	1.05	0.23	1.28	6965	6533	487
S1045-07	71.00	72.00	0.38	2.31	2.69	6994	6572	478
S1045-07	72.00	73.00	0.38	2.31	2.69	6994	6572	477
S1045-07	73.00	74.00	0.02	0.31	0.33	6994	6572	476
S1045-07	74.00	75.00	0.08	0.20	0.29	6994	6572	475
S1045-07	75.00	76.00	0.08	1.42	1.50	6994	6572	474
S1045-07	76.00	77.00	0.00	1.89	1.89	6994	6572	473
S1046-07	56.00	57.00	0.56	4.10	4.66	6729	7029	471
S1046-07	57.00	58.00	2.16	10.30	12.46	6729	7029	470
S1046-07	58.00	59.00	5.70	8.40	14.10	6729	7029	469
S1046-07	59.00	60.00	0.38	0.23	0.61	6729	7029	468
S1046-07	60.00	61.00	1.02	0.35	1.37	6729	7029	467
S1046-07	61.00	62.00	0.54	0.08	0.62	6729	7029	466
S1046-07	62.00	63.00	1.86	0.10	1.96	6729	7029	465
S1047-07	67.00	68.00	3.50	0.20	3.70	7034	6546	481

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1047-07	68.00	69.00	1.71	1.25	2.96	7034	6546	480
S1047-07	69.00	70.00	2.16	0.44	2.60	7034	6546	479
S1048-07	43.00	44.00	7.80	0.43	8.23	7071	6511	504
S1048-07	44.00	45.00	5.70	0.04	5.74	7071	6511	503
S1048-07	45.00	46.00	2.60	0.28	2.88	7071	6511	502
S1048-07	46.00	47.00	2.90	0.25	3.15	7071	6511	501
S1048-07	47.00	48.00	2.90	0.86	3.76	7071	6511	500
S1048-07	48.00	49.00	2.70	1.74	4.44	7071	6511	499
S1048-07	49.00	50.00	2.49	1.21	3.70	7071	6511	498
S1048-07	50.00	51.00	2.49	1.21	3.70	7071	6511	497
S1048-07	51.00	52.00	2.49	1.21	3.70	7071	6511	496
S1048-07	52.00	53.00	2.49	1.21	3.70	7071	6511	495
S1048-07	53.00	54.00	2.49	1.21	3.70	7071	6511	494
S1048-07	54.00	55.00	2.49	1.21	3.70	7071	6511	493
S1049-07	49.50	50.50	3.16	3.51	6.67	6699	6998	482
S1049-07	50.50	51.50	0.63	6.75	7.38	6699	6998	481
S1049-07	51.50	52.50	0.58	6.85	7.43	6699	6998	480
S1049-07	52.50	53.50	0.54	3.89	4.43	6699	6998	479
S1049-07	53.50	54.50	0.87	2.02	2.88	6699	6998	478
S1050-07	74.00	75.00	1.19	2.70	3.89	7036	6591	471
S1050-07	75.00	76.00	0.62	1.57	2.19	7036	6591	470
S1050-07	76.00	77.00	2.40	2.60	5.00	7036	6591	469
S1050-07	77.00	78.00	5.60	1.85	7.45	7036	6591	468
S1050-07	78.00	79.00	1.17	1.07	2.24	7036	6591	467
S1050-07	79.00	80.00	4.60	3.20	7.80	7036	6591	466
S1050-07	80.00	81.00	7.80	4.30	12.10	7036	6591	465
S1050-07	81.00	82.00	1.04	1.72	2.76	7036	6591	464
S1050-07	82.00	83.00	2.44	1.98	4.42	7036	6591	463
S1050-07	83.00	84.00	0.99	1.99	2.98	7036	6591	462
S1050-07	84.00	85.00	0.06	1.30	1.36	7036	6591	461
S1051-07	31.20	32.20	0.75	0.75	1.50	6731	6719	518
S1051-07	32.20	33.20	0.01	0.62	0.63	6731	6719	517
S1051-07	33.20	34.20	0.01	0.90	0.91	6731	6719	516
S1051-07	34.20	35.20	0.00	1.23	1.24	6731	6719	515
S1051-07	35.20	36.20	0.01	0.71	0.72	6731	6719	514
S1051-07	36.20	37.20	0.01	0.80	0.81	6731	6719	513
S1051-07	37.20	38.20	0.01	1.36	1.37	6731	6719	512
S1051-07	38.20	39.20	0.02	1.13	1.15	6731	6719	511
S1051-07	39.20	40.20	0.04	1.27	1.31	6731	6719	510
S1051-07	40.20	41.20	0.03	0.53	0.56	6731	6719	509
S1051-07	41.20	42.20	0.03	0.15	0.18	6731	6719	508
S1051-07	42.20	43.20	0.04	0.14	0.19	6731	6719	507
S1051-07	43.20	44.20	0.10	0.10	0.19	6731	6719	506
S1051-07	44.20	45.20	0.17	0.29	0.47	6731	6719	505
S1051-07	45.20	46.20	0.07	0.18	0.25	6731	6719	504
S1051-07	46.20	47.20	0.08	0.20	0.29	6731	6719	503

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1051-07	47.20	48.20	0.08	0.26	0.34	6731	6719	502
S1051-07	48.20	49.20	0.01	0.17	0.18	6731	6719	501
S1051-07	49.20	50.20	0.01	0.46	0.47	6731	6719	500
S1051-07	50.20	51.20	0.01	0.69	0.70	6731	6719	499
S1051-07	51.20	52.20	0.02	0.56	0.57	6731	6719	498
S1051-07	52.20	53.20	0.00	0.81	0.81	6731	6719	497
S1051-07	53.20	54.20	0.00	1.38	1.38	6731	6719	496
S1051-07	54.20	55.20	0.00	1.26	1.26	6731	6719	495
S1052-07	57.00	58.00	0.16	0.96	1.12	6864	6441	495
S1052-07	58.00	59.00	0.20	0.65	0.85	6864	6441	494
S1052-07	59.00	60.00	0.83	0.69	1.52	6864	6441	493
S1052-07	60.00	61.00	1.45	1.25	2.70	6864	6441	492
S1052-07	61.00	62.00	0.90	0.61	1.51	6864	6441	491
S1052-07	62.00	63.00	2.18	0.69	2.87	6864	6441	490
S1052-07	63.00	64.00	1.97	0.61	2.58	6864	6441	489
S1053-07	52.60	53.60	1.76	1.98	3.74	6857	6525	504
S1053-07	53.60	54.60	3.28	1.78	5.07	6857	6525	503
S1053-07	54.60	55.60	3.82	2.40	6.22	6856	6525	502
S1053-07	55.60	56.60	1.69	2.09	3.78	6856	6525	501
S1053-07	56.60	57.60	0.33	1.02	1.34	6856	6525	500
S1053-07	57.60	58.60	0.49	1.61	2.10	6856	6525	499
S1053-07	58.60	59.60	0.48	1.93	2.41	6856	6525	498
S1053-07	59.60	60.60	0.21	2.37	2.58	6856	6525	497
S1053-07	60.60	61.60	0.12	1.71	1.83	6856	6525	496
S1053-07	61.60	62.60	0.34	2.55	2.89	6856	6525	495
S1053-07	62.60	63.60	0.59	2.15	2.74	6856	6525	494
S1053-07	63.60	64.60	0.53	1.01	1.54	6856	6525	493
S1053-07	64.60	65.60	0.26	0.55	0.81	6856	6525	492
S1053-07	65.60	66.60	0.35	0.74	1.10	6856	6525	491
S1053-07	66.60	67.60	0.21	0.66	0.87	6856	6525	490
S1053-07	67.60	68.60	0.36	0.69	1.05	6856	6525	489
S1053-07	68.60	69.60	0.41	0.94	1.35	6856	6525	488
S1054-07	95.00	96.00	0.87	2.28	3.15	6914	6434	458
S1054-07	96.00	97.00	0.16	0.53	0.69	6914	6434	457
S1054-07	97.00	98.00	0.43	0.16	0.59	6914	6434	456
S1054-07	98.00	99.00	0.10	0.60	0.70	6914	6434	455
S1054-07	99.00	100.00	0.57	0.85	1.42	6914	6434	454
S1054-07	100.00	101.00	1.64	0.91	2.55	6914	6434	453
S1054-07	101.00	102.00	3.50	0.74	4.24	6914	6434	452
S1054-07	102.00	103.00	0.33	0.74	1.07	6914	6434	451
S1054-07	103.00	104.00	0.33	1.39	1.72	6914	6434	450
S1054-07	104.00	105.00	0.37	1.26	1.63	6914	6434	449
S1057-08	93.15	94.15	1.28	1.94	3.22	6976	6618	453
S1057-08	94.15	95.15	4.92	2.23	7.15	6976	6618	452
S1057-08	95.15	96.15	6.50	2.94	9.44	6976	6618	451
S1057-08	96.15	97.15	6.37	2.50	8.88	6976	6618	450

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1058-08	92.50	93.50	0.51	1.14	1.65	6926	6667	452
S1058-08	93.50	94.50	0.45	0.90	1.35	6926	6667	451
S1058-08	94.50	95.50	0.30	0.38	0.68	6926	6667	450
S1059-08	38.50	39.50	0.98	2.53	3.51	6998	6512	514
S1059-08	39.50	40.50	0.91	2.07	2.98	6998	6512	513
S1059-08	40.50	41.50	1.59	2.07	3.66	6998	6512	512
S1059-08	41.50	42.50	2.07	1.81	3.88	6998	6512	511
S1059-08	42.50	43.50	2.17	1.91	4.08	6998	6512	510
S1059-08	43.50	44.50	2.35	2.95	5.30	6998	6512	509
S1059-08	44.50	45.50	2.50	3.00	5.50	6998	6512	508
S1059-08	45.50	46.50	2.87	3.05	5.92	6998	6512	507
S1059-08	46.50	47.50	2.37	3.30	5.67	6998	6512	506
S1059-08	47.50	48.50	2.60	2.41	5.01	6998	6512	505
S1059-08	48.50	49.50	2.19	0.87	3.06	6998	6512	504
S1059-08	49.50	50.50	1.28	1.42	2.70	6998	6512	503
S1059-08	50.50	51.50	0.82	2.11	2.93	6998	6512	502
S1059-08	51.50	52.50	0.73	1.24	1.97	6998	6512	501
S1059-08	52.50	53.50	1.30	0.94	2.24	6998	6512	500
S1059-08	53.50	54.50	1.84	1.58	3.42	6998	6512	499
S1059-08	54.50	55.50	1.38	1.20	2.58	6998	6512	498
S1059-08	55.50	56.50	0.55	0.50	1.05	6998	6512	497
S1059-08	56.50	57.50	0.31	0.41	0.71	6998	6512	496
S1059-08	57.50	58.50	0.54	0.70	1.24	6998	6512	495
S1059-08	58.50	59.50	0.48	0.67	1.14	6998	6512	494
S1059-08	59.50	60.50	0.74	0.56	1.29	6998	6512	493
S1063-08	97.05	98.05	0.00	0.01	0.01	6795	6803	449
S1065-08	27.00	28.00	0.27	1.00	1.27	6853	6229	510
S1065-08	28.00	29.00	0.32	0.04	0.36	6853	6229	509
S1065-08	29.00	30.00	1.26	0.26	1.52	6853	6229	508
S1065-08	30.00	31.00	1.94	0.89	2.83	6853	6229	507
S1065-08	31.00	32.00	6.50	1.61	8.11	6853	6229	506
S1065-08	32.00	33.00	0.53	0.58	1.11	6853	6229	505
S1066-08	31.00	32.00	0.40	0.82	1.22	6884	6318	509
S1066-08	32.00	33.00	0.30	0.77	1.07	6884	6318	508
S1066-08	33.00	34.00	0.08	1.33	1.41	6884	6318	507
S1066-08	34.00	35.00	0.44	0.87	1.31	6884	6318	506
S1066-08	35.00	36.00	1.19	0.37	1.56	6884	6318	505
S1066-08	36.00	37.00	1.10	0.64	1.74	6884	6318	504
S1067-08	30.00	31.00	0.85	0.66	1.51	6884	6115	508
S1067-08	31.00	32.00	3.60	1.05	4.65	6884	6115	507
S1067-08	32.00	33.00	1.34	0.87	2.21	6884	6115	506
S1067-08	33.00	34.00	1.31	0.92	2.23	6884	6115	505
S1067-08	34.00	35.00	0.93	0.38	1.31	6884	6115	504
S1067-08	35.00	36.00	0.52	0.25	0.77	6884	6115	503
S1067-08	36.00	37.00	2.00	0.59	2.59	6884	6115	502
S1067-08	37.00	38.00	3.30	0.91	4.21	6884	6115	501

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1067-08	38.00	39.00	1.78	0.66	2.44	6884	6115	500
S1068-08	103.50	104.50	2.37	1.82	4.19	6917	6722	440
S1068-08	104.50	105.50	5.19	2.31	7.50	6917	6722	439
S1068-08	105.50	106.50	4.27	1.54	5.81	6917	6722	438
S1069-08	63.00	64.00	0.04	0.08	0.11	6907	6055	469
S1069-08	64.00	65.00	0.21	1.01	1.22	6907	6055	468
S1069-08	65.00	66.00	0.53	3.00	3.53	6907	6055	467
S1070-08	78.00	79.00	0.44	2.18	2.62	6910	6370	470
S1070-08	79.00	80.00	0.23	1.42	1.65	6910	6370	469
S1070-08	80.00	81.00	0.01	0.01	0.02	6910	6370	468
S1070-08	81.00	82.00	1.45	0.48	1.93	6910	6370	467
S1070-08	82.00	83.00	0.84	0.34	1.18	6910	6370	466
S1070-08	83.00	84.00	1.44	0.11	1.55	6910	6370	465
S1071-08	64.00	65.00	0.50	1.69	2.19	6826	6747	485
S1071-08	65.00	66.00	0.94	2.48	3.42	6826	6747	484
S1071-08	66.00	67.00	1.92	2.70	4.62	6826	6747	483
S1071-08	67.00	68.00	0.75	0.68	1.43	6826	6747	482
S1071-08	68.00	69.00	0.59	1.26	1.85	6826	6747	481
S1071-08	69.00	70.00	0.32	2.22	2.54	6826	6747	480
S1071-08	70.00	71.00	0.99	2.04	3.03	6826	6747	479
S1071-08	71.00	72.00	0.33	1.64	1.97	6826	6747	478
S1071-08	72.00	73.00	0.02	1.56	1.58	6826	6747	477
S1072-08	83.00	84.00	0.45	1.91	2.36	6852	6788	463
S1072-08	84.00	85.00	0.45	1.91	2.36	6852	6788	463
S1072-08	85.00	86.00	0.45	1.91	2.36	6852	6788	462
S1072-08	86.00	87.00	10.62	7.62	18.25	6852	6788	461
S1072-08	87.00	88.00	12.20	10.20	22.40	6852	6788	460
S1072-08	88.00	89.00	11.90	7.70	19.60	6852	6788	459
S1077-08	47.00	48.00	0.63	2.25	2.88	6812	6038	479
S1077-08	48.00	49.00	0.25	0.77	1.03	6812	6038	478
S1077-08	49.00	50.00	0.48	1.88	2.36	6812	6038	477
S1077-08	50.00	51.00	0.56	0.63	1.19	6812	6038	476
S1077-08	51.00	52.00	0.05	0.09	0.14	6812	6038	475
S1077-08	52.00	53.00	0.01	0.10	0.11	6812	6038	474
S1077-08	53.00	54.00	0.49	1.83	2.32	6812	6038	473
S1079-08	71.30	72.30	1.84	1.04	2.89	6549	7040	457
S1079-08	72.30	73.30	2.63	0.61	3.24	6549	7040	456
S1079-08	73.30	74.30	0.23	0.03	0.26	6549	7040	455
S1082-08	72.45	73.45	2.60	5.59	8.19	6560	6999	459
S1086-08	51.60	52.60	3.39	1.75	5.14	6483	6912	486
S1086-08	52.60	53.60	0.24	1.08	1.32	6483	6912	485
S1086-08	53.60	54.60	0.10	1.63	1.73	6483	6912	484
S1086-08	54.60	55.60	0.06	1.78	1.84	6483	6912	483
S1086-08	55.60	56.60	0.10	1.48	1.58	6483	6912	482
S1086-08	56.60	57.60	0.06	1.98	2.04	6483	6912	481
S1086-08	57.60	58.60	0.29	4.97	5.26	6483	6912	480

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1086-08	58.60	59.60	0.27	5.74	6.01	6483	6912	479
S1093-08	72.50	73.50	1.42	0.37	1.79	6764	7079	442
S1093-08	73.50	74.50	5.24	0.24	5.48	6764	7079	441
S1093-08	74.50	75.50	5.51	0.16	5.67	6764	7079	440
S1100-08	25.00	26.00	0.41	0.62	1.03	6473	6865	514
S1100-08	26.00	27.00	0.20	0.79	0.99	6473	6865	513
S1100-08	27.00	28.00	0.74	0.60	1.34	6473	6865	512
S1100-08	28.00	29.00	0.13	0.43	0.56	6473	6865	511
S1100-08	29.00	30.00	0.92	0.79	1.71	6473	6865	510
S1100-08	30.00	31.00	0.43	1.39	1.82	6473	6865	509
S1100-08	31.00	32.00	0.15	1.27	1.42	6473	6865	508
S1100-08	32.00	33.00	0.20	0.97	1.17	6473	6865	507
S1100-08	33.00	34.00	0.19	1.77	1.96	6473	6865	506
S1100-08	34.00	35.00	0.09	1.05	1.14	6473	6865	505
S1104-08	93.00	94.00	0.46	0.74	1.20	6441	6965	438
S1104-08	94.00	95.00	0.75	1.37	2.12	6441	6965	437
S1104-08	95.00	96.00	1.56	4.50	6.06	6441	6965	436
S1108-08	19.00	20.00	0.42	1.31	1.73	6423	6869	520
S1108-08	20.00	21.00	0.22	3.00	3.22	6423	6869	519
S1108-08	21.00	22.00	0.04	0.56	0.60	6423	6869	518
S1108-08	22.00	23.00	0.04	0.52	0.56	6423	6869	517
S1108-08	23.00	24.00	0.04	0.64	0.68	6423	6869	516
S1108-08	24.00	25.00	0.02	1.08	1.10	6423	6869	515
S1108-08	25.00	26.00	0.01	1.57	1.58	6423	6869	514
S1108-08	26.00	27.00	0.09	1.79	1.88	6423	6869	513
S1108-08	27.00	28.00	0.19	1.28	1.47	6423	6869	512
S1108-08	28.00	29.00	0.65	2.29	2.94	6423	6869	511
S1108-08	29.00	30.00	0.07	2.80	2.87	6423	6869	510
S1108-08	30.00	31.00	0.09	3.90	3.99	6423	6869	509
S1108-08	31.00	32.00	0.60	1.45	2.05	6423	6869	508
S1108-08	32.00	33.00	0.55	2.04	2.59	6423	6869	507
S1108-08	33.00	34.00	0.65	3.90	4.55	6423	6869	506
S1108-08	34.00	35.00	0.29	4.00	4.29	6423	6869	505
S1108-08	35.00	36.00	0.16	1.74	1.90	6423	6869	504
S1108-08	36.00	37.00	0.06	1.86	1.92	6423	6869	503
S1108-08	37.00	38.00	0.05	2.38	2.43	6423	6869	502
S1108-08	38.00	39.00	0.27	2.01	2.28	6423	6869	501
S1108-08	39.00	40.00	0.12	2.30	2.42	6423	6869	500
S1108-08	40.00	41.00	0.03	1.80	1.83	6423	6869	499
S1108-08	41.00	42.00	0.09	0.43	0.52	6423	6869	498
S1108-08	42.00	43.00	0.04	1.09	1.13	6423	6869	497
S1110-08	17.00	18.00	0.01	1.05	1.06	6370	6864	520
S1110-08	18.00	19.00	0.04	0.70	0.74	6370	6864	519
S1110-08	19.00	20.00	0.01	2.11	2.12	6370	6864	518
S1110-08	20.00	21.00	0.01	1.17	1.18	6370	6864	517
S1110-08	21.00	22.00	0.10	0.97	1.07	6370	6864	516

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1110-08	22.00	23.00	0.04	0.80	0.84	6370	6864	515
S1110-08	23.00	24.00	0.04	0.81	0.85	6370	6864	514
S1110-08	24.00	25.00	0.14	1.64	1.78	6370	6864	513
S1110-08	25.00	26.00	0.76	2.50	3.26	6370	6864	512
S1110-08	26.00	27.00	0.36	1.50	1.86	6370	6864	511
S1110-08	27.00	28.00	0.12	0.66	0.78	6370	6864	510
S1110-08	28.00	29.00	0.12	0.81	0.93	6370	6864	509
S1110-08	29.00	30.00	0.07	0.40	0.47	6370	6864	508
S1110-08	30.00	31.00	0.22	0.01	0.23	6370	6864	507
S1110-08	31.00	32.00	0.17	0.43	0.60	6370	6864	506
S1110-08	32.00	33.00	0.41	0.19	0.60	6370	6864	505
S1110-08	33.00	34.00	0.36	0.60	0.96	6370	6864	504
S1110-08	34.00	35.00	1.35	0.23	1.58	6370	6864	503
S1111-08	43.00	44.00	1.44	1.99	3.43	6390	6916	490
S1111-08	45.00	46.00	0.12	0.78	0.90	6390	6916	488
S1111-08	46.00	47.00	0.20	3.70	3.90	6390	6916	487
S1111-08	47.00	48.00	0.22	1.37	1.59	6390	6916	486
S1111-08	48.00	49.00	0.09	0.77	0.86	6390	6916	485
S1111-08	49.00	50.00	0.05	0.72	0.77	6390	6916	484
S1111-08	50.00	51.00	0.03	1.24	1.27	6390	6916	483
S1111-08	51.00	52.00	0.10	4.40	4.50	6390	6916	482
S1111-08	52.00	53.00	0.02	3.40	3.42	6390	6916	481
S1111-08	53.00	54.00	0.09	3.50	3.59	6390	6916	480
S1111-08	54.00	55.00	0.01	1.40	1.41	6390	6916	479
S1111-08	55.00	56.00	0.22	1.58	1.80	6390	6916	478
S1111-08	56.00	57.00	0.01	2.24	2.25	6390	6916	477
S1111-08	57.00	58.00	0.02	0.77	0.79	6390	6916	476
S1111-08	58.00	59.00	0.01	0.27	0.28	6390	6916	475
S1111-08	59.00	60.00	0.01	1.30	1.31	6390	6916	474
S1124-08	40.40	41.40	0.73	2.54	3.26	6896	6538	517
S1124-08	41.40	42.40	1.17	2.85	4.03	6896	6538	516
S1124-08	42.40	43.40	1.80	4.42	6.22	6896	6538	515
S1124-08	43.40	44.40	1.53	2.09	3.61	6896	6538	514
S1124-08	44.40	45.40	1.51	1.74	3.26	6896	6538	513
S1124-08	45.40	46.40	1.07	1.33	2.40	6896	6538	512
S1124-08	46.40	47.40	0.07	0.37	0.45	6896	6538	511
S1124-08	47.40	48.40	0.35	0.93	1.27	6896	6538	510
S1124-08	48.40	49.40	0.68	1.67	2.35	6896	6538	509
S1124-08	49.40	50.40	0.68	1.30	1.98	6896	6538	508
S1124-08	50.40	51.40	0.68	1.53	2.22	6896	6538	507
S1124-08	51.40	52.40	0.88	1.61	2.49	6896	6538	506
S1124-08	52.40	53.40	0.87	1.46	2.33	6896	6538	505
S1124-08	53.40	54.40	0.69	1.53	2.22	6896	6538	504
S1124-08	54.40	55.40	0.97	1.28	2.25	6896	6538	503
S1124-08	55.40	56.40	0.97	0.89	1.86	6896	6538	502
S1124-08	56.40	57.40	0.82	0.86	1.68	6896	6538	501

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1124-08	57.40	58.40	0.97	0.70	1.66	6896	6538	500
S1124-08	58.40	59.40	2.43	0.80	3.23	6896	6538	499
S1124-08	59.40	60.40	3.50	0.78	4.28	6896	6538	498
S1124-08	60.40	61.40	1.85	0.46	2.31	6896	6538	497
S1125-08	39.60	40.60	0.54	0.81	1.35	6987	6470	514
S1125-08	40.60	41.60	0.50	0.75	1.25	6987	6470	513
S1125-08	41.60	42.60	1.04	1.35	2.39	6987	6470	512
S1125-08	42.60	43.60	1.21	1.84	3.05	6987	6470	511
S1125-08	43.60	44.60	0.54	1.23	1.76	6987	6470	510
S1125-08	44.60	45.60	0.94	1.18	2.12	6987	6470	509
S1125-08	45.60	46.60	1.09	1.19	2.29	6987	6470	508
S1125-08	46.60	47.60	0.59	1.23	1.82	6987	6470	507
S1125-08	47.60	48.60	0.32	0.81	1.13	6987	6470	506
S1125-08	48.60	49.60	0.76	1.19	1.95	6987	6470	505
S1125-08	49.60	50.60	1.58	1.94	3.52	6987	6470	504
S1125-08	50.60	51.60	1.20	1.81	3.01	6987	6470	503
S1125-08	51.60	52.60	0.59	0.90	1.48	6987	6470	502
S1125-08	52.60	53.60	0.38	0.50	0.88	6987	6470	501
S1125-08	53.60	54.60	0.29	0.69	0.98	6987	6470	500
S1125-08	54.60	55.60	1.40	1.01	2.41	6987	6470	499
S1125-08	55.60	56.60	1.23	0.78	2.01	6987	6470	498
S1125-08	56.60	57.60	0.64	0.51	1.16	6987	6470	497
S1125-08	57.60	58.60	0.52	0.47	0.99	6987	6470	496
S1125-08	58.60	59.60	0.40	0.34	0.74	6987	6470	495
S1125-08	59.60	60.60	0.24	0.32	0.56	6987	6470	494
S1125-08	60.60	61.60	0.09	0.67	0.76	6987	6470	493
S1125-08	61.60	62.60	0.04	0.65	0.68	6987	6470	492
S1125-08	62.60	63.60	0.17	1.17	1.34	6987	6470	491
S1125-08	63.60	64.60	0.20	0.74	0.94	6986	6470	490
S1125-08	64.60	65.60	0.20	0.13	0.33	6986	6470	489
S1125-08	65.60	66.60	0.27	0.26	0.53	6986	6470	488
S1125-08	66.60	67.60	0.21	0.26	0.47	6986	6470	487
S1125-08	67.60	68.60	1.07	0.82	1.89	6986	6470	486
S1125-08	68.60	69.60	1.71	0.97	2.67	6986	6470	485
S1125-08	69.60	70.60	0.88	0.60	1.48	6986	6470	484
S1125-08	70.60	71.60	0.27	0.57	0.83	6986	6470	483
S1125-08	71.60	72.60	0.22	0.74	0.96	6986	6470	482
S1125-08	72.60	73.60	0.16	0.65	0.80	6986	6470	481
S1125-08	73.60	74.60	0.59	1.21	1.80	6986	6470	480
S1125-08	74.60	75.60	0.89	1.34	2.23	6986	6470	479
S1125-08	75.60	76.60	0.60	0.78	1.38	6986	6470	478
S1125-08	76.60	77.60	0.03	0.03	0.06	6986	6470	477
S1125-08	77.60	78.60	0.36	0.34	0.70	6986	6470	476
S1125-08	78.60	79.60	0.90	0.45	1.35	6986	6470	475
S1126-08	25.00	26.00	2.41	1.04	3.45	6817	6151	509
S1126-08	26.00	27.00	1.75	0.94	2.69	6817	6151	508

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1126-08	27.00	28.00	0.46	0.10	0.56	6817	6151	507
S1126-08	28.00	29.00	0.85	0.11	0.96	6817	6151	506
S1126-08	29.00	30.00	1.08	0.31	1.39	6817	6151	505
S526	45.16	46.16	2.80	0.68	3.48	6521	6942	490
S526	46.16	47.16	0.85	0.20	1.06	6521	6942	489
S526	47.16	48.16	1.07	1.28	2.35	6521	6942	488
S526	48.16	49.16	0.89	2.66	3.55	6521	6942	487
S526	49.16	50.16	0.52	4.01	4.53	6521	6942	486
S526	50.16	51.16	0.48	4.15	4.64	6521	6942	485
S526	51.16	52.16	0.45	4.29	4.74	6521	6942	484
S526	52.16	53.16	0.69	2.49	3.18	6521	6942	483
S526	53.16	54.16	1.02	4.16	5.18	6521	6942	482
S526	54.16	55.16	1.59	5.44	7.03	6521	6942	481
S526	55.16	56.16	1.98	6.07	8.05	6521	6942	480
S526	56.16	57.16	2.05	5.63	7.68	6521	6942	479
S526	57.16	58.16	1.18	3.99	5.17	6521	6942	478
S526	58.16	59.16	0.31	2.35	2.66	6521	6942	477
S526	59.16	60.16	0.03	1.82	1.85	6521	6942	476
S527	20.17	21.17	0.09	3.53	3.62	6517	6882	521
S527	21.17	22.17	0.47	3.05	3.52	6517	6882	520
S527	22.17	23.17	0.16	1.62	1.78	6517	6882	519
S527	23.17	24.17	0.11	1.47	1.58	6517	6882	518
S527	24.17	25.17	0.11	2.80	2.91	6517	6882	517
S527	25.17	26.17	0.07	2.11	2.18	6517	6882	516
S527	26.17	27.17	0.02	1.03	1.05	6517	6882	515
S527	27.17	28.17	0.01	0.64	0.65	6517	6882	514
S527	28.17	29.17	0.14	0.54	0.68	6517	6882	513
S527	29.17	30.17	0.10	0.80	0.91	6517	6882	512
S527	30.17	31.17	0.04	1.23	1.28	6517	6882	511
S527	31.17	32.17	0.03	1.26	1.30	6517	6882	510
S527	32.17	33.17	0.06	0.62	0.68	6517	6882	509
S527	33.17	34.17	0.18	1.65	1.83	6517	6882	508
S527	34.17	35.17	0.19	1.67	1.86	6517	6882	507
S527	35.17	36.17	6.27	4.74	11.01	6517	6882	506
S527	36.17	37.17	0.56	3.79	4.35	6517	6882	505
S527	37.17	38.17	0.01	2.83	2.85	6517	6882	504
S527	38.17	39.17	0.00	1.89	1.89	6517	6882	503
S527	39.17	40.17	0.02	2.05	2.07	6517	6882	502
S527	40.17	41.17	0.02	1.79	1.81	6517	6882	501
S527	41.17	42.17	0.00	0.81	0.81	6517	6882	500
S527	42.17	43.17	0.00	0.66	0.66	6517	6882	499
S527	43.17	44.17	0.00	0.53	0.53	6517	6882	498
S527	44.17	45.17	0.00	2.53	2.53	6517	6882	497
S527	45.17	46.17	0.00	2.21	2.21	6517	6882	496
S527	46.17	47.17	0.00	1.59	1.59	6517	6882	495
S528	19.86	20.86	0.00	1.16	1.16	6517	6819	526

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S528	20.86	21.86	0.05	1.51	1.56	6517	6819	525
S528	21.86	22.86	0.07	0.49	0.56	6517	6819	524
						0	0	0
GGR093	40.13	41.13	0.16	0.99	1.15	6632	6338	507
GGR093	41.13	42.13	0.37	3.20	3.56	6632	6338	506
GGR093	42.13	43.13	1.06	2.57	3.63	6632	6338	505
GGR094	28.35	29.35	0.20	0.83	1.03	6622	6260	510
GGR094	29.35	30.35	0.17	0.93	1.10	6622	6260	509
GGR094	30.35	31.35	0.13	1.04	1.17	6622	6260	508
GGR094	31.35	32.35	0.04	0.67	0.71	6622	6260	507
GGR094	32.35	33.35	0.02	0.67	0.69	6622	6260	506
GGR094	33.35	34.35	0.01	0.61	0.62	6622	6260	505
GGR094	34.35	35.35	0.04	0.74	0.78	6622	6260	504
GGR094	35.35	36.35	0.19	3.09	3.28	6622	6260	503
GGR094	36.35	37.35	0.14	2.27	2.42	6622	6260	502
GGR094	37.35	38.35	0.06	0.76	0.82	6622	6260	501
GGR096	18.11	19.11	0.53	2.32	2.85	6631	6148	512
GGR096	19.11	20.11	0.23	1.08	1.31	6631	6148	511
GGR096	20.11	21.11	0.21	1.06	1.26	6631	6148	510
GGR096	21.11	22.11	0.11	2.58	2.69	6631	6148	509
GGR096	22.11	23.11	0.02	0.48	0.50	6631	6148	508
GGR096	23.11	24.11	0.07	0.40	0.47	6631	6148	507
GGR096	24.11	25.11	0.09	0.36	0.45	6631	6148	506
GGR096	25.11	26.11	0.04	0.76	0.80	6631	6148	505
GGR096	26.11	27.11	0.07	0.73	0.80	6631	6148	504
GGR096	27.11	28.11	0.14	0.57	0.71	6631	6148	503
GGR096	28.11	29.11	0.14	0.75	0.89	6631	6148	502
GGR096	29.11	30.11	0.15	0.76	0.91	6631	6148	501
GGR096	30.11	31.11	0.55	1.05	1.60	6631	6148	500
GGR096	31.11	32.11	0.72	1.49	2.21	6631	6148	499
GGR096	32.11	33.11	1.45	1.55	2.99	6631	6148	498
GGR096	33.11	34.11	2.59	2.37	4.96	6631	6148	497
GGR096	34.11	35.11	2.16	2.46	4.62	6631	6148	496
GGR096	35.11	36.11	6.21	4.31	10.51	6631	6148	495
GGR096	36.11	37.11	6.72	4.55	11.26	6631	6148	494
GGR096	37.11	38.11	3.66	3.10	6.76	6631	6148	493
GGR096	38.11	39.11	4.14	1.31	5.45	6631	6148	492
GGR096	39.11	40.11	3.42	1.15	4.57	6631	6148	491
GGR096	40.11	41.11	2.40	0.92	3.32	6631	6148	490
GGR096	41.11	42.11	0.27	0.28	0.55	6631	6148	489
GGR096	42.11	43.11	0.35	0.21	0.56	6631	6148	488
GGR096	43.11	44.11	0.50	0.15	0.65	6631	6148	487
GGR096	44.11	45.11	1.00	0.28	1.28	6631	6148	486
GGR096	45.11	46.11	1.05	0.29	1.34	6631	6148	485
GGR102	97.65	98.65	0.68	0.70	1.38	6541	6146	433
GGR102	98.65	99.65	2.81	3.43	6.24	6541	6146	432

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR102	99.65	100.65	0.16	0.15	0.31	6541	6146	431
GGR103	78.03	79.03	2.46	1.91	4.37	6512	6268	463
GGR103	79.03	80.03	0.60	0.73	1.33	6512	6268	462
GGR103	80.03	81.03	0.07	0.02	0.09	6512	6268	461
GGR163	75.59	76.59	0.03	0.16	0.19	6568	6201	454
GGR163	76.59	77.59	0.15	1.33	1.49	6568	6201	453
GGR163	77.59	78.59	0.24	1.94	2.17	6568	6201	452
GGR169	46.63	47.63	10.30	0.07	10.37	6575	6222	489
GGR169	47.63	48.63	6.78	0.07	6.85	6575	6222	488
GGR169	48.63	49.63	2.82	0.07	2.89	6575	6222	487
GGR169	49.63	50.63	2.37	0.19	2.57	6575	6222	486
GGR169	50.63	51.63	2.28	0.17	2.46	6575	6222	485
GGR169	51.63	52.63	2.19	0.14	2.33	6575	6222	484
GGR169	52.63	53.63	2.11	0.18	2.29	6575	6222	483
GGR169	53.63	54.63	2.20	0.15	2.35	6575	6222	482
GGR169	54.63	55.63	2.35	0.11	2.46	6575	6222	481
GGR169	55.63	56.63	5.82	1.86	7.68	6575	6222	480
GGR169	56.63	57.63	6.43	2.17	8.60	6575	6222	479
GGR169	59.63	60.63	0.27	1.69	1.96	6575	6222	476
GGR220	36.21	37.21	0.01	3.43	3.44	6567	6341	515
GGR220	37.21	38.21	0.03	1.41	1.45	6567	6341	514
GGR220	38.21	39.21	0.14	0.74	0.88	6567	6341	513
GGR220	39.21	40.21	0.54	1.20	1.74	6567	6341	512
GGR220	40.21	41.21	0.44	0.89	1.33	6567	6341	511
GGR220	41.21	42.21	0.43	0.83	1.26	6567	6341	510
GGR220	42.21	43.21	0.54	1.05	1.59	6567	6341	509
GGR220	43.21	44.21	0.33	0.87	1.20	6567	6341	508
GGR220	44.21	45.21	0.34	1.52	1.86	6567	6341	507
GGR220	45.21	46.21	0.81	2.38	3.19	6567	6341	506
GGR220	46.21	47.21	0.77	1.34	2.11	6567	6341	505
GGR220	47.21	48.21	0.31	0.68	0.99	6567	6341	504
GGR220	48.21	49.21	0.07	0.11	0.18	6567	6341	503
GGR220	49.21	50.21	0.09	0.68	0.77	6567	6341	502
GGR220	50.21	51.21	1.04	2.63	3.68	6567	6341	501
GGR220	51.21	52.21	0.49	2.96	3.45	6567	6341	500
GGR220	52.21	53.21	0.12	2.15	2.27	6567	6341	499
GGR220	53.21	54.21	0.05	1.47	1.53	6567	6341	498
GGR220	54.21	55.21	0.01	1.07	1.08	6567	6341	497
GGR220	55.21	56.21	0.08	0.91	0.99	6567	6341	496
GGR220	56.21	57.21	0.06	1.01	1.07	6567	6341	495
GGR220	57.21	58.21	0.03	2.23	2.26	6567	6341	494
GGR220	58.21	59.21	0.30	1.54	1.84	6567	6341	493
GGR220	59.21	60.21	0.13	1.54	1.66	6567	6341	492
GGR221	40.54	41.54	0.18	1.86	2.04	6573	6262	499
GGR221	41.54	42.54	0.18	1.87	2.04	6573	6262	498
GGR221	42.54	43.54	0.14	1.94	2.08	6573	6262	497

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR221	43.54	44.54	0.13	1.72	1.86	6573	6262	496
GGR226	54.47	55.47	0.65	1.54	2.19	6574	6462	507
GGR226	55.47	56.47	0.64	1.48	2.11	6574	6462	506
GGR226	56.47	57.47	0.51	1.16	1.67	6574	6462	505
GGR226	57.47	58.47	0.27	0.73	1.01	6574	6462	504
GGR226	58.47	59.47	0.08	0.24	0.32	6574	6462	503
GGR226	59.47	60.47	0.03	0.31	0.34	6574	6462	502
GGR226	60.47	61.47	0.06	1.23	1.29	6574	6462	501
GGR226	61.47	62.47	0.09	0.78	0.87	6574	6462	500
GGR226	62.47	63.47	0.12	1.52	1.65	6574	6462	499
GGR226	63.47	64.47	0.27	1.78	2.05	6574	6462	498
GGR226	64.47	65.47	0.29	0.49	0.78	6574	6462	497
GGR226	65.47	66.47	1.54	0.58	2.12	6574	6462	496
GGR227	55.11	56.11	0.12	0.92	1.04	6572	6404	506
GGR227	56.11	57.11	0.55	0.48	1.03	6572	6404	505
GGR227	57.11	58.11	0.61	0.73	1.33	6572	6404	504
GGR227	58.11	59.11	0.42	1.77	2.19	6572	6404	503
GGR227	59.11	60.11	0.30	2.33	2.63	6572	6404	502
GGR227	60.11	61.11	0.12	1.21	1.33	6572	6404	501
GGR227	61.11	62.11	0.18	0.93	1.11	6572	6404	500
GGR227	62.11	63.11	0.62	1.92	2.54	6572	6404	499
GGR227	63.11	64.11	0.66	3.82	4.47	6572	6404	498
GGR227	64.11	65.11	0.63	4.08	4.70	6572	6404	497
GGR227	65.11	66.11	0.44	1.89	2.33	6572	6404	496
GGR227	66.11	67.11	1.00	1.91	2.91	6572	6404	495
GGR227	67.11	68.11	1.22	1.92	3.14	6572	6404	494
GGR227	68.11	69.11	0.43	1.03	1.46	6572	6404	493
GGR227	69.11	70.11	0.06	0.43	0.48	6572	6404	492
GGR230	32.61	33.61	2.33	0.24	2.56	6601	6158	497
GGR230	33.61	34.61	2.47	0.10	2.57	6601	6158	496
GGR230	34.61	35.61	1.54	0.45	1.99	6601	6158	495
GGR230	35.61	36.61	0.81	0.31	1.12	6601	6158	494
GGR230	36.61	37.61	0.78	0.33	1.11	6601	6158	493
GGR230	37.61	38.61	0.90	0.74	1.64	6601	6158	492
GGR230	38.61	39.61	0.96	1.03	1.99	6601	6158	491
GGR230	39.61	40.61	0.34	0.60	0.94	6601	6158	490
GGR231	36.58	37.58	1.08	0.25	1.33	6563	6159	493
GGR231	38.58	39.58	0.40	0.04	0.44	6563	6159	491
GGR231	39.58	40.58	1.39	0.09	1.48	6563	6159	490
GGR231	40.58	41.58	1.50	0.10	1.60	6563	6159	489
GGR231	41.58	42.58	2.39	1.93	4.31	6563	6159	488
GGR231	42.58	43.58	1.11	0.89	2.00	6563	6159	487
GGR231	43.58	44.58	0.73	0.12	0.85	6563	6159	486
GGR231	44.58	45.58	1.39	0.24	1.63	6563	6159	485
GGR231	45.58	46.58	0.61	0.80	1.41	6563	6159	484
GGR231	46.58	47.58	0.25	0.07	0.32	6563	6159	483

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
GGR231	47.58	48.58	0.40	0.08	0.48	6563	6159	482
GGR231	48.58	49.58	0.41	0.09	0.50	6563	6159	481
GGR231	49.58	50.58	0.41	0.10	0.51	6563	6159	480
GGR231	50.58	51.58	0.55	0.96	1.50	6563	6159	479
GGR231	51.58	52.58	0.61	1.36	1.97	6563	6159	478
GGR231	52.58	53.58	0.26	1.05	1.31	6563	6159	477
GGR231	53.58	54.58	0.19	0.97	1.17	6563	6159	476
GGR231	54.58	55.58	0.43	2.07	2.50	6563	6159	475
GGR231	55.58	56.58	0.10	0.59	0.69	6563	6159	474
GGR231	56.58	57.58	0.05	0.24	0.29	6563	6159	473
GGR231	57.58	58.58	0.05	0.05	0.10	6563	6159	472
GGR231	58.58	59.58	0.09	0.31	0.40	6563	6159	471
GGR231	59.58	60.58	0.16	0.57	0.73	6563	6159	470
GGR231	60.58	61.58	0.26	0.81	1.08	6563	6159	469
GGR231	61.58	62.58	0.80	0.97	1.76	6563	6159	468
S1074-08	72.00	73.00	1.92	0.16	2.08	6608	6108	452
S1074-08	73.00	74.00	4.70	0.07	4.77	6608	6108	451
S1074-08	74.00	75.00	0.55	0.03	0.58	6608	6108	450
S1080-08	56.65	57.65	0.02	1.19	1.21	6585	6311	486
S1080-08	57.65	58.65	0.03	1.18	1.21	6585	6311	485
S1080-08	58.65	59.65	0.20	1.06	1.25	6585	6311	484
S1083-08	16.00	17.00	0.19	1.16	1.35	6616	6221	513
S1083-08	17.00	18.00	0.25	0.30	0.55	6616	6221	512
S1083-08	18.00	19.00	0.26	0.43	0.69	6616	6221	511
S1083-08	19.00	20.00	0.77	1.04	1.81	6616	6221	510
S1083-08	20.00	21.00	1.10	0.73	1.83	6616	6221	509
S1083-08	21.00	22.00	0.02	0.38	0.40	6616	6221	508
S1083-08	22.00	23.00	0.01	0.14	0.15	6616	6221	507
S1083-08	23.00	24.00	0.01	0.14	0.15	6616	6221	506
S1083-08	24.00	25.00	0.01	0.68	0.69	6616	6221	505
S1083-08	25.00	26.00	0.01	0.52	0.53	6616	6221	504
S1083-08	26.00	27.00	0.01	0.96	0.97	6616	6221	503
S1083-08	27.00	28.00	0.01	2.70	2.71	6616	6221	502
S1083-08	28.00	29.00	0.01	1.99	2.00	6616	6221	501
S1083-08	29.00	30.00	0.01	0.95	0.96	6616	6221	500
S1083-08	30.00	31.00	0.36	1.12	1.48	6616	6222	499
S1083-08	31.00	32.00	0.01	1.81	1.82	6616	6222	498
S1083-08	32.00	33.00	0.01	3.10	3.11	6616	6222	497
S1083-08	33.00	34.00	0.01	1.05	1.06	6616	6222	496
S1083-08	34.00	35.00	0.01	1.23	1.24	6616	6222	495
S1083-08	35.00	36.00	0.01	0.12	0.13	6616	6222	494
S1083-08	36.00	37.00	0.01	0.21	0.22	6616	6222	493
S1083-08	37.00	38.00	0.01	0.65	0.66	6616	6222	492
S1083-08	38.00	39.00	0.01	1.04	1.05	6616	6222	491
S1083-08	39.00	40.00	0.01	1.33	1.34	6616	6222	490
S1085-08	106.00	107.00	1.83	5.70	7.53	6524	6186	422

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1085-08	107.00	108.00	0.01	0.77	0.78	6524	6186	421
S1085-08	108.00	109.00	0.01	0.09	0.10	6524	6186	420
S1085-08	109.00	110.00	0.55	1.79	2.34	6524	6186	419
S1089-08	87.00	88.00	0.44	2.45	2.89	6537	6224	445
S1089-08	88.00	89.00	0.56	0.50	1.06	6537	6224	444
S1089-08	89.00	90.00	0.23	0.95	1.18	6537	6224	443
S1090-08	56.50	57.50	0.64	2.15	2.79	6537	6352	496
S1090-08	57.50	58.50	0.24	0.82	1.06	6537	6352	495
S1090-08	58.50	59.50	0.09	0.59	0.68	6537	6352	494
S1090-08	59.50	60.50	0.12	0.38	0.49	6537	6352	493
S1090-08	60.50	61.50	0.26	0.32	0.58	6537	6352	492
S1090-08	61.50	62.50	0.21	0.19	0.40	6537	6352	491
S1090-08	62.50	63.50	0.04	0.34	0.38	6537	6352	490
S1090-08	63.50	64.50	0.14	1.16	1.30	6537	6352	489
S1090-08	64.50	65.50	0.14	1.23	1.37	6537	6352	488
S1090-08	65.50	66.50	0.03	0.58	0.60	6537	6352	487
S1090-08	66.50	67.50	0.03	0.29	0.32	6537	6352	486
S1090-08	67.50	68.50	0.01	0.28	0.29	6537	6352	485
S1090-08	68.50	69.50	0.00	0.38	0.38	6537	6352	484
S1090-08	69.50	70.50	0.00	0.34	0.34	6537	6352	483
S1090-08	70.50	71.50	0.00	0.31	0.31	6537	6352	482
S1090-08	71.50	72.50	0.01	0.54	0.55	6537	6352	481
S1090-08	72.50	73.50	0.02	2.48	2.49	6537	6352	480
S1090-08	73.50	74.50	0.02	2.37	2.39	6537	6352	479
S1092-08	43.00	44.00	0.47	0.72	1.19	6605	6355	507
S1092-08	44.00	45.00	0.10	0.64	0.74	6605	6355	506
S1092-08	45.00	46.00	0.22	1.25	1.47	6605	6355	505
S1094-08	76.00	77.00	0.00	3.60	3.60	6522	6395	484
S1094-08	77.00	78.00	0.00	0.57	0.57	6522	6395	483
S1094-08	78.00	79.00	0.01	0.93	0.94	6522	6395	482
S1094-08	79.00	80.00	0.00	0.10	0.10	6522	6395	481
S1094-08	80.00	81.00	0.00	0.43	0.43	6522	6395	480
S1094-08	81.00	82.00	0.00	1.31	1.31	6522	6395	479
S1096-08	95.00	96.00	0.14	0.99	1.13	6478	6369	461
S1096-08	96.00	97.00	0.14	0.99	1.13	6478	6369	460
S1096-08	97.00	98.00	0.14	0.99	1.13	6478	6370	459
S1096-08	98.00	99.00	0.05	1.13	1.18	6478	6370	458
S1096-08	99.00	100.00	0.05	1.13	1.18	6478	6370	457
S1098-08	57.00	58.00	0.14	0.90	1.04	6539	6442	507
S1098-08	58.00	59.00	0.00	0.53	0.53	6539	6442	506
S1098-08	59.00	60.00	0.01	0.60	0.61	6539	6442	505
S1098-08	60.00	61.00	0.18	1.37	1.55	6539	6442	504
S1098-08	61.00	62.00	0.47	2.39	2.86	6539	6442	503
S1098-08	62.00	63.00	0.34	1.30	1.64	6539	6442	502
S1098-08	63.00	64.00	0.07	0.66	0.73	6539	6442	501
S1098-08	64.00	65.00	0.02	0.10	0.12	6539	6442	500

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1098-08	65.00	66.00	0.01	0.11	0.12	6539	6442	499
S1098-08	66.00	67.00	0.04	1.60	1.64	6539	6442	498
S1102-08	57.00	58.00	0.16	1.32	1.48	6552	6493	507
S1102-08	58.00	59.00	0.14	2.60	2.74	6552	6493	506
S1102-08	59.00	60.00	0.31	1.52	1.83	6552	6493	505
S1102-08	60.00	61.00	0.30	0.33	0.63	6552	6493	504
S1102-08	61.00	62.00	0.28	0.89	1.17	6552	6493	503
S1102-08	62.00	63.00	0.48	1.90	2.38	6552	6493	502
S1102-08	63.00	64.00	0.16	1.07	1.22	6552	6493	501
S1102-08	64.00	65.00	0.06	0.28	0.34	6552	6493	500
S1102-08	65.00	66.00	0.01	0.01	0.02	6552	6493	499
S1102-08	66.00	67.00	0.97	1.20	2.17	6552	6493	498
S1105-08	53.00	54.00	0.25	0.80	1.05	6558	6553	511
S1105-08	54.00	55.00	0.43	0.51	0.94	6558	6553	510
S1105-08	55.00	56.00	0.03	0.02	0.05	6558	6553	509
S1105-08	56.00	57.00	3.10	0.76	3.86	6558	6553	508
S1107-08	41.00	42.00	0.01	1.54	1.55	6518	6592	521
S1107-08	42.00	43.00	0.26	3.10	3.36	6518	6592	520
S1107-08	43.00	44.00	0.13	0.93	1.06	6518	6592	519
S1107-08	44.00	45.00	0.12	0.90	1.02	6518	6592	518
S1107-08	45.00	46.00	0.21	0.43	0.64	6518	6592	517
S1107-08	46.00	47.00	0.26	0.79	1.05	6518	6592	516
S1113-08	29.00	30.00	0.60	1.09	1.69	6657	6116	497
S1113-08	30.00	31.00	0.12	0.58	0.70	6657	6116	496
S1113-08	31.00	32.00	0.23	0.82	1.05	6657	6116	495
S1113-08	32.00	33.00	0.06	0.47	0.53	6657	6116	494
S1113-08	33.00	34.00	1.60	0.45	2.05	6657	6116	493
S1113-08	34.00	35.00	1.37	1.21	2.58	6657	6116	492
S1113-08	35.00	36.00	0.78	1.84	2.62	6657	6116	491
S1113-08	36.00	37.00	1.30	1.12	2.42	6657	6116	490
S1113-08	37.00	38.00	0.90	0.44	1.34	6657	6116	489
S1113-08	38.00	39.00	1.22	0.44	1.66	6657	6116	488
S1115-08	17.00	18.00	0.02	0.44	0.46	6663	6243	514
S1115-08	18.00	19.00	0.44	1.08	1.52	6663	6243	513
S1115-08	19.00	20.00	0.05	0.99	1.04	6663	6243	512
S1116-08	53.00	54.00	0.25	0.83	1.08	6571	6407	508
S1116-08	54.00	55.00	1.11	1.44	2.55	6571	6407	507
S1116-08	55.00	56.00	0.68	1.02	1.70	6571	6407	506
S1116-08	56.00	57.00	0.05	0.48	0.53	6571	6407	505
S1116-08	57.00	58.00	0.23	0.66	0.89	6571	6407	504
S1116-08	58.00	59.00	0.05	0.86	0.91	6571	6407	503
S1116-08	59.00	60.00	0.04	0.46	0.50	6571	6407	502
S1116-08	60.00	61.00	0.09	0.55	0.64	6571	6407	501
S1116-08	61.00	62.00	0.14	2.14	2.28	6571	6407	500
S1116-08	62.00	63.00	0.21	3.60	3.81	6571	6407	499
S1116-08	63.00	64.00	0.57	1.61	2.18	6571	6407	498

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S1118-08	97.70	98.70	0.91	2.06	2.97	6490	6252	441
S1118-08	98.70	99.70	0.21	1.44	1.65	6490	6252	440
S1118-08	99.70	100.70	0.03	0.09	0.12	6490	6252	439
S1122-08	55.00	56.00	0.32	1.36	1.68	6571	6219	475
S1122-08	56.00	57.00	0.52	1.19	1.71	6571	6219	474
S1122-08	57.00	58.00	0.08	0.35	0.43	6571	6219	473
						0	0	0
GGR018	59.65	60.65	3.00	8.42	11.42	6654	6984	475
GGR024	72.12	73.12	0.17	0.08	0.25	6766	7014	454
GGR025A	120.21	121.21	2.83	0.01	2.84	6768	6875	422
GGR027	45.15	46.15	0.67	0.82	1.49	6755	6636	509
GGR032	94.80	95.80	1.40	0.01	1.41	6776	7117	418
GGR036	47.94	48.94	0.71	0.59	1.30	6884	6634	502
GGR037	39.50	40.50	0.73	2.35	3.08	6997	6511	513
GGR037	61.50	62.50	0.33	0.06	0.39	6997	6511	491
GGR038	69.40	70.40	0.33	0.83	1.16	6889	6509	487
GGR039A	93.54	94.54	2.45	1.94	4.39	6987	6433	459
GGR039A	98.54	99.54	1.35	0.02	1.37	6987	6433	454
GGR040	79.55	80.55	0.57	0.44	1.01	6882	6762	466
GGR079	33.37	34.37	1.27	1.00	2.27	6878	6271	502
GGR116	79.53	80.53	0.84	0.29	1.13	7063	6455	464
GGR118	79.15	80.15	1.31	0.28	1.59	6942	6578	474
GGR125	64.20	65.20	1.47	0.53	2.00	6696	6938	475
GGR129	87.07	88.07	0.05	1.43	1.48	6702	6816	461
GGR130	52.46	53.46	1.88	0.64	2.51	6826	6576	505
GGR133	51.75	52.75	0.01	1.36	1.37	6694	6697	500
GGR146	49.11	50.11	1.16	0.02	1.18	6940	6098	483
GGR168	45.18	46.18	0.64	0.37	1.01	6906	6155	491
GGR171	29.40	30.40	1.50	0.78	2.28	6815	6275	508
GGR173	38.61	39.61	1.31	0.81	2.12	6907	6275	498
GGR177	69.55	70.55	0.22	1.52	1.74	6913	6484	486
GGR178	58.45	59.45	0.50	0.44	0.94	6943	6483	497
GGR179	59.75	60.75	0.41	0.51	0.92	6972	6482	495
GGR181	54.01	55.01	0.99	0.70	1.69	7032	6482	496
GGR182	49.98	50.98	7.16	5.96	13.12	6847	6483	504
GGR183	60.52	61.52	1.72	0.42	2.14	6897	6538	497
GGR184	47.78	48.78	0.93	0.70	1.63	6919	6556	508
GGR191	48.39	49.39	0.18	0.84	1.02	6776	6656	505
GGR193	63.10	64.10	0.42	0.86	1.28	6842	6719	484
GGR205	38.87	39.87	0.06	0.22	0.28	6610	6706	516
GGR206	65.12	66.12	0.10	1.00	1.10	6654	6779	483
GGR208	105.37	106.37	2.10	0.65	2.75	6719	6847	439
GGR209	115.79	116.79	1.22	0.31	1.53	6741	6869	428
GGR213	54.16	55.16	0.13	1.33	1.46	6675	6921	486
GGR214	67.72	68.72	0.27	0.95	1.22	6728	6972	468
GGR215	68.47	69.47	3.45	1.48	4.93	6750	6998	469

Hole Id	Depth From (m)	Depth To (m)	Pb Pct	Zn Pct	Pb + Zn Pct	Mid Y	Mid X	Mid Z
S0997-07	58.60	59.60	0.38	0.61	0.99	6931	6509	497
S1019-07	69.50	70.50	0.99	1.57	2.56	6717	6769	478
S1020-07	76.00	77.00	0.00	1.83	1.83	6686	6840	469
S1025-07	58.00	59.00	0.00	1.90	1.90	6651	6898	483
S1029-07	74.10	75.10	1.18	0.60	1.78	6696	6896	468
S1031-07	95.75	96.75	0.86	0.21	1.07	6750	6795	451
S1032-07	39.80	40.80	0.00	1.32	1.32	6547	6901	500
S1037-07	103.00	104.00	2.21	0.24	2.45	6751	6930	436
S1042-07	54.00	55.00	0.99	3.60	4.59	6673	7032	475
S1053-07	69.60	70.60	0.30	0.98	1.28	6856	6525	487
S1057-08	97.15	98.15	0.96	4.40	5.36	6976	6618	449
S1059-08	60.50	61.50	1.12	0.62	1.74	6998	6512	492
S1063-08	96.05	97.05	0.17	6.43	6.60	6795	6803	450
S1068-08	106.50	107.50	0.54	0.27	0.81	6917	6722	437
S1082-08	73.45	74.45	0.01	0.00	0.01	6560	6999	458
S1086-08	49.60	50.60	6.20	1.03	7.23	6483	6912	488
S1086-08	50.60	51.60	6.90	2.43	9.33	6483	6912	487
S1086-08	59.60	60.60	0.13	5.10	5.23	6483	6912	478
S1104-08	96.00	97.00	1.56	4.50	6.06	6441	6965	435
S1125-08	79.60	80.60	1.11	0.39	1.50	6986	6471	474
S526	60.16	61.16	0.02	1.81	1.83	6521	6942	475
GGR169	58.63	59.63	0.25	0.48	0.73	6575	6222	477
GGR169	60.63	61.63	0.30	3.10	3.40	6575	6222	475
GGR220	60.21	61.21	0.12	1.54	1.66	6567	6341	491
GGR221	44.54	45.54	0.13	1.57	1.70	6573	6262	495
GGR227	70.11	71.11	0.14	1.10	1.24	6572	6404	491
GGR230	40.61	41.61	0.34	0.60	0.94	6601	6158	489
GGR231	37.58	38.58	0.45	0.06	0.51	6563	6159	492
GGR231	62.58	63.58	0.38	0.78	1.15	6563	6159	467
S1090-08	74.50	75.50	0.02	0.54	0.56	6537	6352	478
S1102-08	67.00	68.00	0.97	1.20	2.17	6552	6493	497

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Table A-3: Getty Resource Estimate - December 2007
Nearest Neighbour Drill Hole Intercepts Sorted By - Length (m) x (Zn% +Pb%) Factor

Hole Id	From (m)	To (m)	Length (m)	Zn (%)	Pb (%)	Zn % + Pb %	Length (m) x (Zn% + Pb%)
GGR018	87.50	90.50	3.00	1.22	0.11	1.33	3.99
GGR019	91.80	95.06	3.26	0.22	1.21	1.43	4.66
GGR172	58.83	61.83	3.00	0.01	1.67	1.68	5.04
GGR231	78.03	82.78	4.75	0.70	0.67	1.37	6.51
S527	17.53	28.86	11.33	0.47	0.21	0.68	7.70
GGR221	94.31	99.61	5.30	0.82	0.69	1.51	8.00
GGR022	122.71	125.71	3.00	0.01	2.86	2.87	8.61
GGR102	22.86	29.32	6.46	0.45	0.99	1.44	9.30
GGR124	71.55	79.76	8.21	0.56	0.61	1.17	9.61
GGR113A	61.72	68.03	6.31	1.32	0.25	1.57	9.91
GGR178	23.10	29.90	6.80	0.56	0.90	1.46	9.93
GGR025A	27.37	33.53	6.16	0.77	1.08	1.85	11.40
GGR039A	35.39	43.13	7.74	1.28	0.31	1.59	12.31
GGR182	71.69	81.20	9.51	0.79	0.64	1.43	13.60
GGR230	26.82	38.53	11.71	1.11	0.09	1.20	14.05
GGR220	39.94	50.00	10.06	0.53	0.87	1.40	14.08
GGR222	26.82	35.66	8.84	0.46	1.18	1.64	14.50
GGR177	32.61	44.81	12.20	0.55	0.72	1.27	15.49
GGR040	28.35	41.03	12.68	0.52	0.83	1.35	17.12
GGR026	56.65	59.70	3.05	5.18	1.00	6.18	18.85
GGR116	44.10	60.96	16.86	0.94	0.18	1.12	18.88
GGR179	28.32	41.15	12.83	0.45	1.07	1.52	19.50
GGR021	42.06	49.68	7.62	2.29	0.56	2.85	21.72
GGR037	35.97	57.30	21.33	0.49	0.56	1.05	22.40
GGR215	26.00	38.77	12.77	0.59	1.20	1.79	22.86
GGR032	70.12	73.12	3.00	2.85	4.87	7.72	23.16
GGR158	65.53	81.47	15.94	0.56	0.91	1.47	23.43
GGR038	65.47	68.64	3.17	2.25	5.17	7.42	23.52
GGR036	27.58	62.48	34.90	0.63	0.05	0.68	23.73
GGR094	22.56	48.25	25.69	0.86	0.07	0.93	23.89
GGR024	26.82	34.14	7.32	1.36	2.05	3.41	24.96
GGR093	31.10	48.45	17.35	0.74	0.77	1.51	26.20
GGR027	43.29	61.59	18.30	1.21	0.24	1.45	26.54
GGR079	29.87	53.04	23.17	1.06	0.15	1.21	28.04
S526	80.07	87.48	7.41	2.23	1.62	3.85	28.53
GGR209	109.73	119.48	9.75	1.33	1.68	3.01	29.35
GGR130	27.44	49.85	22.41	1.06	0.26	1.32	29.58
GGR183	21.52	38.16	16.64	1.53	0.26	1.79	29.79
GGR103	32.25	54.25	22.00	1.11	0.28	1.39	30.58
GGR170	30.18	56.39	26.21	1.17	0.02	1.19	31.19
GGR193	36.58	64.31	27.73	0.57	0.58	1.15	31.89
GGR211	65.44	85.95	20.51	1.17	0.46	1.63	33.43
GGR167	25.45	39.20	13.75	0.58	2.08	2.66	36.58
GGR206	71.34	82.62	11.28	1.80	1.49	3.29	37.11
GGR192	40.36	62.64	22.28	1.22	0.63	1.85	41.22
GGR035A	46.65	83.51	36.86	0.82	0.32	1.14	42.02
GGR166	36.21	66.20	29.99	1.28	0.24	1.52	45.58
GGR173	41.45	58.67	17.22	1.40	1.37	2.77	47.70
GGR136	40.75	60.05	19.30	1.48	1.08	2.56	49.41

ACADIAN MINING CORP.
Table A-3: Getty Resource Estimate - December 2007
Nearest Neighbour Drill Hole Intercepts Sorted By - Length (m) x (Zn% +Pb%) Factor

Hole Id	From (m)	To (m)	Length (m)	Zn (%)	Pb (%)	Zn % + Pb %	Length (m) x (Zn% + Pb%)
GGR157	30.54	65.23	34.69	1.06	0.37	1.43	49.61
GGR219	46.63	60.78	14.15	0.47	3.10	3.57	50.52
GGR214	44.20	64.31	20.11	1.57	0.95	2.52	50.68
GGR126	120.21	130.18	9.97	0.09	5.15	5.24	52.24
GGR169	39.62	60.66	21.04	1.43	1.16	2.59	54.49
GGR181	25.00	58.54	33.54	1.42	0.28	1.70	57.02
GGR081	20.17	49.24	29.07	1.71	0.30	2.01	58.43
GGR208	98.37	105.70	7.33	2.67	5.36	8.03	58.86
GGR213	45.16	61.62	16.46	3.10	0.97	4.07	66.99
GGR176	39.94	60.76	20.82	1.52	1.89	3.41	71.00
GGR191	29.50	63.40	33.90	1.86	0.27	2.13	72.21
GGR217	18.11	45.72	27.61	1.35	1.40	2.75	75.93
GGR216	96.62	121.34	24.72	1.72	1.50	3.22	79.60
GGR135	38.10	66.60	28.50	1.53	1.33	2.86	81.51
GGR096	47.55	85.65	38.10	1.04	1.16	2.20	83.82
GGR125	58.54	98.60	40.06	0.92	1.33	2.25	90.14
GGR133	22.83	56.60	33.77	2.17	0.52	2.69	90.84
GGR129	40.23	63.40	23.17	2.21	2.07	4.28	99.17

ACADIAN MINING CORP.
Table A-1: Getty Resource Estimate - December 2007
Listing of Getty Project Drill Holes With Coordinates and Survey Data

Hole Id	Local Grid Easting (m)	Local Grid Northing (m)	Local Grid Elevation (m)	Depth (m)	Dip	Azimuth	Included in December 2007 Resource Outline	Drilled By
GGR012	7617.83	6616.13	519.66	101.04	-90	0	NO	Getty Mines
GGR013	7374.23	6621.59	513.62	169.50	-90	0	NO	Getty Mines
GGR014	7497.14	6613.84	514.26	144.80	-90	0	NO	Getty Mines
GGR015	7121.37	6641.60	523.93	112.80	-90	0	NO	Getty Mines
GGR017	7732.86	6672.02	535.00	144.50	-90	0	NO	Getty Mines
GGR018	6983.94	6653.60	535.38	67.40	-90	0	NO	Getty Mines
GGR019	6877.31	6658.86	542.96	66.80	-90	0	YES	Getty Mines
GGR020	6630.77	6628.38	561.67	62.80	-90	0	NO	Getty Mines
GGR021	6756.30	6628.57	549.68	57.30	-90	0	YES	Getty Mines
GGR022	6931.49	6641.35	539.06	71.02	-90	0	YES	Getty Mines
GGR023	7063.97	6652.07	527.74	85.04	-90	0	NO	Getty Mines
GGR024	7014.19	6765.62	526.58	78.94	-90	0	YES	Getty Mines
GGR025	6872.51	6764.38	543.16	139.60	-90	0	NO	Getty Mines
GGR025A	6874.55	6768.11	543.13	139.60	-90	0	YES	Getty Mines
GGR026	6760.72	6759.28	547.53	93.30	-90	0	YES	Getty Mines
GGR027	6636.42	6755.27	554.53	56.40	-90	0	YES	Getty Mines
GGR028	6516.48	6760.60	554.96	56.10	-90	0	NO	Getty Mines
GGR029	6397.32	6757.72	553.31	39.01	-90	0	NO	Getty Mines
GGR030	6252.36	6777.16	537.09	21.80	-90	0	NO	Getty Mines
GGR031	5985.54	6755.89	525.36	96.01	-90	0	NO	Getty Mines
GGR032	7116.82	6775.98	513.72	98.80	-90	0	YES	Getty Mines
GGR033	6882.52	7005.26	537.00	164.00	-90	0	NO	Getty Mines
GGR033A	6852.04	7004.99	540.00	170.08	-90	0	NO	Getty Mines
GGR034	6760.61	7004.18	543.37	164.59	-90	0	NO	Getty Mines
GGR035	6639.07	7006.17	545.10	94.20	-90	0	NO	Getty Mines
GGR035A	6602.04	7005.14	545.95	98.15	-90	0	YES	Getty Mines
GGR036	6633.62	6884.17	550.51	91.44	-90	0	YES	Getty Mines
GGR037	6510.67	6997.37	553.07	75.60	-90	0	YES	Getty Mines
GGR038	6508.73	6889.20	557.08	97.54	-90	0	YES	Getty Mines
GGR039	6382.04	6996.25	550.32	118.90	-90	0	NO	Getty Mines
GGR039A	6432.71	6986.68	552.83	106.70	-90	0	YES	Getty Mines
GGR040	6761.69	6882.26	545.84	85.34	-90	0	YES	Getty Mines
GGR041	6899.25	6871.29	542.00	73.20	-90	0	NO	Getty Mines

ACADIAN MINING CORP.
Table A-1: Getty Resource Estimate - December 2007
Listing of Getty Project Drill Holes With Coordinates and Survey Data

Hole Id	Local Grid Easting (m)	Local Grid Northing (m)	Local Grid Elevation (m)	Depth (m)	Dip	Azimuth	Included in December 2007 Resource Outline	Drilled By
GGR041A	6909.55	6879.00	540.97	73.15	-90	0	NO	Getty Mines
GGR042	6266.96	6987.61	538.50	105.20	-90	0	NO	Getty Mines
GGR043	6514.17	7123.92	548.00	101.35	-90	0	NO	Getty Mines
GGR044	6383.33	7131.90	547.00	115.80	-90	0	NO	Getty Mines
GGR044A	6381.49	7133.41	549.50	103.63	-90	0	NO	Getty Mines
GGR044B	6364.81	7123.51	552.00	115.82	-90	0	NO	Getty Mines
GGR045	6300.51	7122.33	539.00	149.40	-90	0	NO	Getty Mines
GGR046	6393.02	6898.50	550.11	87.50	-90	0	NO	Getty Mines
GGR066	7423.52	7697.41	550.00	289.00	-90	0	NO	Getty Mines
GGR067	7259.03	7513.06	550.00	151.80	-90	0	NO	Getty Mines
GGR068	7621.99	6731.08	522.00	169.20	-90	0	NO	Getty Mines
GGR069	4505.94	7103.97	550.00	125.00	-90	0	NO	Getty Mines
GGR070	7470.33	6887.33	520.00	143.60	-90	0	NO	Getty Mines
GGR071	6454.22	7215.44	542.50	152.10	-90	0	NO	Getty Mines
GGR072	7467.61	6884.87	522.00	135.33	-90	0	NO	Getty Mines
GGR073	4976.98	6988.36	550.00	342.60	-90	0	NO	Getty Mines
GGR074	7386.33	7250.53	545.00	154.84	-90	0	NO	Getty Mines
GGR075	6321.39	7311.50	545.00	128.02	-90	0	NO	Getty Mines
GGR076	6215.32	7241.67	532.00	176.50	-90	0	NO	Getty Mines
GGR077	7339.51	7615.58	550.00	212.80	-90	0	NO	Getty Mines
GGR078	6159.59	6995.19	534.00	100.00	-90	0	NO	Getty Mines
GGR079	6270.65	6877.94	535.97	57.91	-90	0	YES	Getty Mines
GGR080	5771.97	6744.24	520.00	139.90	-90	0	NO	Getty Mines
GGR081	6179.99	6868.08	539.73	60.96	-90	0	YES	Getty Mines
GGR082	6030.22	6872.73	531.00	64.01	-90	0	NO	Getty Mines
GGR083	5515.72	6869.69	519.00	94.50	-90	0	NO	Getty Mines
GGR084	5516.76	6752.95	519.00	212.80	-90	0	NO	Getty Mines
GGR086	5802.28	6865.83	525.00	140.21	-90	0	NO	Getty Mines
GGR087	6186.70	6757.68	532.00	33.53	-90	0	NO	Getty Mines
GGR088	5907.53	6993.26	528.00	103.02	-90	0	NO	Getty Mines
GGR089	5882.51	6756.20	520.00	113.70	-90	0	NO	Getty Mines
GGR090	6867.27	6903.62	540.00	145.70	-90	0	NO	Getty Mines
GGR091	5903.42	7009.68	519.00	138.84	-90	0	NO	Getty Mines

ACADIAN MINING CORP.
Table A-1: Getty Resource Estimate - December 2007
Listing of Getty Project Drill Holes With Coordinates and Survey Data

Hole Id	Local Grid Easting (m)	Local Grid Northing (m)	Local Grid Elevation (m)	Depth (m)	Dip	Azimuth	Included in December 2007 Resource Outline	Drilled By
GGR092	6530.99	6636.98	565.00	79.20	-90	0	NO	Getty Mines
GGR093	6337.78	6631.60	548.00	50.30	-90	0	YES	Getty Mines
GGR094	6259.53	6621.77	539.00	44.81	-90	0	YES	Getty Mines
GGR095	6150.25	7120.69	532.00	136.60	-90	0	NO	Getty Mines
GGR096	6148.19	6631.45	531.00	93.00	-90	0	YES	Getty Mines
GGR097	6023.20	6633.69	526.00	146.30	-90	0	NO	Getty Mines
GGR098	6027.76	7149.78	531.00	133.50	-90	0	NO	Getty Mines
GGR099	5904.37	6627.76	523.00	210.31	-90	0	NO	Getty Mines
GGR101	6022.32	6526.09	528.00	149.40	-90	0	NO	Getty Mines
GGR102	6145.95	6540.59	531.00	105.20	-90	0	YES	Getty Mines
GGR103	6267.52	6512.10	542.00	86.90	-90	0	YES	Getty Mines
GGR104	7248.46	6642.73	522.00	131.10	-90	0	NO	Getty Mines
GGR105	7241.90	6764.60	522.00	125.00	-90	0	NO	Getty Mines
GGR109	7373.99	6752.36	517.00	146.30	-90	0	NO	Getty Mines
GGR110	6572.52	7246.36	540.00	122.53	-90	0	NO	Getty Mines
GGR111	6219.00	6937.00	535.14	96.93	-90	0	NO	Getty Mines
GGR112	6456.54	6940.85	552.00	100.60	-90	0	NO	Getty Mines
GGR113	6349.37	6951.91	547.67	80.80	-90	0	NO	Getty Mines
GGR113A	6314.64	6952.33	543.03	88.10	-90	0	YES	Getty Mines
GGR114	6209.94	7058.12	533.00	157.90	-90	0	NO	Getty Mines
GGR115	6333.37	7059.83	541.00	131.70	-90	0	NO	Getty Mines
GGR116	6455.35	7062.64	544.35	92.70	-90	0	YES	Getty Mines
GGR117	6577.28	7063.57	545.03	90.22	-90	0	NO	Getty Mines
GGR118	6578.24	6941.57	553.45	94.50	-90	0	NO	Getty Mines
GGR119	6700.49	6943.29	548.00	118.90	-90	0	NO	Getty Mines
GGR121	6696.06	7064.87	544.00	129.54	-90	0	NO	Getty Mines
GGR122	6823.62	6944.38	545.50	128.02	-90	0	NO	Getty Mines
GGR123	6945.04	6822.98	539.79	137.80	-90	0	NO	Getty Mines
GGR124	6833.02	6816.70	547.51	129.54	-90	0	YES	Getty Mines
GGR125	6937.67	6695.79	540.02	69.50	-90	0	YES	Getty Mines
GGR126	6694.59	6818.27	548.15	73.20	-90	0	YES	Getty Mines
GGR129	6815.65	6701.67	548.50	103.02	-90	0	YES	Getty Mines
GGR130	6576.21	6825.64	557.60	70.10	-90	0	YES	Getty Mines

ACADIAN MINING CORP.
Table A-1: Getty Resource Estimate - December 2007
Listing of Getty Project Drill Holes With Coordinates and Survey Data

Hole Id	Local Grid Easting (m)	Local Grid Northing (m)	Local Grid Elevation (m)	Depth (m)	Dip	Azimuth	Included in December 2007 Resource Outline	Drilled By
GGR131	6457.44	6818.60	553.00	64.01	-90	0	NO	Getty Mines
GGR132	6335.52	6817.52	540.00	42.70	-90	0	NO	Getty Mines
GGR133	6696.64	6693.62	552.13	78.33	-90	0	YES	Getty Mines
GGR134	6574.48	6701.11	559.04	45.11	-90	0	NO	Getty Mines
GGR135	6216.08	6811.66	537.60	48.80	-90	0	YES	Getty Mines
GGR136	6091.68	6813.84	530.62	45.50	-90	0	YES	Getty Mines
GGR137	6455.47	6696.96	552.00	42.10	-90	0	NO	Getty Mines
GGR138	5969.78	6814.28	523.00	90.22	-90	0	NO	Getty Mines
GGR139	6335.06	6697.72	541.00	28.04	-90	0	NO	Getty Mines
GGR140	7065.07	6699.63	535.00	70.10	-90	0	NO	Getty Mines
GGR141	6211.64	6694.50	524.00	23.80	-90	0	NO	Getty Mines
GGR142	6089.10	6696.63	531.00	75.30	-90	0	NO	Getty Mines
GGR143	7423.62	6827.17	520.00	143.30	-90	0	NO	Getty Mines
GGR144	7352.98	6887.51	519.00	146.30	-90	0	NO	Getty Mines
GGR145	5967.81	6692.33	525.00	140.21	-90	0	NO	Getty Mines
GGR146	6097.88	6939.98	533.00	63.40	-90	0	NO	Getty Mines
GGR147	5968.70	6936.19	527.00	100.00	-90	0	NO	Getty Mines
GGR149	7660.88	6676.87	529.00	140.21	-90	0	NO	Getty Mines
GGR150	7556.06	6672.89	525.00	151.18	-90	0	NO	Getty Mines
GGR151	7434.11	6674.86	519.00	149.40	-90	0	NO	Getty Mines
GGR152	7313.45	6704.27	520.00	130.50	-90	0	NO	Getty Mines
GGR153	7682.07	6555.44	526.00	103.33	-90	0	NO	Getty Mines
GGR154	7682.07	6555.44	526.00	76.20	-90	0	NO	Getty Mines
GGR155	7730.30	6615.91	537.00	118.90	-90	0	NO	Getty Mines
GGR156	7069.18	6580.18	527.00	84.73	-90	0	NO	Getty Mines
GGR157	6942.75	6576.04	538.07	56.70	-90	0	YES	Getty Mines
GGR158	6816.85	6575.43	546.07	45.11	-90	0	YES	Getty Mines
GGR159	6703.38	6576.94	556.78	40.84	-90	0	NO	Getty Mines
GGR160	7438.26	6551.44	519.00	143.30	-90	0	NO	Getty Mines
GGR161	6072.52	6571.03	527.00	106.10	-90	0	NO	Getty Mines
GGR162	6072.00	6624.00	527.00	111.30	-90	0	NO	Getty Mines
GGR163	6163.00	6572.00	530.00	83.10	-90	0	NO	Getty Mines
GGR164	6123.56	6693.72	530.00	35.81	-90	0	NO	Getty Mines

ACADIAN MINING CORP.
Table A-1: Getty Resource Estimate - December 2007
Listing of Getty Project Drill Holes With Coordinates and Survey Data

Hole Id	Local Grid Easting (m)	Local Grid Northing (m)	Local Grid Elevation (m)	Depth (m)	Dip	Azimuth	Included in December 2007 Resource Outline	Drilled By
GGR165	6156.06	6783.26	532.56	31.40	-90	0	NO	Getty Mines
GGR166	6152.40	6820.75	536.88	39.93	-90	0	YES	Getty Mines
GGR167	6152.32	6850.95	539.70	43.90	-90	0	YES	Getty Mines
GGR168	6154.95	6905.77	536.57	58.52	-90	0	NO	Getty Mines
GGR169	6221.54	6575.10	536.00	71.32	-90	0	YES	Getty Mines
GGR170	6190.61	6626.03	535.00	60.40	-90	0	YES	Getty Mines
GGR171	6275.49	6815.46	538.00	39.93	-90	0	NO	Getty Mines
GGR172	6274.69	6845.40	537.44	55.80	-90	0	YES	Getty Mines
GGR173	6275.35	6906.94	537.02	69.80	-90	0	YES	Getty Mines
GGR174	6396.93	6870.49	545.00	84.73	-90	0	NO	Getty Mines
GGR176	6481.52	6883.13	555.85	102.60	-90	0	YES	Getty Mines
GGR177	6483.93	6912.73	556.44	90.83	-90	0	YES	Getty Mines
GGR178	6483.19	6942.88	555.89	78.33	-90	0	YES	Getty Mines
GGR179	6482.30	6971.60	554.91	86.30	-90	0	YES	Getty Mines
GGR180	6480.15	7005.28	552.81	72.54	-90	0	NO	Getty Mines
GGR181	6482.35	7031.82	550.13	77.82	-90	0	YES	Getty Mines
GGR182	6483.12	6847.47	554.18	80.99	-90	0	YES	Getty Mines
GGR183	6537.83	6896.69	557.70	80.50	-90	0	YES	Getty Mines
GGR184	6555.95	6919.19	556.60	80.50	-90	0	NO	Getty Mines
GGR190	6614.28	6731.29	555.01	48.20	-90	0	NO	Getty Mines
GGR191	6656.29	6776.18	553.42	63.40	-90	0	YES	Getty Mines
GGR192	6678.02	6796.82	550.77	72.24	-90	0	YES	Getty Mines
GGR193	6719.08	6841.98	548.09	78.64	-90	0	YES	Getty Mines
GGR205	6706.16	6610.49	554.92	46.94	-90	0	NO	Getty Mines
GGR206	6779.26	6654.11	548.47	70.71	-90	0	YES	Getty Mines
GGR208	6846.62	6719.39	545.11	109.73	-90	0	YES	Getty Mines
GGR209	6868.71	6740.56	544.05	122.22	-90	0	YES	Getty Mines
GGR210	6882.05	6782.73	543.07	124.40	-90	0	NO	Getty Mines
GGR211	7031.21	6634.64	533.26	61.30	-90	0	YES	Getty Mines
GGR212	6898.35	6651.37	541.45	100.60	-90	0	NO	Getty Mines
GGR213	6921.08	6674.85	540.35	61.00	-90	0	YES	Getty Mines
GGR214	6972.24	6727.87	536.30	74.70	-90	0	YES	Getty Mines
GGR215	6998.48	6750.40	537.70	72.24	-90	0	YES	Getty Mines

ACADIAN MINING CORP.
Table A-1: Getty Resource Estimate - December 2007
Listing of Getty Project Drill Holes With Coordinates and Survey Data

Hole Id	Local Grid Easting (m)	Local Grid Northing (m)	Local Grid Elevation (m)	Depth (m)	Dip	Azimuth	Included in December 2007 Resource Outline	Drilled By
GGR216	7040.53	6787.83	517.25	65.23	-90	0	YES	Getty Mines
GGR217	6395.36	6946.57	551.48	127.41	-90	0	YES	Getty Mines
GGR219	6844.98	6598.95	545.17	55.50	-90	0	YES	Getty Mines
GGR220	6341.10	6567.32	552.00	77.11	-90	0	YES	Getty Mines
GGR221	6262.40	6573.02	540.00	72.54	-90	0	YES	Getty Mines
GGR222	6096.97	6850.50	537.10	42.10	-90	0	YES	Getty Mines
GGR223	6091.52	6784.73	531.34	44.50	-90	0	NO	Getty Mines
GGR224	6737.45	6863.75	546.37	80.80	-90	0	NO	Getty Mines
GGR225	6461.57	6627.83	547.00	53.95	-90	0	NO	Getty Mines
GGR226	6461.74	6574.48	562.00	70.41	-90	0	NO	Getty Mines
GGR227	6403.58	6572.10	562.00	76.20	-90	0	NO	Getty Mines
GGR228	6404.57	6627.62	557.00	52.43	-90	0	NO	Getty Mines
GGR229	6276.38	6784.08	538.00	30.80	-90	0	NO	Getty Mines
GGR230	6157.91	6600.75	530.00	53.04	-90	0	YES	Getty Mines
GGR231	6158.85	6563.26	530.00	72.54	-90	0	YES	Getty Mines
S277	6997.39	6500.29	530.42	108.81	-90	0	NO	Imperial Oil
S526	6941.67	6520.86	535.42	68.58	-90	0	YES	Imperial Oil
S527	6881.68	6517.20	541.85	52.73	-90	0	YES	Imperial Oil
S528	6818.68	6517.20	545.96	35.66	-90	0	NO	Imperial Oil
Twin Holes By Acadian								
S1021-07	6731.32	6614.94	555.01	41.00	-90	0	NO	Acadian
S1025-07	6651.11	6897.88	541.49	62.00	-90	0	NO	Acadian
S1043-07	6773.05	6958.01	536.65	68.00	-90	0	NO	Acadian
S1059-08	6512.286	6997.462	553.103	71.00	-90	0	NO	Acadian

Table A-4: Getty Resource Estimate - 2007
Lithocode Summary

Lithocode	Primary Rock Description	Primary Modifier	Description	Secondary Modifier	Description
OB	Overburden	GYP	gypsiiferous	LM	Limestone
LM	Limestone	MA	massive	DOL	Dolostone
DOL	Dolostone	FOL	foliated	GYP	Gypsum
GYP	Gypsum	FS	fossiliferous	ANH	Anhydrite
ANH	Anhydrite	IMP	impure	G	Greywacke
G	Greywacke	BIOT	bioturbated	A	Argillite
A	Argillite	LAM	laminated	VD	Void/Cavity
VD	Void/Cavity	TB	thin bedded	SS	Sandstone
SS	Sandstone			SLT	Siltstone
SLT	Siltstone			MST	Mudstone
MST	Mudstone			CGL	Conglomerate
CGL	Conglomerate				
BX	Breccia				

ALS Chemex

Sample Preparation Package – PREP-31

Standard Sample Preparation: Dry, Crush, Split and Pulverize

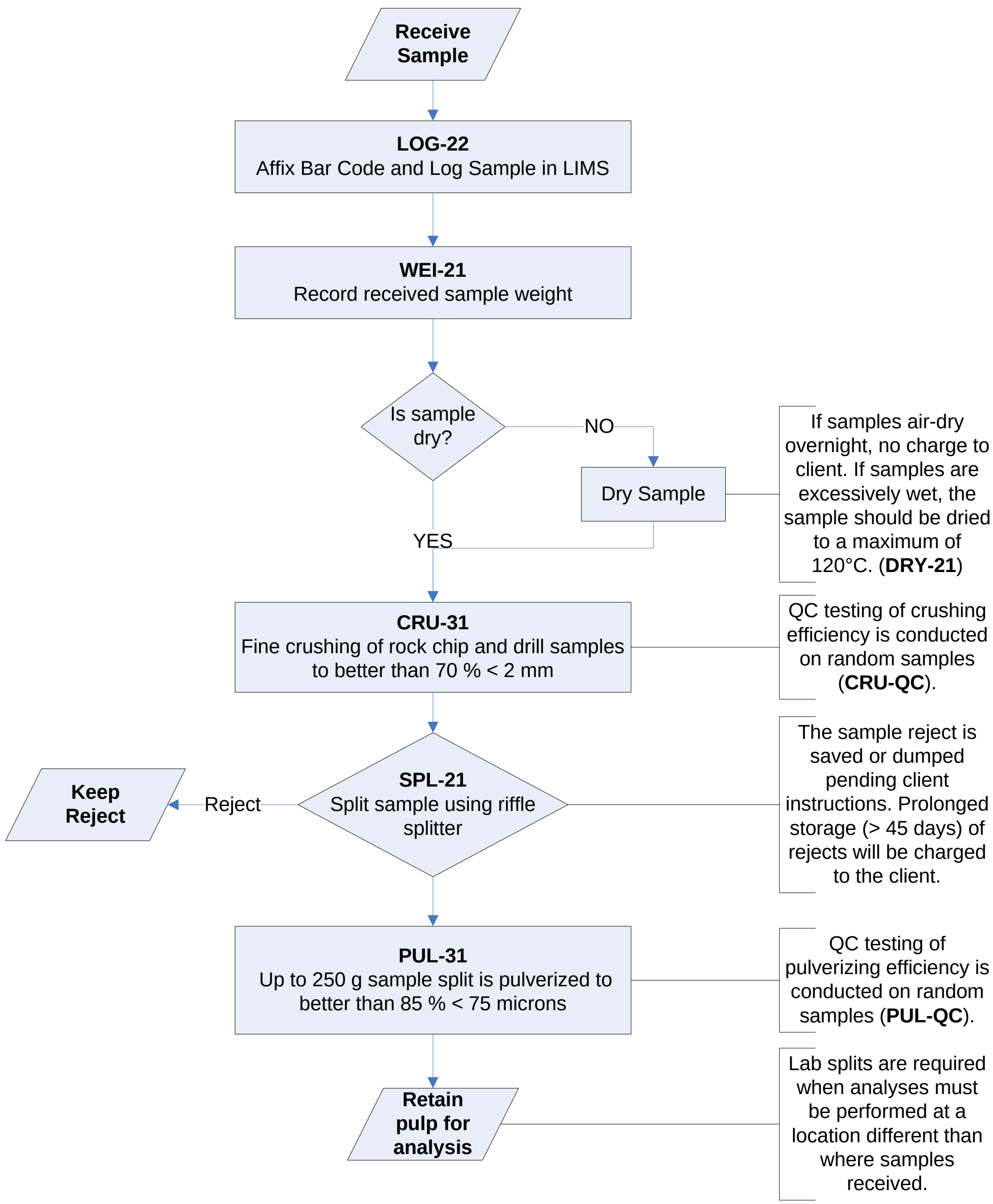
Sample preparation is the most critical step in the entire laboratory operation. The purpose of preparation is to produce a homogeneous analytical sub-sample that is fully representative of the material submitted to the laboratory.

The sample is logged in the tracking system, weighed, dried and finely crushed to better than 70 % passing a 2 mm (Tyler 9 mesh, US Std. No.10) screen. A split of up to 250 g is taken and pulverized to better than 85 % passing a 75 micron (Tyler 200 mesh, US Std. No. 200) screen. This method is appropriate for rock chip or drill samples.

Method Code	**Description**
LOG-22	Sample is logged in tracking system and a bar code label is attached.
CRU-31	Fine crushing of rock chip and drill samples to better than 70 % of the sample passing 2 mm.
SPL-21	Split sample using riffle splitter.
PUL-31	A sample split of up to 250 g is pulverized to better than 85 % of the sample passing 75 microns.

ALS Chemex

Flow Chart - Sample Preparation Package – PREP-31
Standard Sample Preparation: Dry, Crush, Split and Pulverize



ALS Chemex

Ore Grade Analysis by XRF – ME-XRF10

Sample Decomposition: 50% $Li_2B_4O_7$ – 50% $LiBO_2$ (WEI-GRA06)
Analytical Method: X-Ray Fluorescence Spectroscopy (XRF)

A calcined or ignited sample (0.9 g) is added to 9.0g of Lithium Borate Flux (50 % - 50 % $Li_2B_4O_7$ – $LiBO_2$), mixed well and fused in an auto fluxer between 1050 - 1100°C. A flat molten glass disc is prepared from the resulting melt. This disc is then analysed by X-ray fluorescence spectrometry.

Element	Symbol	Units	Lower Limit	Upper Limit
Barium	Ba	%	0.01	50
Niobium	Nb	%	0.01	10
Antimony	Sb	%	0.01	50
Tin	Sn	%	0.01	60
Tantalum	Ta	%	0.01	50
Thorium	Th	%	0.01	15
Uranium	U	%	0.01	15
Tungsten	W	%	0.01	50
Zirconium	Zr	%	0.01	50

Elements listed below are available upon request

Element	Symbol	Units	Lower Limit	Upper Limit
Iron	Fe_2O_3	%	0.01	100
Potassium	K_2O	%	0.01	100
Magnesium	MgO	%	0.01	100
Sodium	Na_2O	%	0.01	100

ALS Chemex

Assay Procedure – ME-OG62
Ore Grade Elements by Four Acid Digestion Using Conventional ICP-AES Analysis

Sample Decomposition: HNO_3-$HClO_4$-HF-HCl Digestion (ASY-4A01)
Analytical Method: Inductively Coupled Plasma - Atomic Emission Spectroscopy (ICP - AES)*

Assays for the evaluation of ores and high-grade materials are optimized for accuracy and precision at high concentrations. Ultra high concentration samples (> 15 -20%) may require the use of methods such as titrimetric and gravimetric analysis, in order to achieve maximum accuracy.

A prepared sample is digested with nitric, perchloric, hydrofluoric, and hydrochloric acids, and then evaporated to incipient dryness. Hydrochloric acid and de-ionized water is added for further digestion, and the sample is heated for an additional allotted time. The sample is cooled to room temperature and transferred to a volumetric flask (100 mL). The resulting solution is diluted to volume with de-ionized water, homogenized and the solution is analyzed by inductively coupled plasma - atomic emission spectroscopy or by atomic absorption spectrometry.

***NOTE**: ICP-AES is the default finish technique for ME-OG62. However, under some conditions and at the discretion of the laboratory an AA finish may be substituted. The certificate will clearly reflect which instrument finish was used.

Element	Symbol	Units	Lower Limit	Upper Limit
Silver	Ag	ppm	1	1500
Arsenic	As	%	0.01	30
Bismuth	Bi	%	0.01	30
Cadmium	Cd	%	0.0001	10
Cobalt	Co	%	0.001	20

Element	Symbol	Units	Lower Limit	Upper Limit
Chromium	Cr	%	0.002	30
Copper	Cu	%	0.01	40
Iron	Fe	%	0.01	100
Manganese	Mn	%	0.01	50
Molybdenum	Mo	%	0.001	10
Nickel	Ni	%	0.01	30
Lead	Pb	%	0.01	20
Zinc	Zn	%	0.01	30

Eastern Analytical Ltd. Preparation and Analytical Procedures

SAMPLE PREPARATION

ROCK/CORE

Samples are organized and labeled when they enter the lab. They are then placed in drying ovens until they are completely dry.

After drying is complete samples are taken and crushed in a Rhino Jaw Crusher to approximately 75% -10 mesh material.

The complete sample is rifle split until we are left with approximately 250 – 300 grams of material. The remainder of the sample is bagged and stored as coarse reject.

The 250 – 300 gram split is then pulverized using a ring mill to approximately 98% -150 mesh material.

SOILS/STREAMS/SILTS

Soils are dried at 90^{o}F. They are then pounded with a rubber mallet in the soil bag. Then the soil is screened through a 80 mesh screen. The -80 fraction is rolled and kept as the sample. The +80 mesh fraction is discarded.

ASSAY PROCEDURE FOR CU/PB/ZN/NI/CO

A 0.200g sample is digested in a beaker with 10ml of nitric acid and 5ml of hydrochloric acid for 45 minutes. Samples are then transferred to 100ml volumetric flasks and then analyzed on the AA.

Lower detection limit is 0.01%, no upper detection limit.

ASSAY PROCEDURE FOR AG

A 1000mg sample is digested in a 500ml beaker with 10ml of hydrochloric acid and 10ml of nitric acid with the cover left on for 1 hour. Remove the covers and evaporate to a moist paste. Add 25ml of hydrochloric acid and 25ml of deoinized water, heat gently and swirl to dissolve solids. Cool, transfer to 100ml Volumetric and analyze on the AA.Lower detection limit is 0.01oz/t, no upper detection limit.

PROCEDURE FOR AR-ICP30

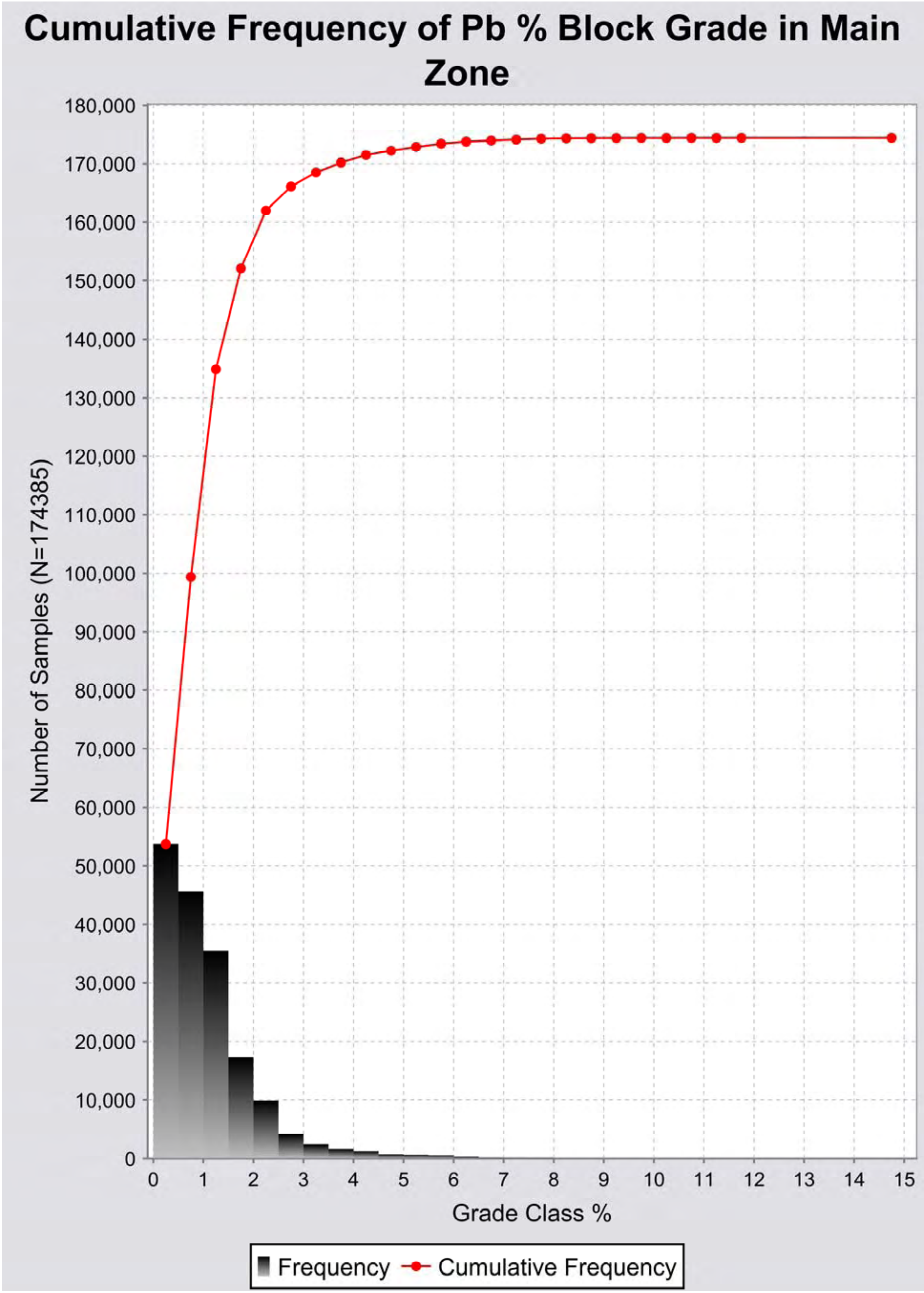
Each rack is to contain one blank, two CanMet standards and 37 unknowns, of which two will be duplicates.

A 0.500 gram sample is digested with 2ml HNO3 in a 95^{o}C water bath for ½ hour, after which 1ml HCL is added and the samples is returned to the water bath for an additional ½ hour. After cooling, samples are diluted to 10ml with deionized water, stirred and let stand for 1 hour to allow precipitate to settle. They are now prepared for ICP analysis.

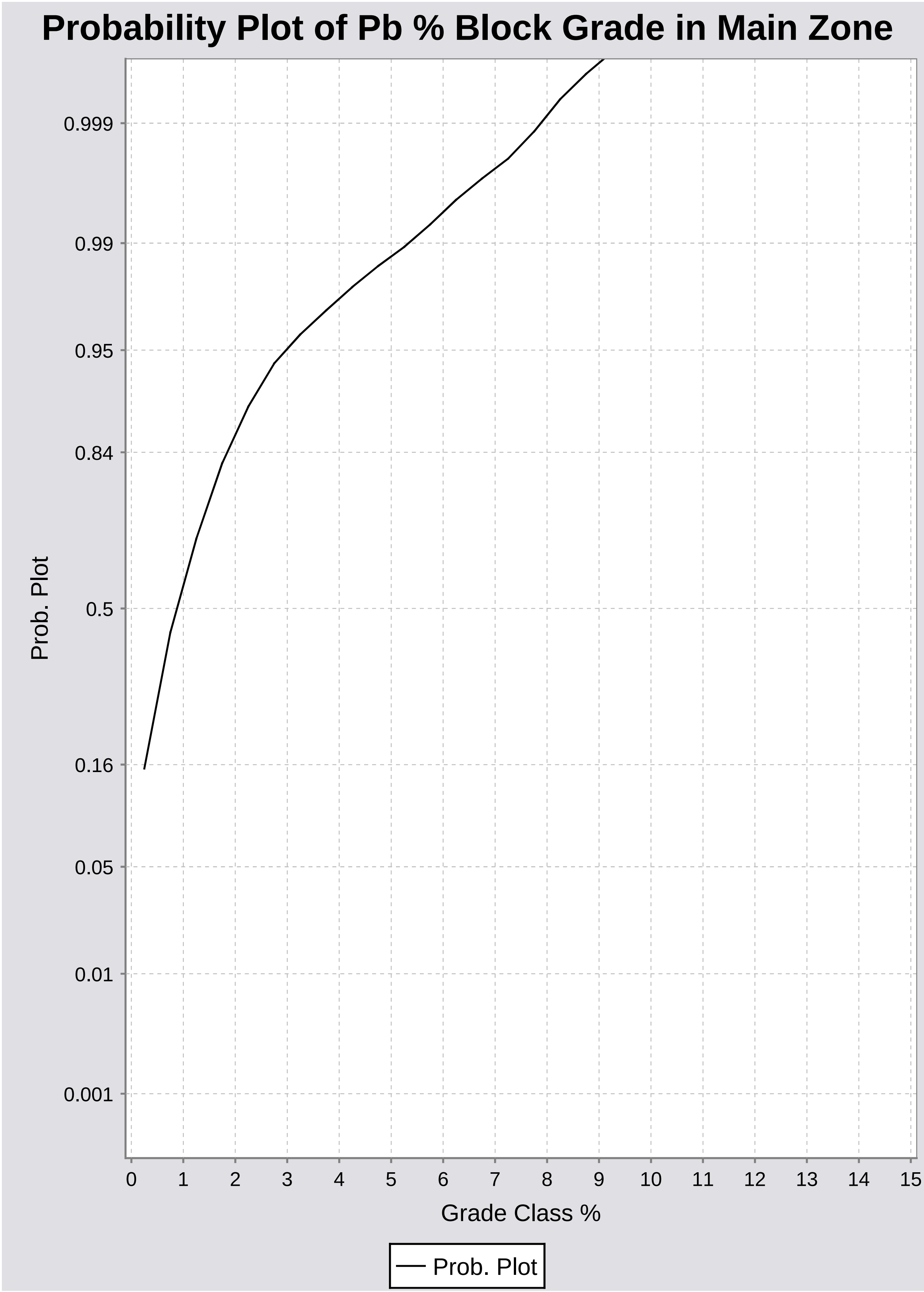
Updated January 25, 2008

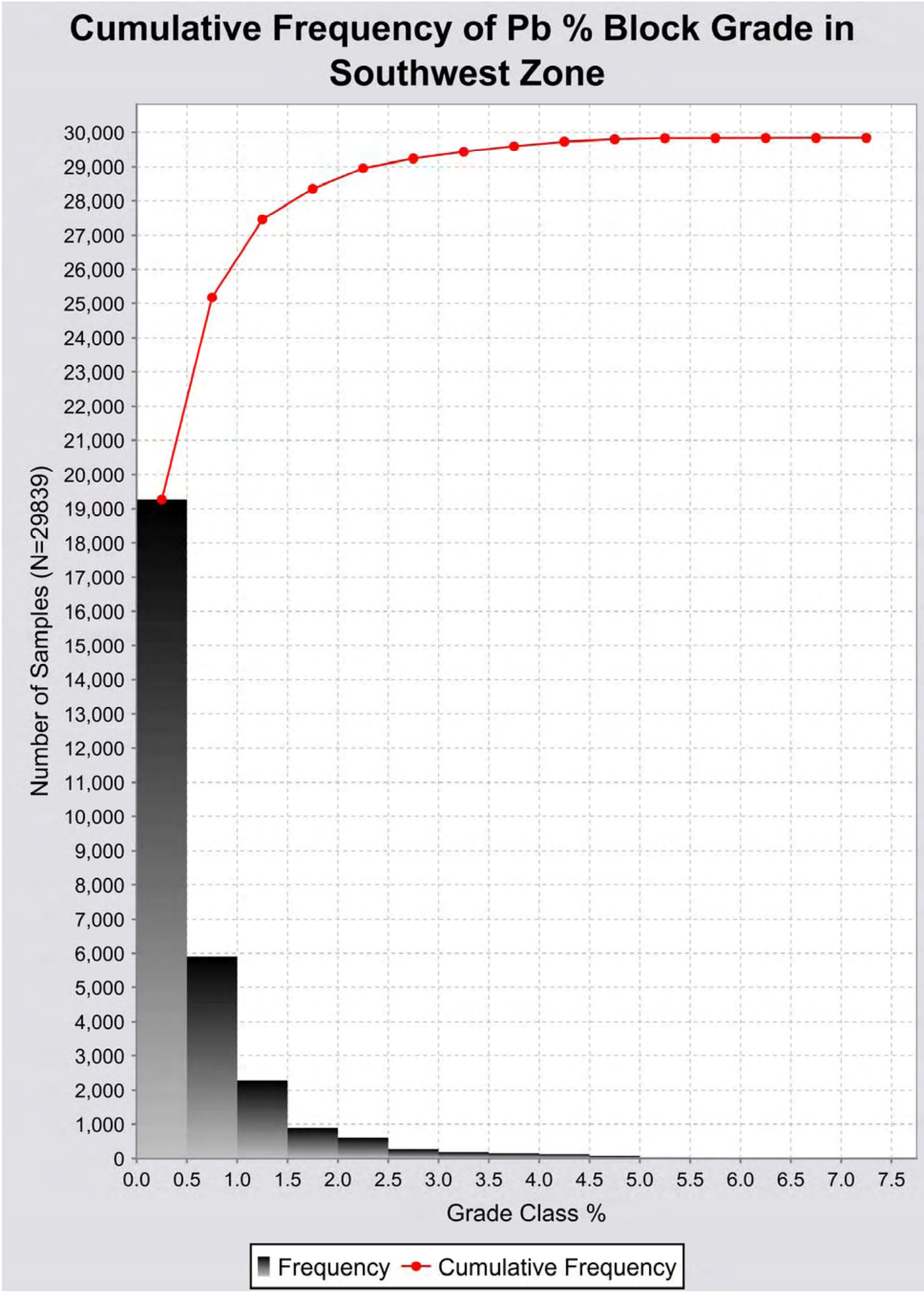
Appendix 3: Resource Estimate Support Documents

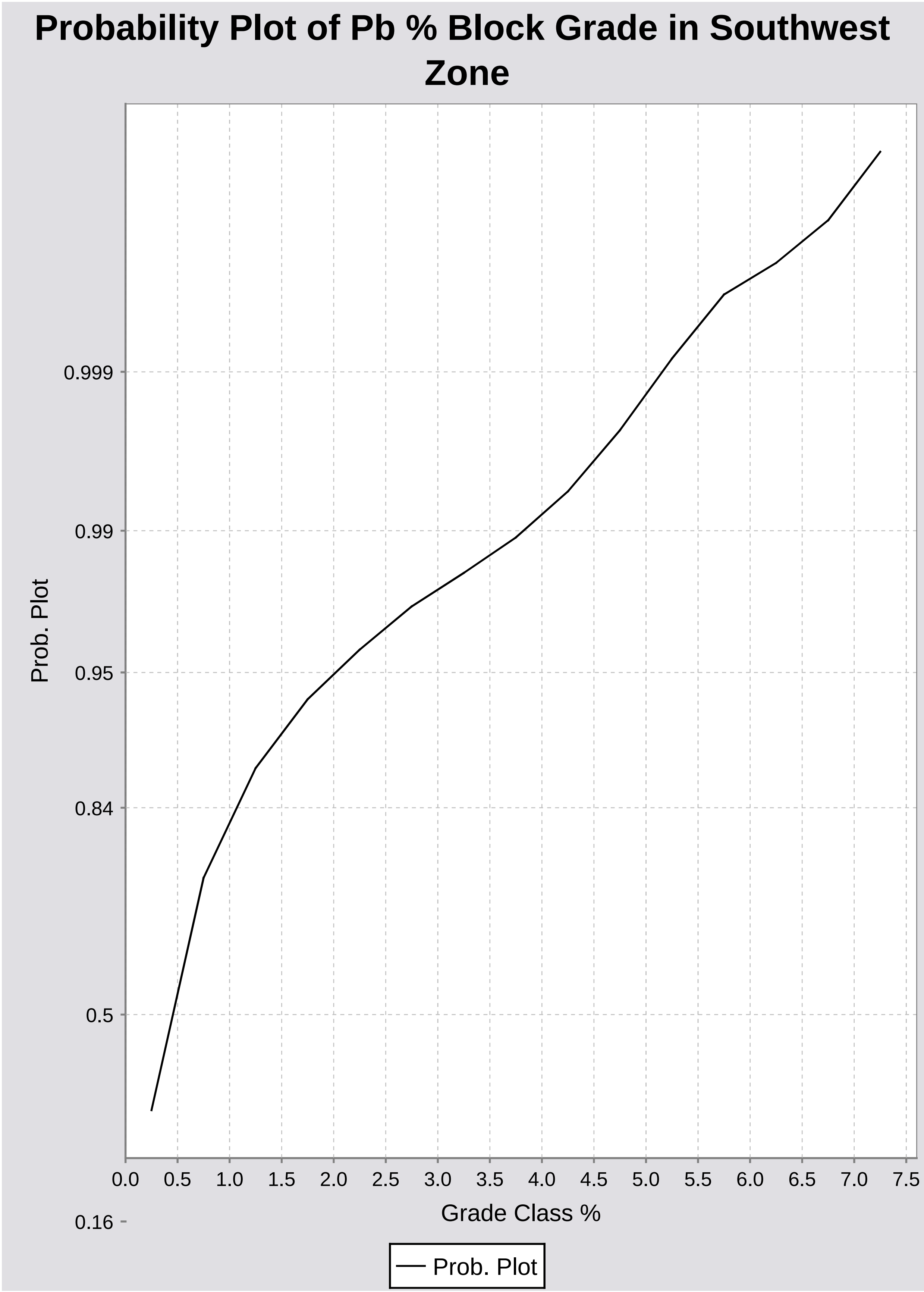
Histograms and Cumulative Frequency Plots
Total Population Variograms

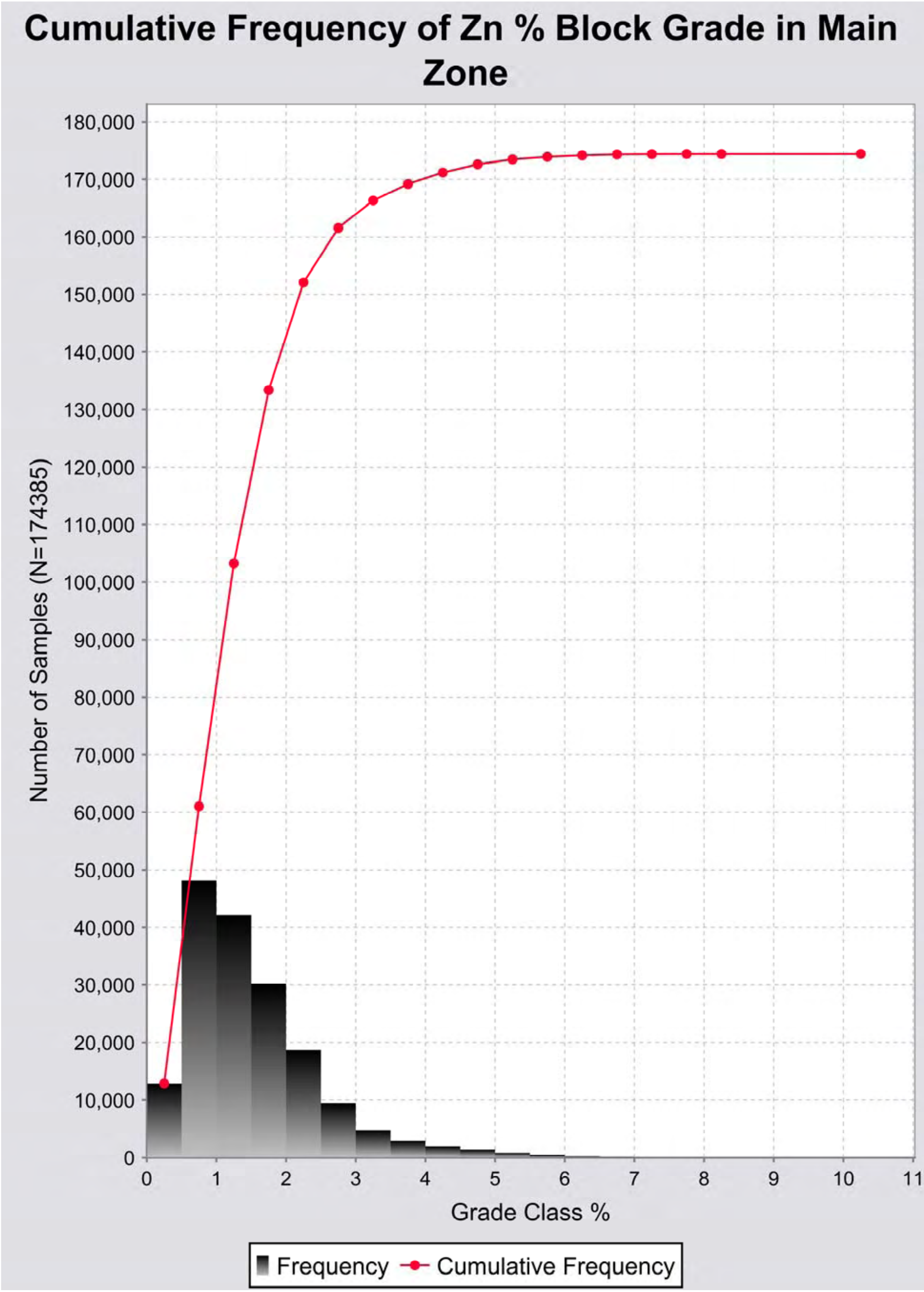


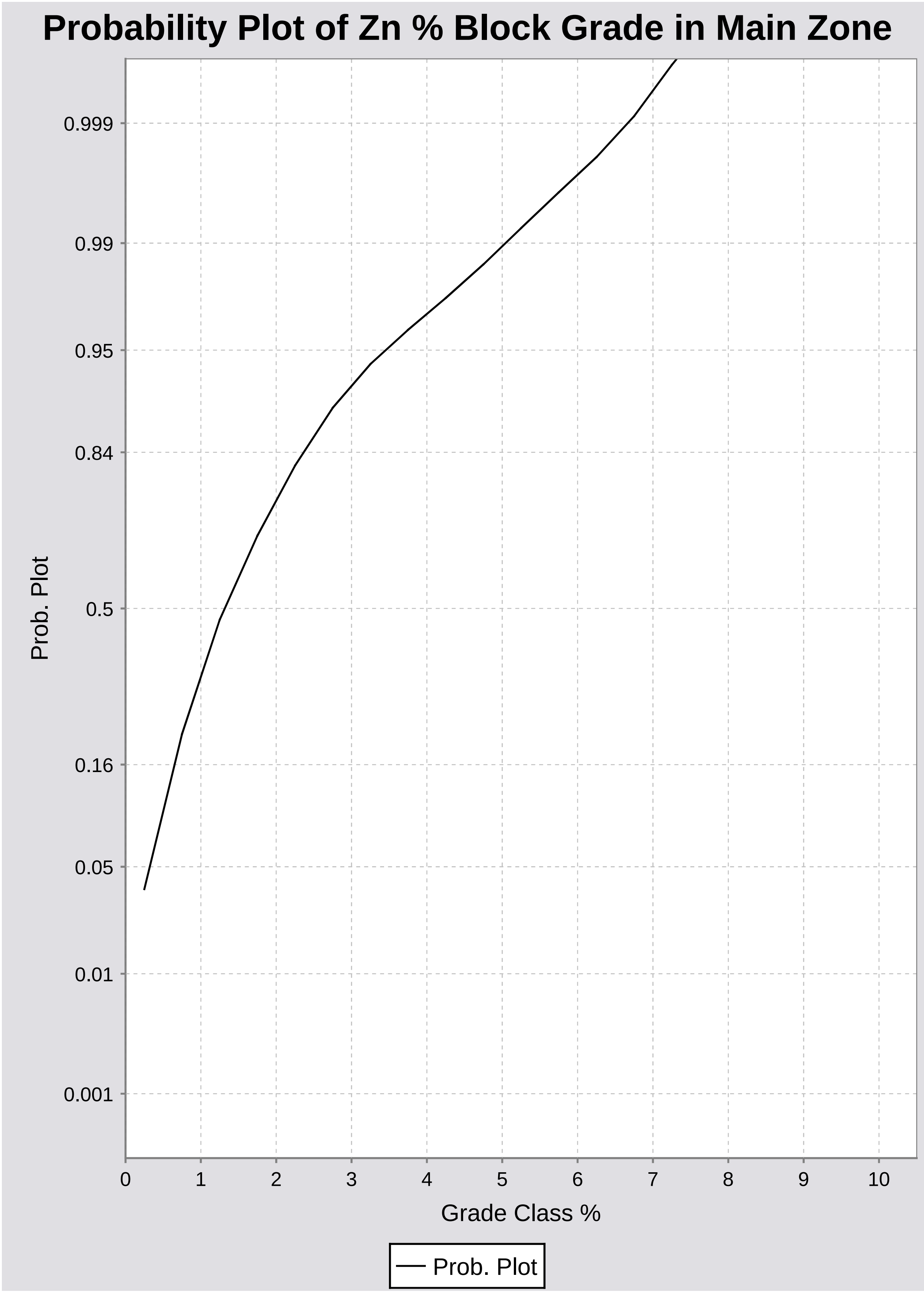
Cumulative Frequency of Pb % Block Grade in Main Zone
Number of Samples (N=174385)
180,000
170,000
160,000
150,000
140,000
130,000
120,000
110,000
100,000
90,000
80,000
70,000
60,000
50,000
40,000
30,000
20,000
10,000
0
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
Grade Class %
Frequency
Cumulative Frequency

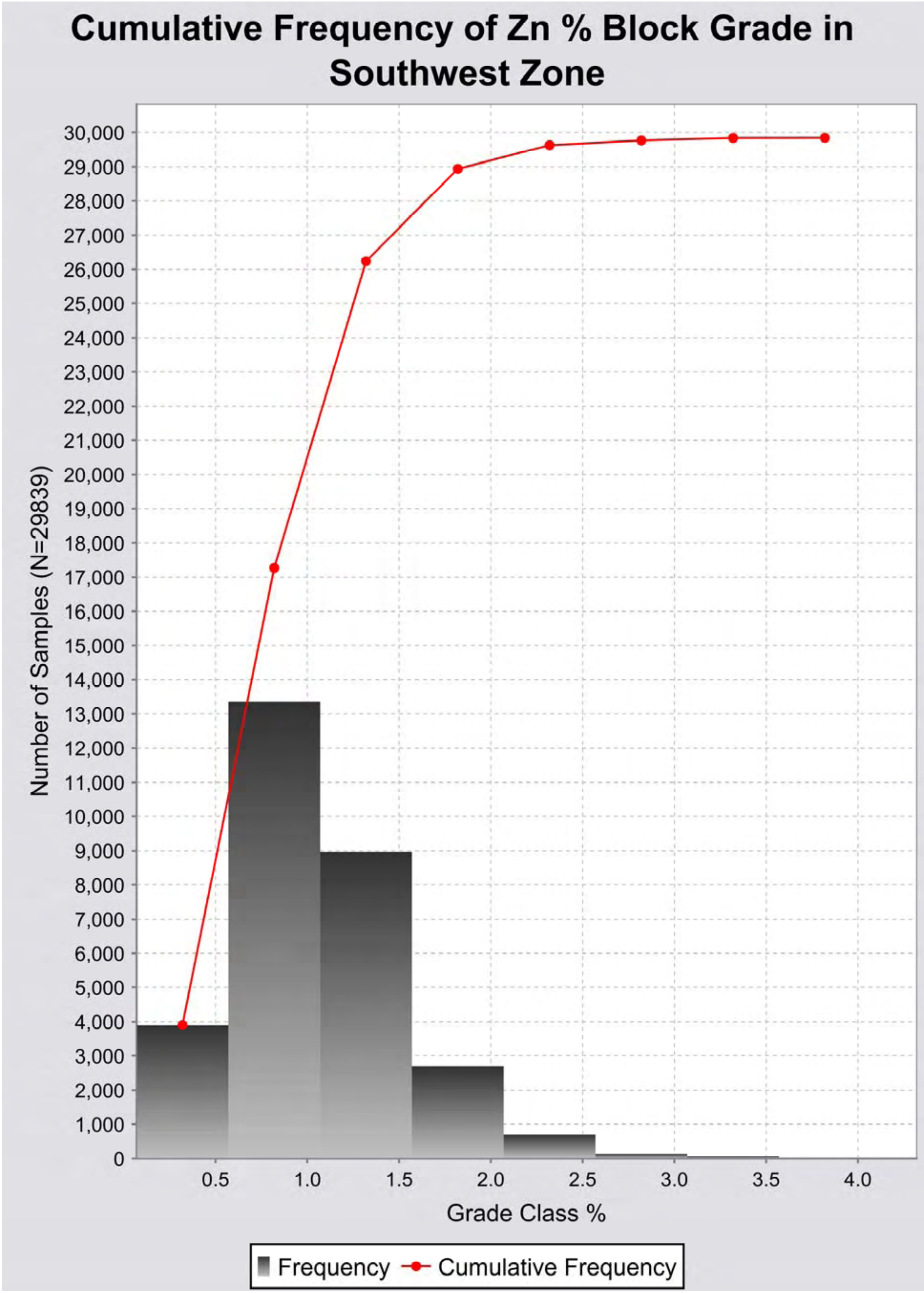

Probability Plot of Pb % Block Grade in Main Zone
Prob. Plot
0.999
0.99
0.95
0.84
0.5
0.16
0.05
0.01
0.001
0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
Grade Class %
Prob. Plot

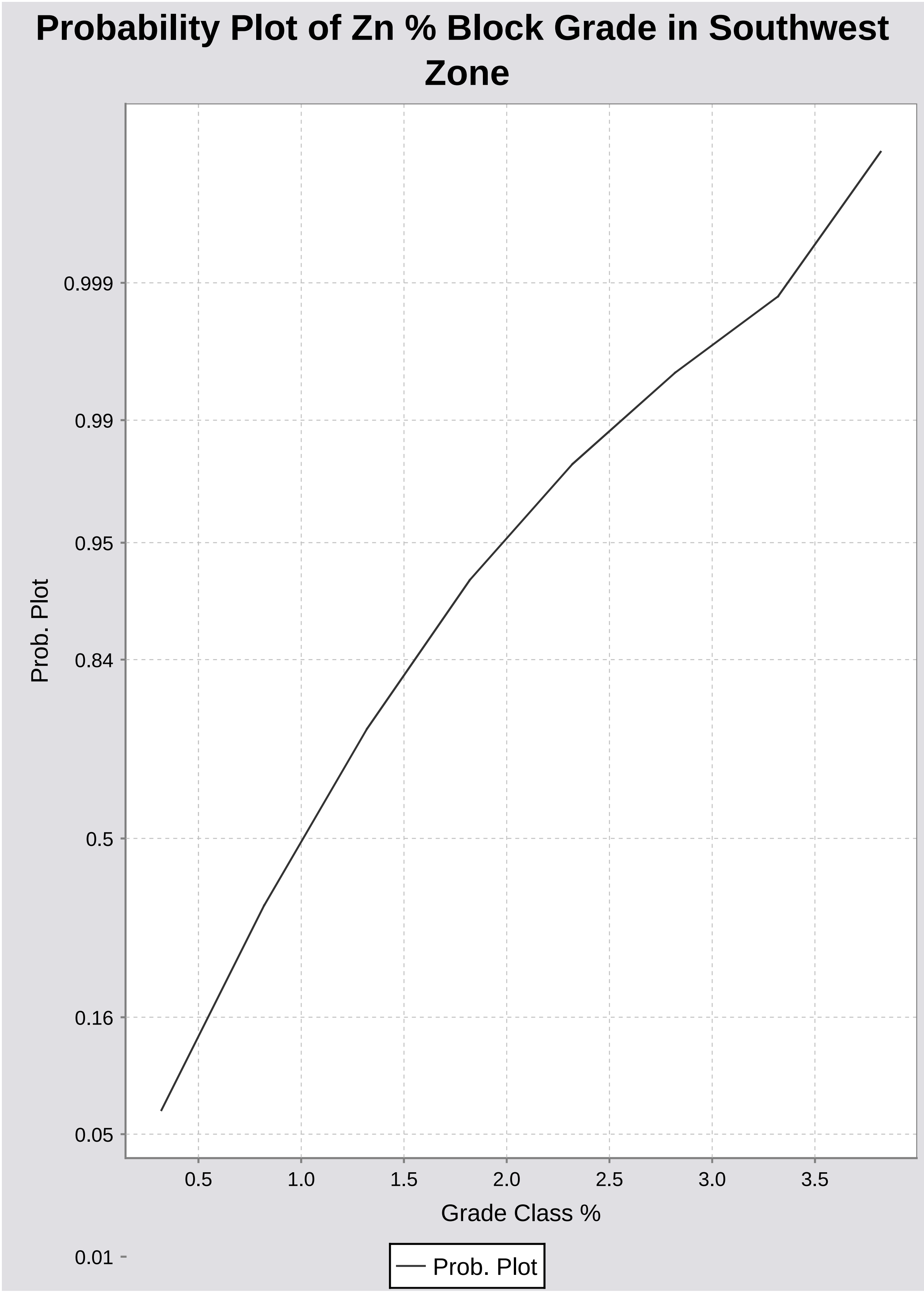

Cumulative Frequency of Pb % Block Grade in Southwest Zone
Number of Samples (N=29839)
30,000
29,000
28,000
27,000
26,000
25,000
24,000
23,000
22,000
21,000
20,000
19,000
18,000
17,000
16,000
15,000
14,000
13,000
12,000
11,000
10,000
9,000
8,000
7,000
6,000
5,000
4,000
3,000
2,000
1,000
0
0.0 0.5 1.0 1.5 2.0 2.5 3.0 3.5 4.0 4.5 5.0 5.5 6.0 6.5 7.0 7.5
Grade Class %
Frequency
Cumulative Frequency

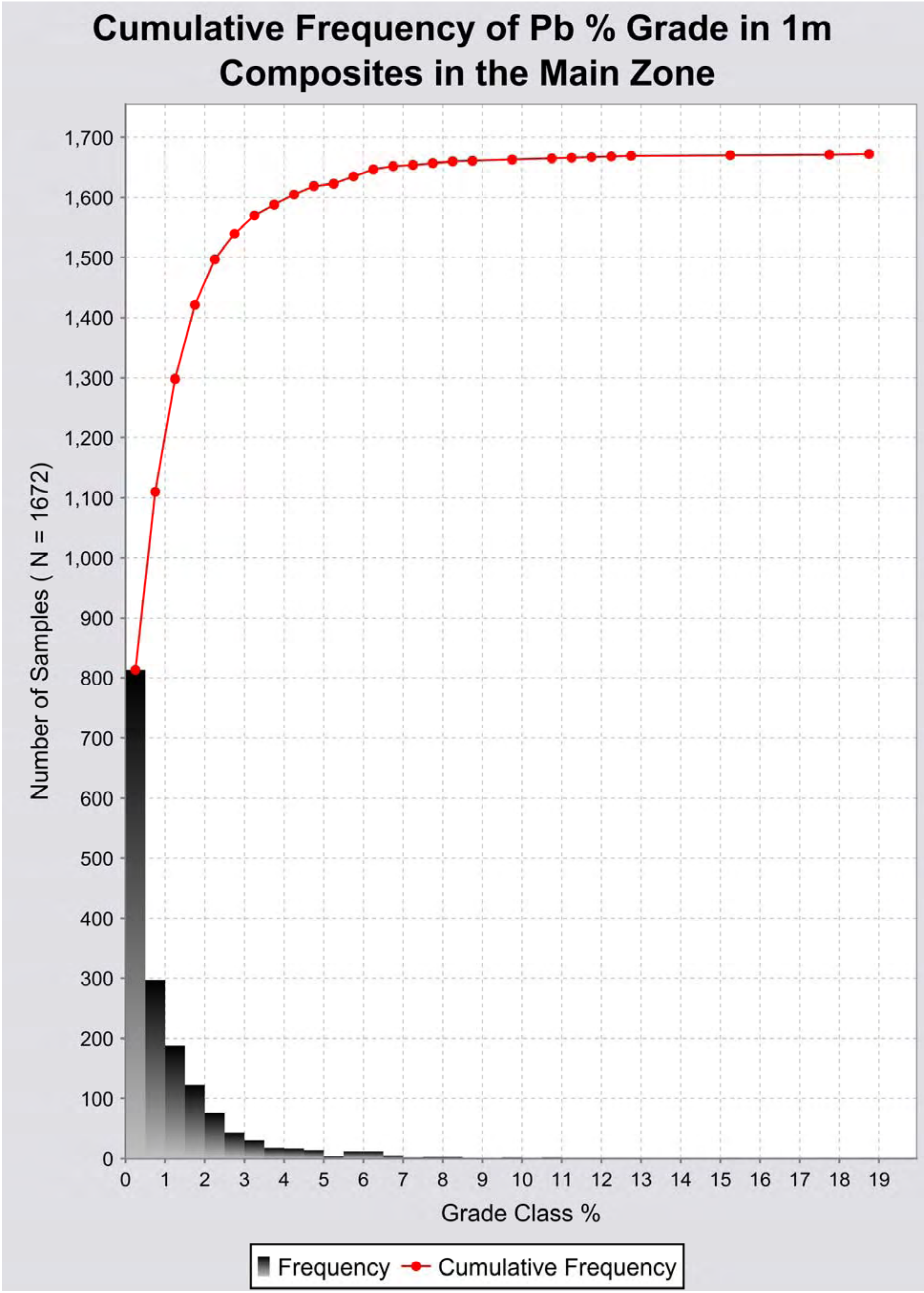

Probability Plot of Pb % Block Grade in Southwest Zone
Prob. Plot
0.999
0.99
0.95
0.84
0.5
0.16
0.0 0.5 1.0 1.5 2.0 2.5 3.0 3.5 4.0 4.5 5.0 5.5 6.0 6.5 7.0 7.5
Grade Class %
Prob. Plot

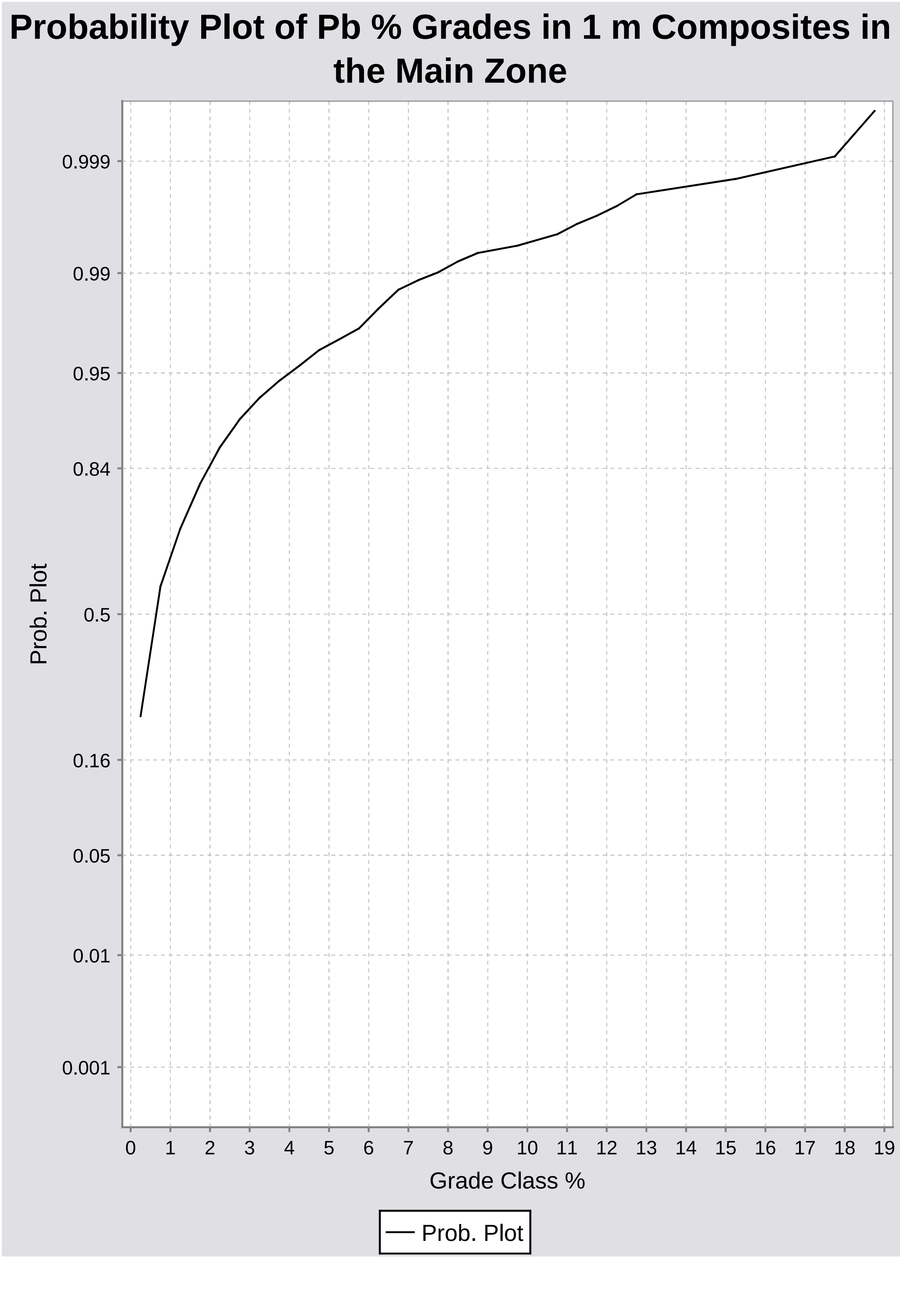

Cumulative Frequency of Zn % Block Grade in Main Zone
Number of Samples (N=174385)
180,000
170,000
160,000
150,000
140,000
130,000
120,000
110,000
100,000
90,000
80,000
70,000
60,000
50,000
40,000
30,000
20,000
10,000
0
0
1
2
3
4
5
6
7
8
9
10
11
Grade Class %
Frequency
Cumulative Frequency


Probability Plot of Zn % Block Grade in Main Zone
0.999
0.99
0.95
0.84
0.5
0.16
0.05
0.01
0.001
Prob. Plot
0
1
2
3
4
5
6
7
8
9
10
Grade Class %
Prob. Plot

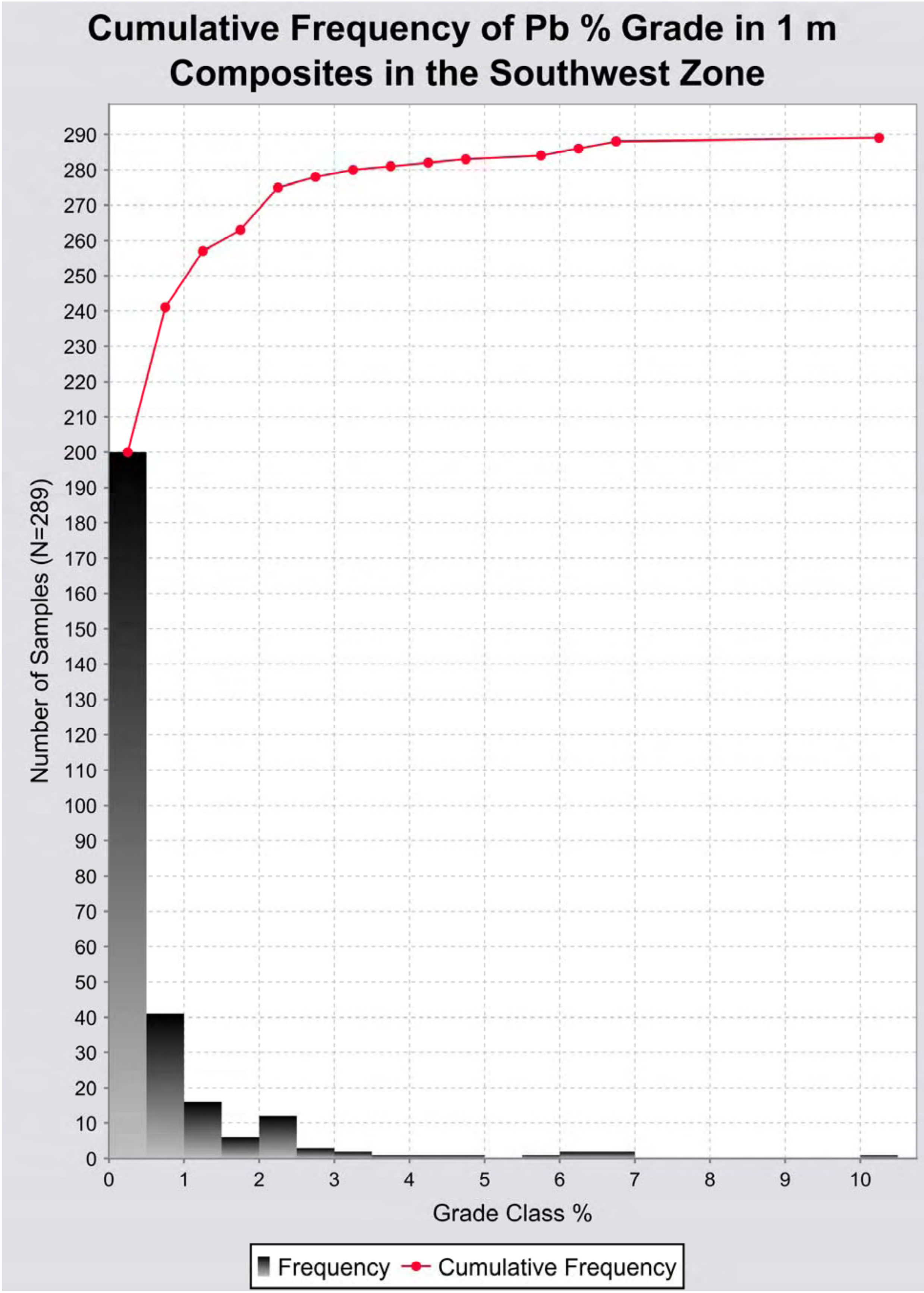

Cumulative Frequency of Zn % Block Grade in Southwest Zone
Number of Samples (N=29839)
30,000
29,000
28,000
27,000
26,000
25,000
24,000
23,000
22,000
21,000
20,000
19,000
18,000
17,000
16,000
15,000
14,000
13,000
12,000
11,000
10,000
9,000
8,000
7,000
6,000
5,000
4,000
3,000
2,000
1,000
0
0.5
1.0
1.5
2.0
2.5
3.0
3.5
4.0
Grade Class %
Frequency
Cumulative Frequency

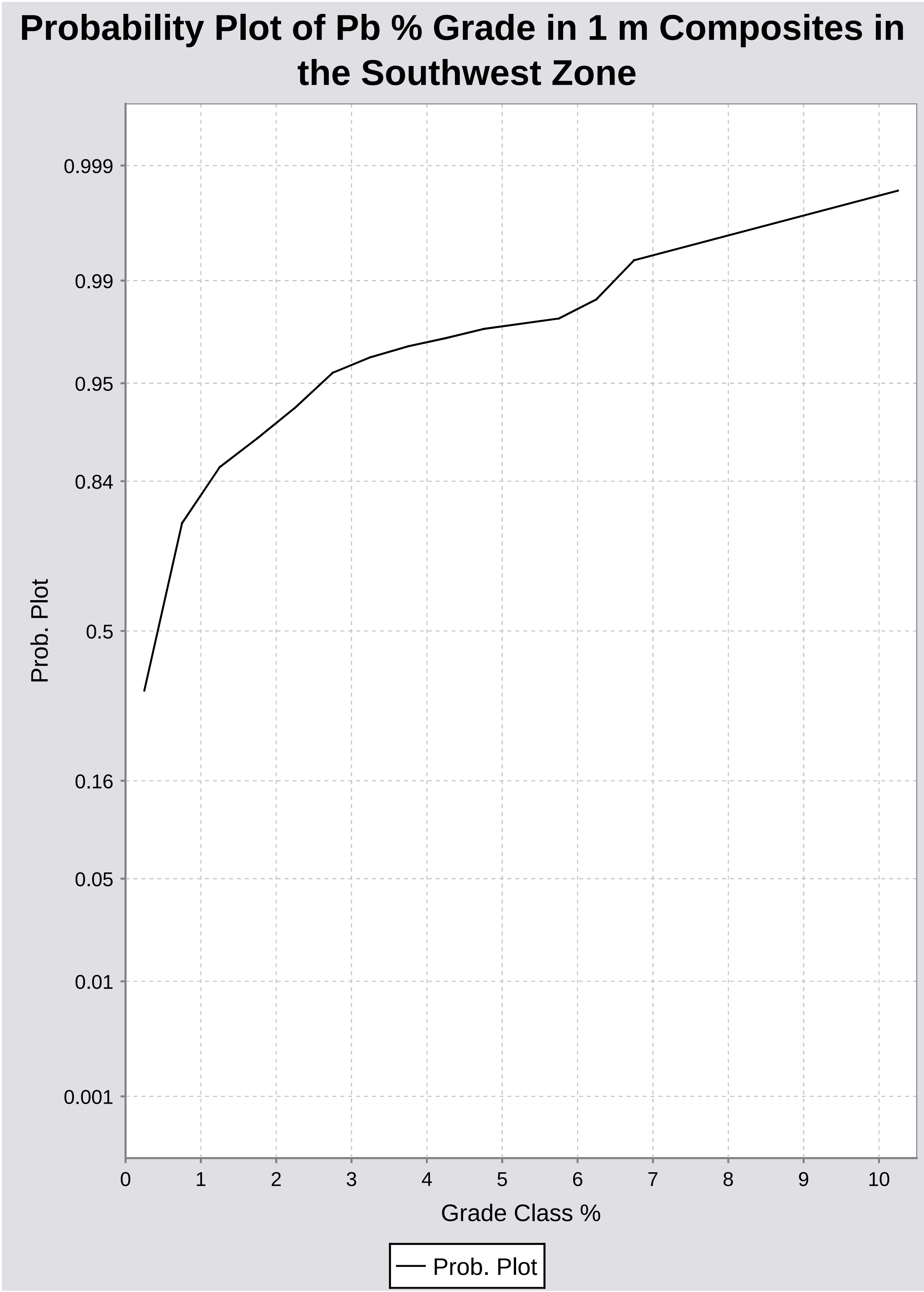

Probability Plot of Zn % Block Grade in Southwest Zone
Prob. Plot
0.999
0.99
0.95
0.84
0.5
0.16
0.05
0.01
0.5
1.0
1.5
2.0
2.5
3.0
3.5
Grade Class %
Prob. Plot

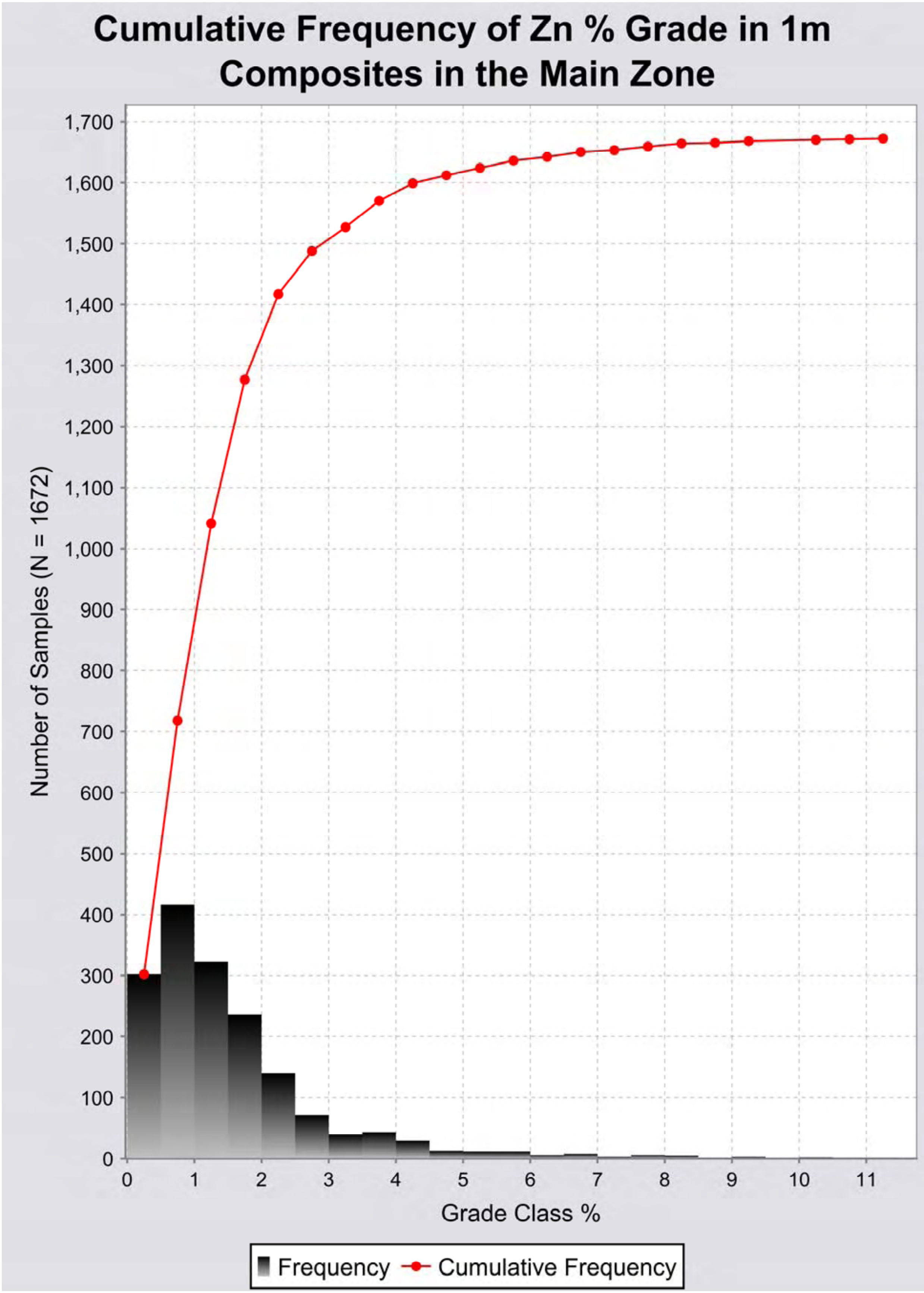

Cumulative Frequency of Pb % Grade in 1m Composites in the Main Zone
Number of Samples (N = 1672)
Grade Class %
Frequency
Cumulative Frequency
0
100
200
300
400
500
600
700
800
900
1,000
1,100
1,200
1,300
1,400
1,500
1,600
1,700
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19

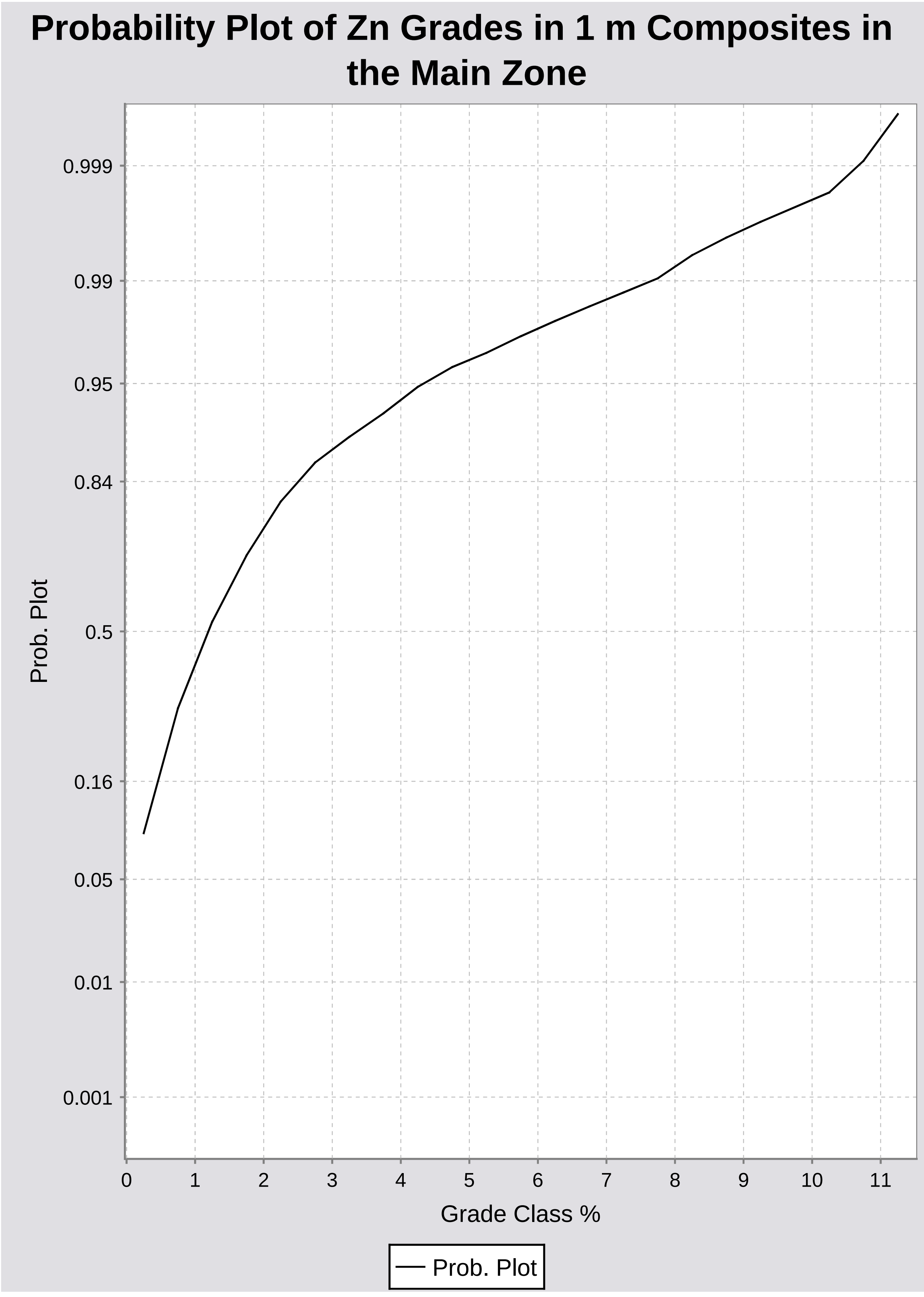


Probability Plot of Pb % Grades in 1 m Composites in the Main Zone
Prob. Plot
0.999
0.99
0.95
0.84
0.5
0.16
0.05
0.01
0.001
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19
Grade Class %
Prob. Plot

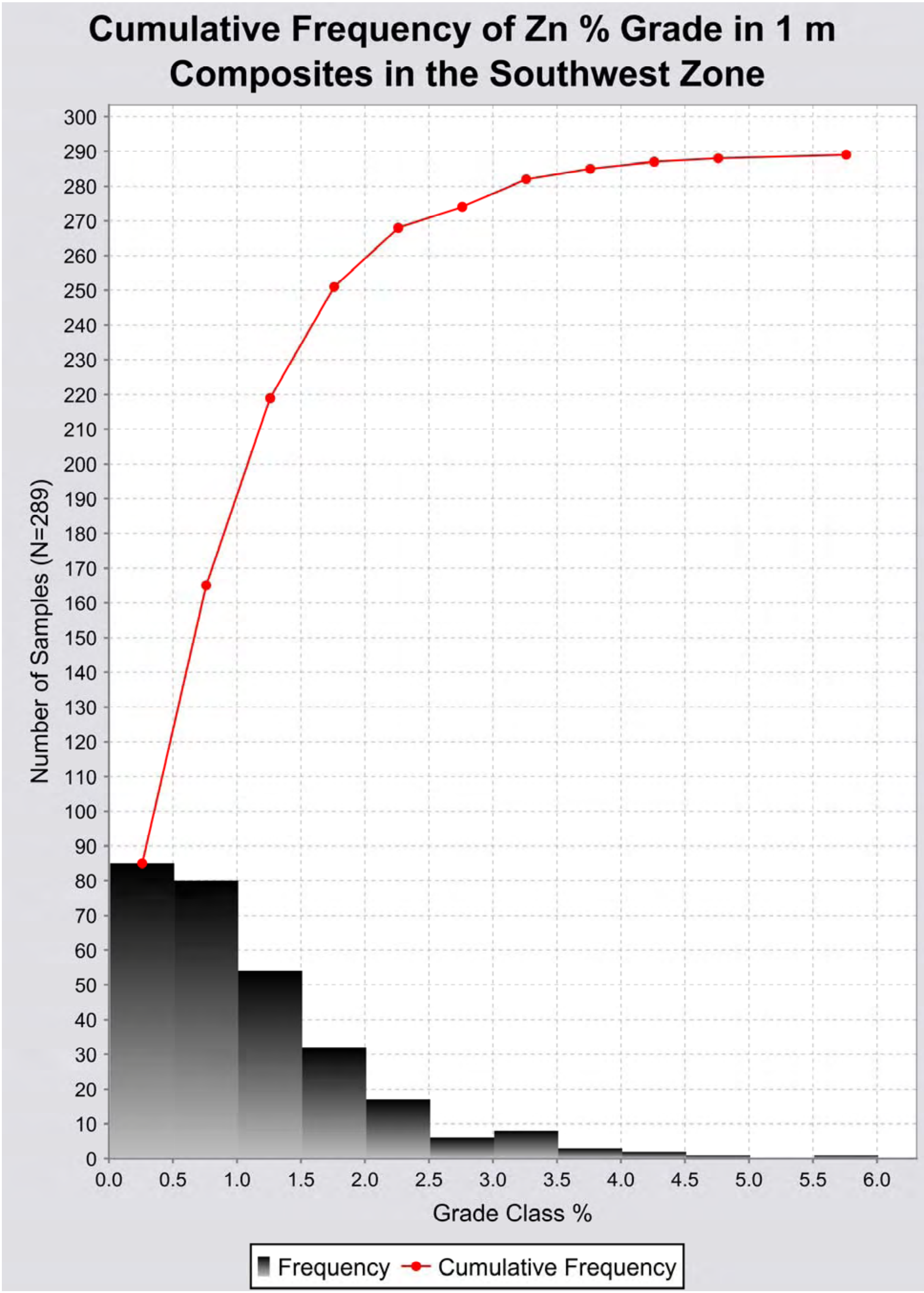

Cumulative Frequency of Pb % Grade in 1 m Composites in the Southwest Zone
Number of Samples (N=289)
Grade Class %
Frequency
Cumulative Frequency


Probability Plot of Pb % Grade in 1 m Composites in the Southwest Zone
Prob. Plot
0.999
0.99
0.95
0.84
0.5
0.16
0.05
0.01
0.001
0
1
2
3
4
5
6
7
8
9
10
Grade Class %
Prob. Plot


Cumulative Frequency of Zn % Grade in 1m Composites in the Main Zone
Number of Samples (N = 1672)
Grade Class %
1,700
1,600
1,500
1,400
1,300
1,200
1,100
1,000
900
800
700
600
500
400
300
200
100
0
0 1 2 3 4 5 6 7 8 9 10 11
Frequency
Cumulative Frequency

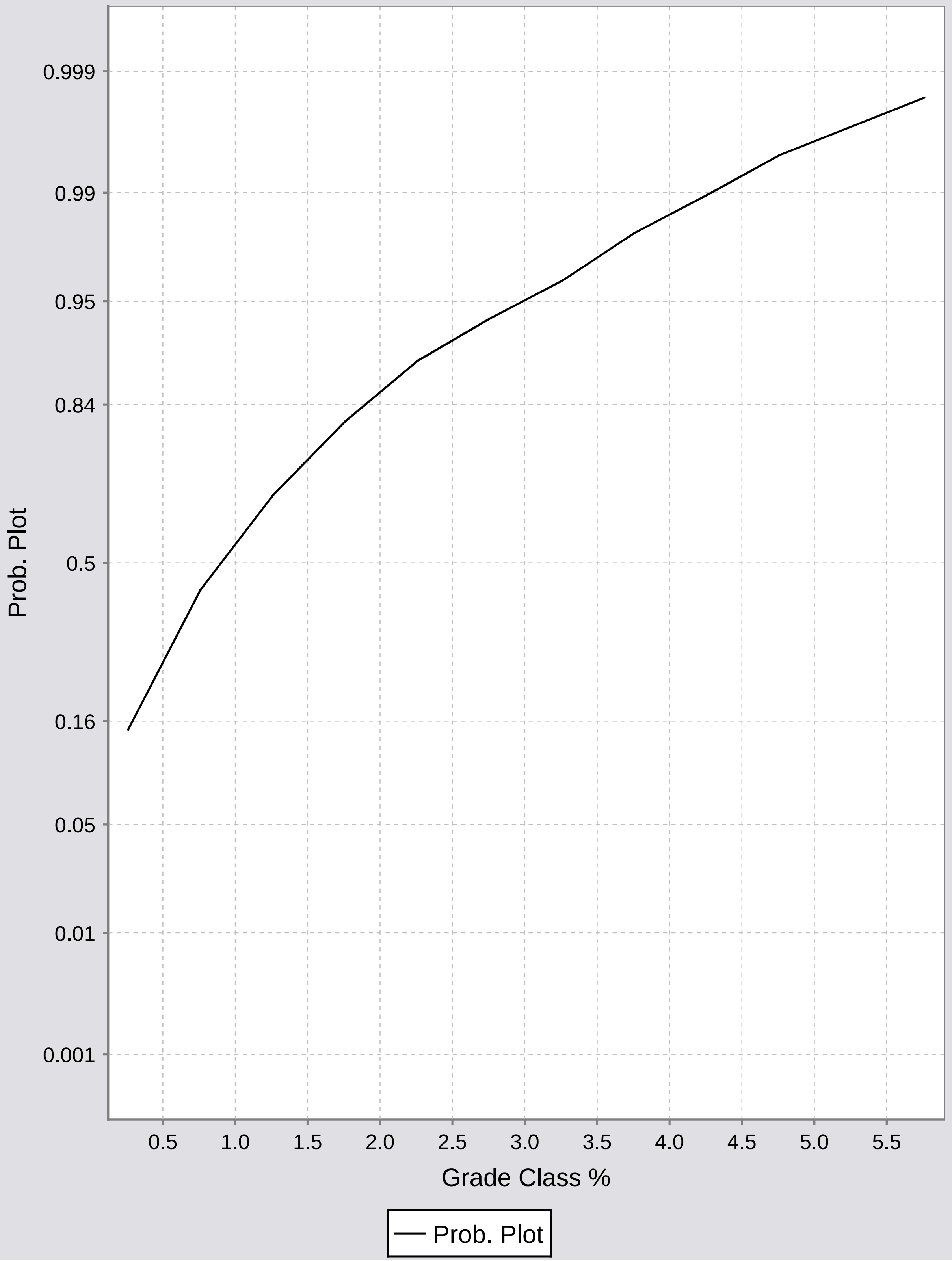


Probability Plot of Zn Grades in 1 m Composites in the Main Zone
Prob. Plot
0.999
0.99
0.95
0.84
0.5
0.16
0.05
0.01
0.001
0
1
2
3
4
5
6
7
8
9
10
11
Grade Class %
Prob. Plot



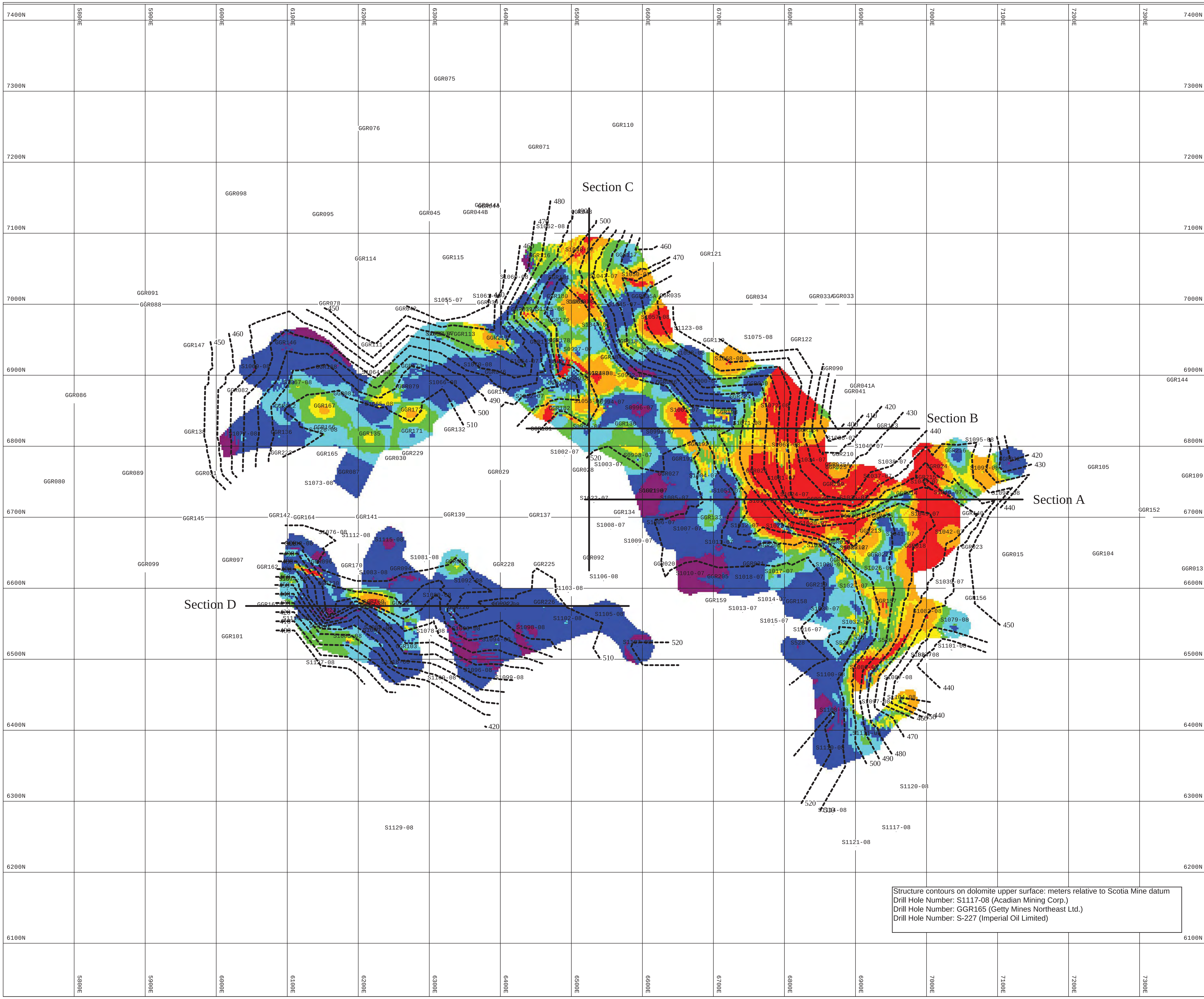
Cumulative Frequency of Zn % Grade in 1 m Composites in the Southwest Zone
Number of Samples (N=289)
300
290
280
270
260
250
240
230
220
210
200
190
180
170
160
150
140
130
120
110
100
90
80
70
60
50
40
30
20
10
0
0.0
0.5
1.0
1.5
2.0
2.5
3.0
3.5
4.0
4.5
5.0
5.5
6.0
Grade Class %
Frequency
Cumulative Frequency

Probability of Zn % Grade in 1 m Composites in the Southwest Zone



Appendix 4: Resource Estimate Plans and Sections

Drill Hole Location And Grade Distribution Plan
Resource Category Plan
Block Model Cross Sections and Level Plans



Block Grade (Zn% + Pb%)

- > 5.00
- 3.50 - 5.00
- 3.00 - 3.50
- 2.50 - 3.00
- 2.00 - 2.50
- 1.00 - 2.00
- 0.01 - 1.00
- < 0.01

Lithology

- Overburden
- Gypsum
- Anhydrite
- Dolomite
- Basal Breccia
- Metasedimentary
- Sulfides
- Void

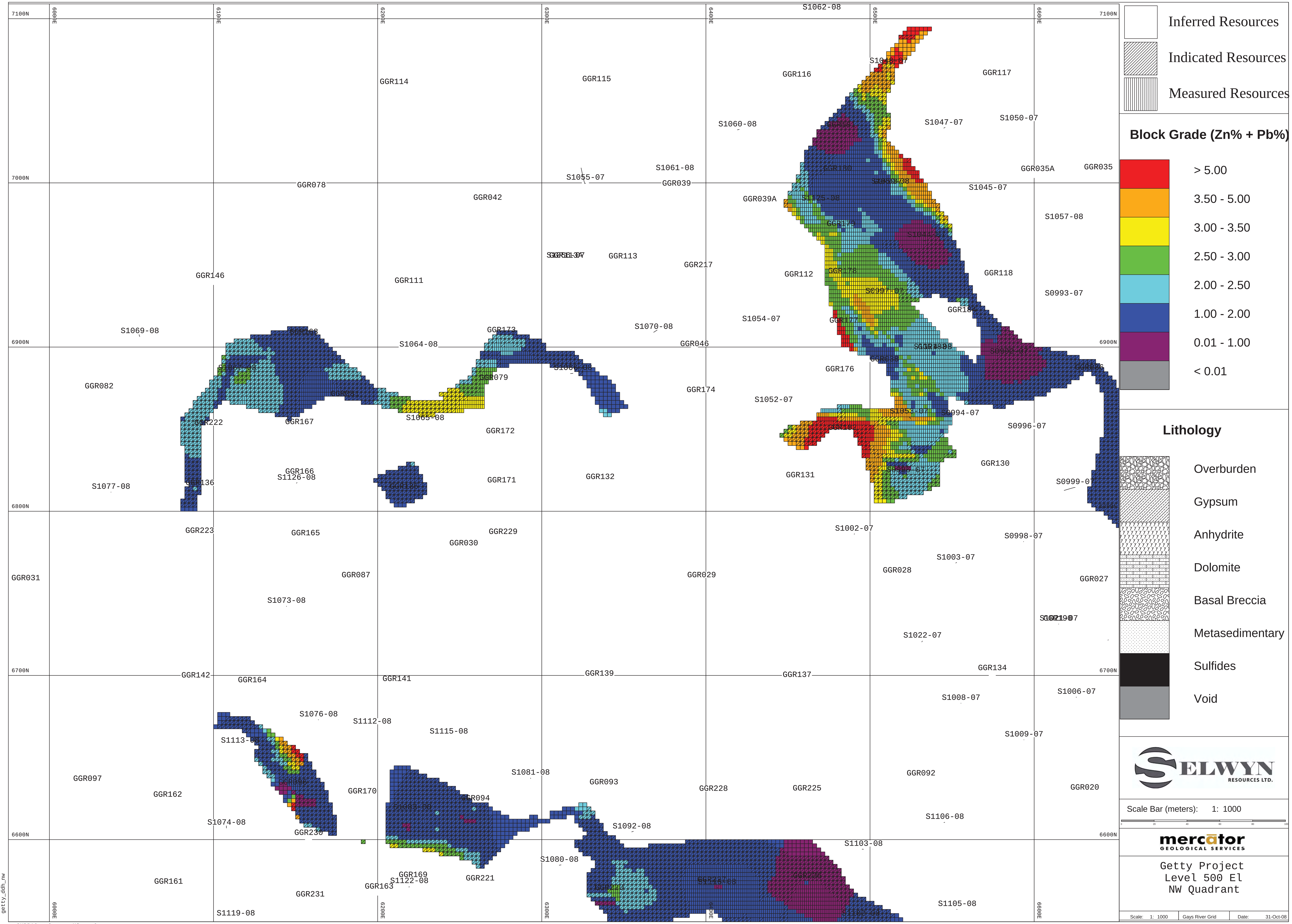
SELWYN RESOURCES LTD.

Scale Bar (meters): 1: 2500

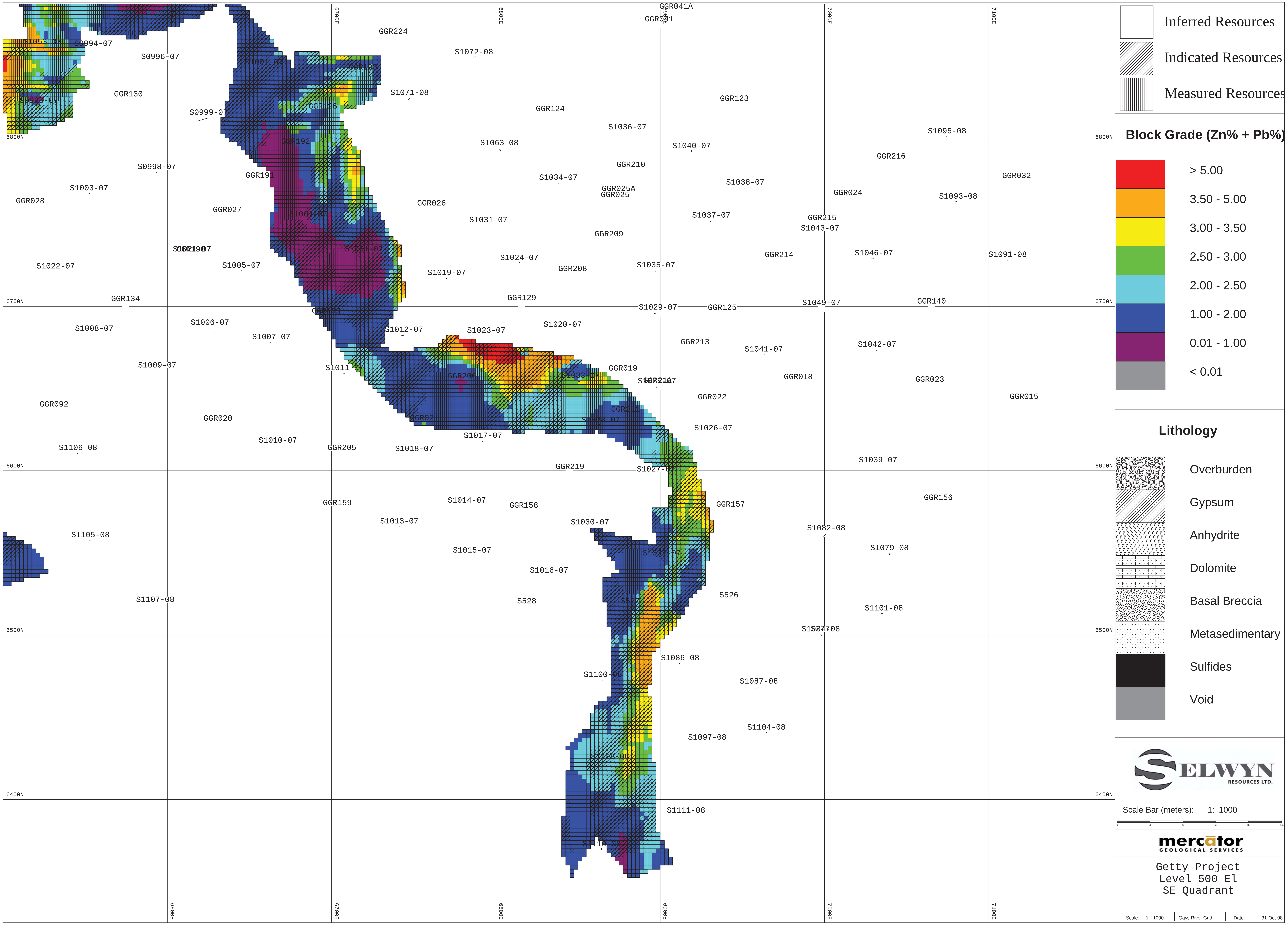
mercator GEOLOGICAL SERVICES

Getty Project
Block Model Level Plan
Resource Classification
Not Represented

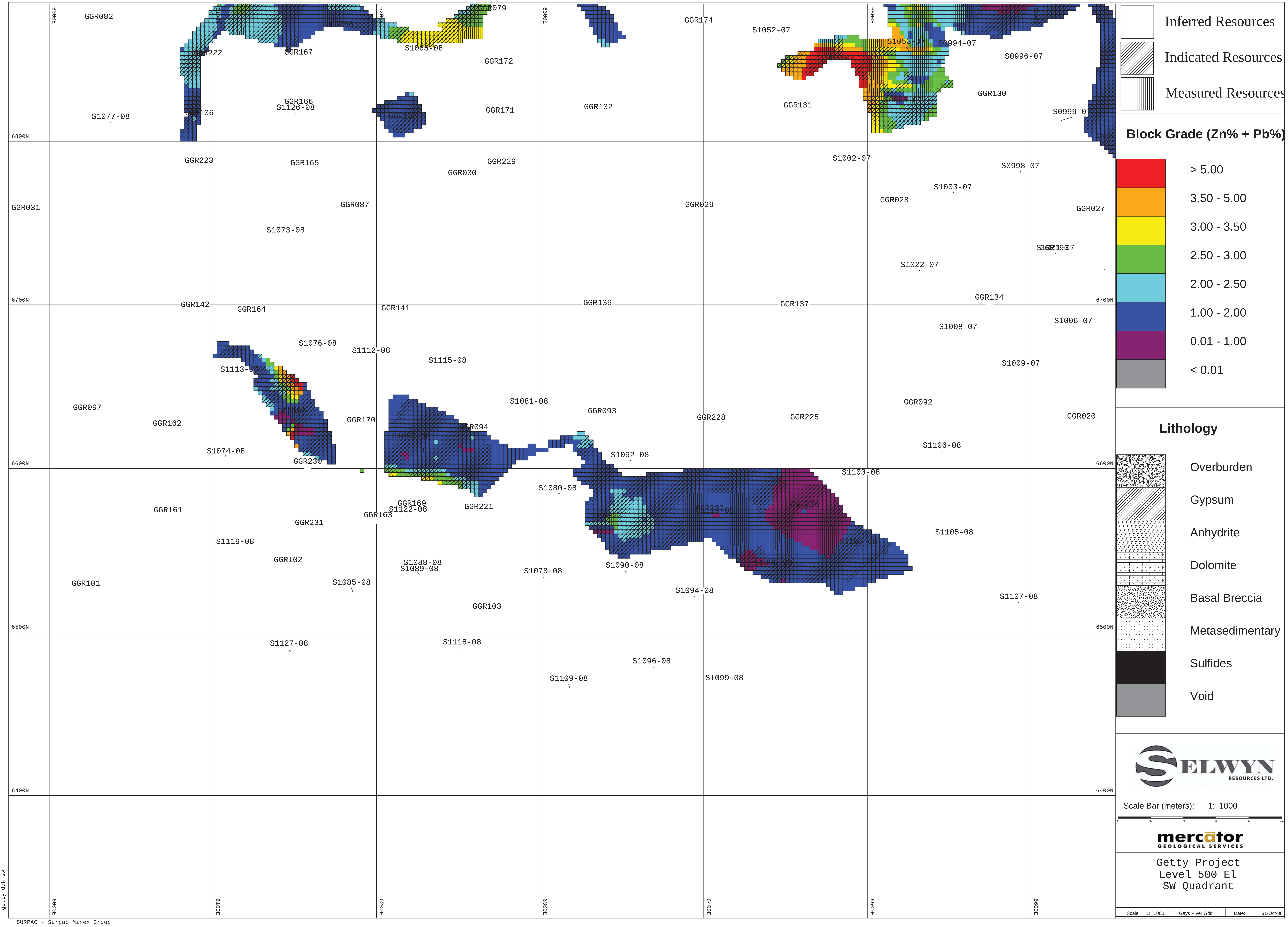
Scale: 1: 2500 | Gays River Grid | Date: 31-Oct-08

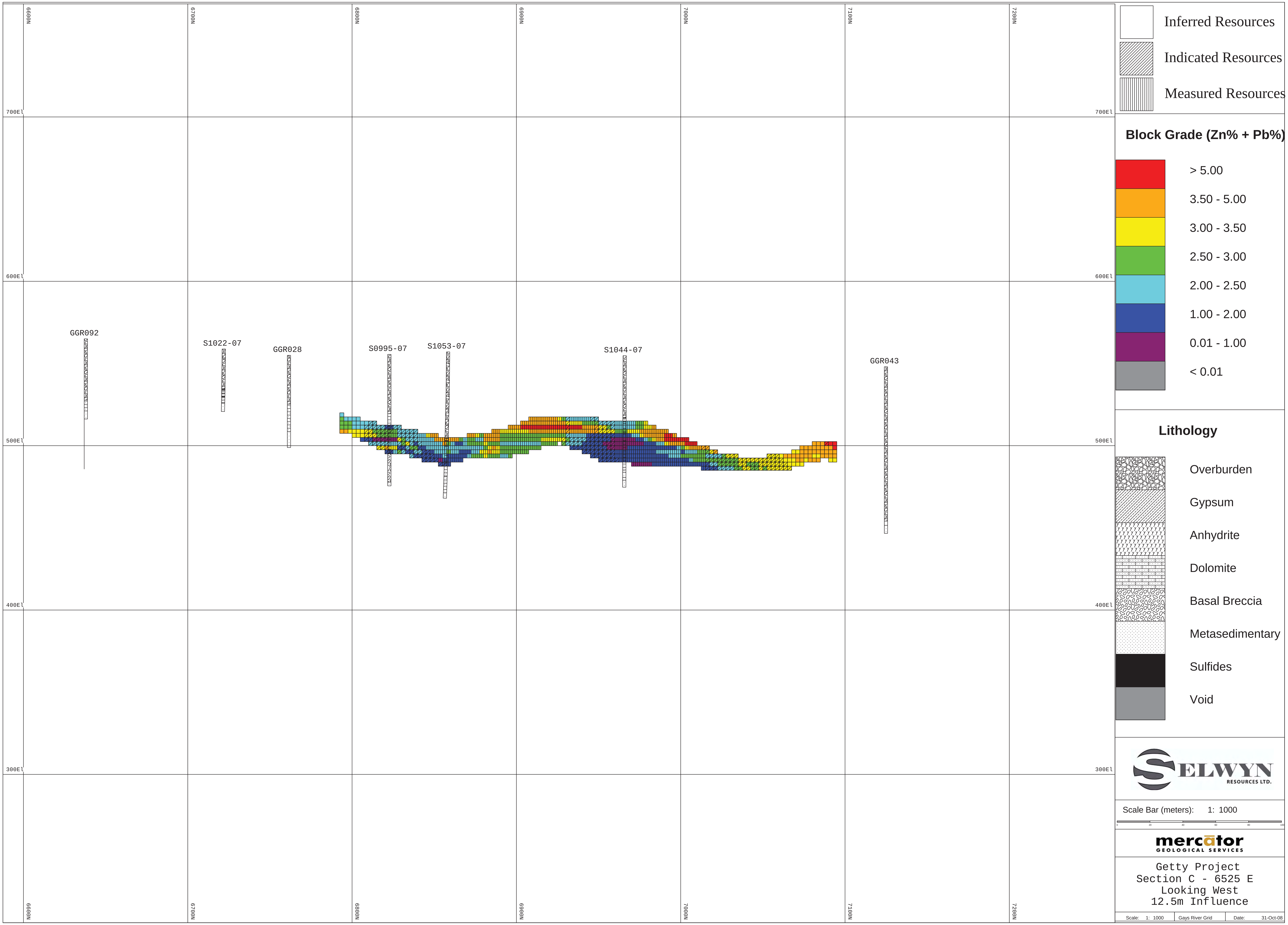


SURPAC - Surpac Minex Group

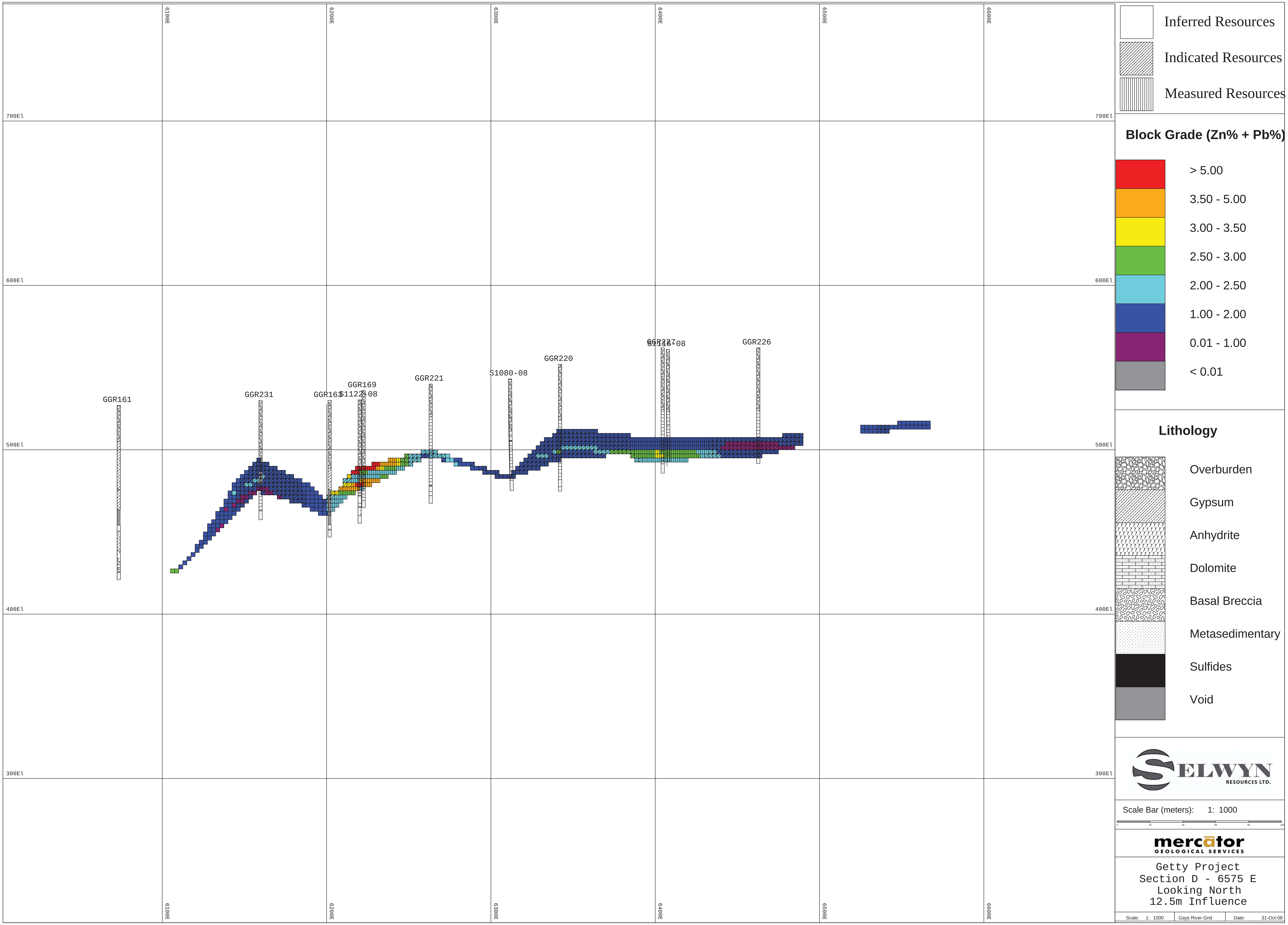


Inferred Resources
Indicated Resources
Measured Resources
Block Grade (Zn% + Pb%)
> 5.00
3.50 - 5.00
3.00 - 3.50
2.50 - 3.00
2.00 - 2.50
1.00 - 2.00
0.01 - 1.00
< 0.01
Lithology
Overburden
Gypsum
Anhydrite
Dolomite
Basal Breccia
Metasedimentary
Sulfides
Void
SELWYN RESOURCES LTD.
Scale Bar (meters): 1: 1000
mercator GEOLOGICAL SERVICES
Getty Project
Level 500 El
SE Quadrant
Scale: 1: 1000
Gays River Grid
Date: 31-Oct-08
6800N
6700N
6600N
6500N
6400N
6600E
6700E
6800E
6900E
7000E
7100E
GGR041A
GGR224
S1072-08
S0994-07
S0996-07
S1071-08
GGR130
GGR124
GGR123
S0999-07
S1036-07
S1095-08
S1063-08
S1040-07
GGR216
S0998-07
GGR210
S1034-07
S1038-07
GGR032
S1003-07
GGR025A
GGR025
GGR024
S1093-08
GGR028
GGR027
GGR026
S1031-07
S1037-07
GGR215
S1043-07
GGR209
S1005-07
S1024-07
S1046-07
S1022-07
S1019-07
GGR208
S1035-07
GGR214
S1091-08
GGR134
GGR129
S1029-07
GGR125
S1049-07
GGR140
S1008-07
S1006-07
S1007-07
S1012-07
S1023-07
S1020-07
GGR213
S1041-07
S1042-07
S1009-07
S1011-07
GGR019
GGR018
GGR023
GGR022
GGR015
GGR092
GGR020
S1026-07
S1010-07
S1017-07
S1106-08
GGR205
S1018-07
S1039-07
GGR219
S1027-07
GGR159
S1014-07
GGR158
GGR157
GGR156
S1013-07
S1030-07
S1082-08
S1105-08
S1015-07
S1079-08
S1016-07
S1107-08
S528
S526
S1101-08
S1086-08
S1100-08
S1087-08
S1104-08
S1097-08
S1111-08

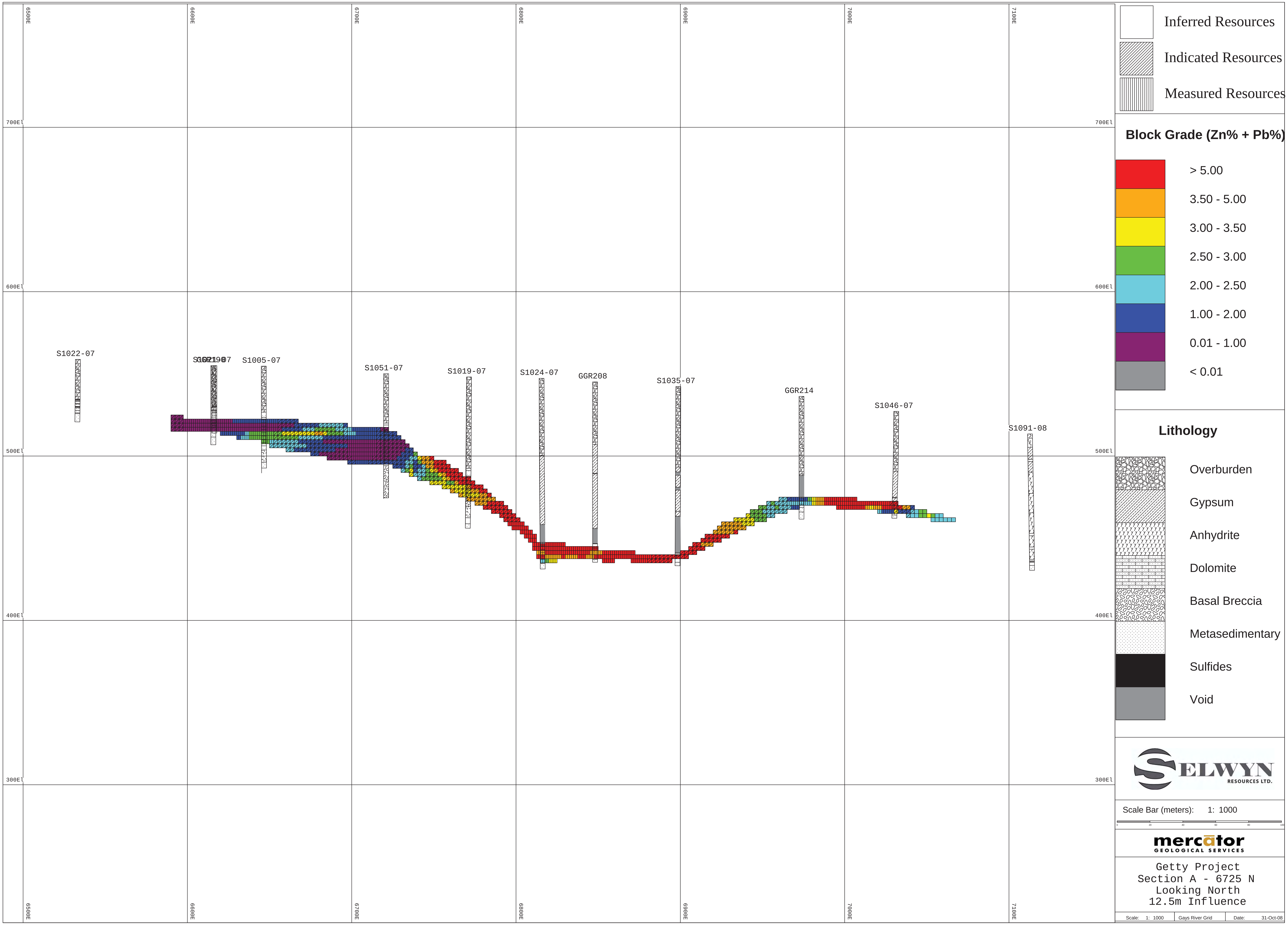

GGR082
GGR079
S1065-08
GGR174
S1052-07
S0994-07
S0996-07
GGR222
GGR167
GGR172
GGR166
S1126-08
S1077-08
GGR136
GGR171
GGR132
GGR131
GGR130
S0999-07
6800N
GGR223
GGR165
GGR229
GGR030
S1002-07
S0998-07
S1003-07
GGR031
GGR087
GGR029
GGR028
GGR027
S1073-08
S1022-07
GGR134
6700N
GGR142
GGR164
GGR141
GGR139
GGR137
S1008-07
S1006-07
S1076-08
S1112-08
S1115-08
S1113-08
S1009-07
S1081-08
GGR097
GGR162
GGR170
GGR094
GGR093
GGR228
GGR225
GGR092
GGR020
S1074-08
GGR230
S1092-08
S1106-08
6600N
S1103-08
S1080-08
GGR161
GGR169
S1122-08
GGR163
GGR221
GGR231
S1105-08
S1119-08
GGR102
S1088-08
S1089-08
S1078-08
S1090-08
GGR101
S1085-08
S1094-08
S1107-08
GGR103
6500N
S1127-08
S1118-08
S1096-08
S1109-08
S1099-08
6400N
6000E
6100E
6200E
6300E
6400E
6500E
6600E
getty_ddh_sw
SURPAC - Surpac Minex Group
Inferred Resources
Indicated Resources
Measured Resources
Block Grade (Zn% + Pb%)
> 5.00
3.50 - 5.00
3.00 - 3.50
2.50 - 3.00
2.00 - 2.50
1.00 - 2.00
0.01 - 1.00
< 0.01
Lithology
Overburden
Gypsum
Anhydrite
Dolomite
Basal Breccia
Metasedimentary
Sulfides
Void
SELWYN RESOURCES LTD.
Scale Bar (meters): 1: 1000
mercator GEOLOGICAL SERVICES
Getty Project
Level 500 El
SW Quadrant
Scale: 1: 1000
Gays River Grid
Date: 31-Oct-08

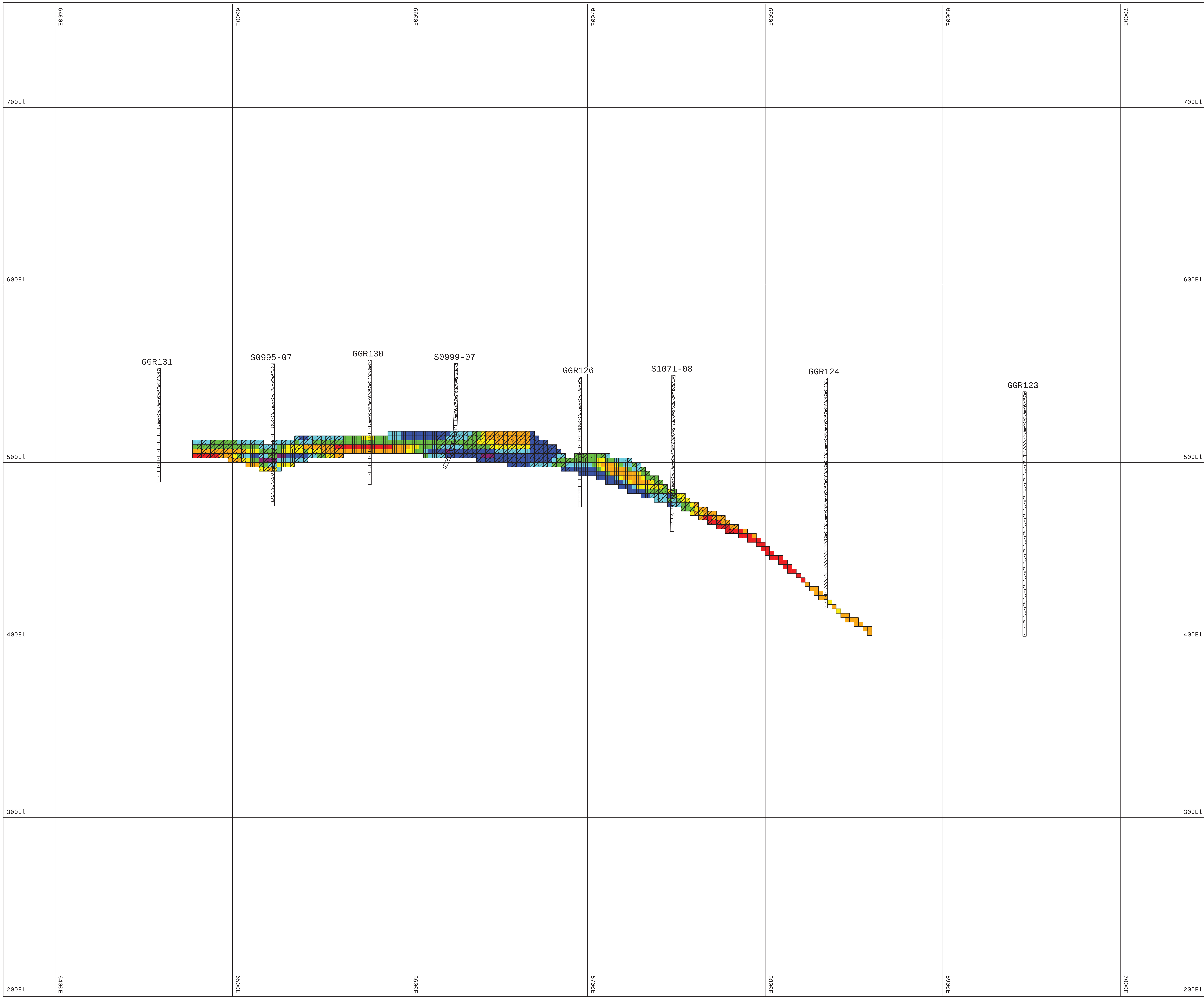


6600N
6700N
6800N
6900N
7000N
7100N
7200N
700El
600El
500El
400El
300El
GGR092
S1022-07
GGR028
S0995-07
S1053-07
S1044-07
GGR043
Inferred Resources
Indicated Resources
Measured Resources
Block Grade (Zn% + Pb%)
> 5.00
3.50 - 5.00
3.00 - 3.50
2.50 - 3.00
2.00 - 2.50
1.00 - 2.00
0.01 - 1.00
< 0.01
Lithology
Overburden
Gypsum
Anhydrite
Dolomite
Basal Breccia
Metasedimentary
Sulfides
Void
SELWYN
RESOURCES LTD.
Scale Bar (meters): 1: 1000
mercator
GEOLOGICAL SERVICES
Getty Project
Section C - 6525 E
Looking West
12.5m Influence
Scale: 1: 1000
Gays River Grid
Date: 31-Oct-08



6100E
6200E
6300E
6400E
6500E
6600E
700El
600El
500El
400El
300El
GGR161
GGR231
GGR163
S1122-08
GGR169
GGR221
S1080-08
GGR220
GGR227
S1116-08
GGR226
Inferred Resources
Indicated Resources
Measured Resources
Block Grade (Zn% + Pb%)
> 5.00
3.50 - 5.00
3.00 - 3.50
2.50 - 3.00
2.00 - 2.50
1.00 - 2.00
0.01 - 1.00
< 0.01
Lithology
Overburden
Gypsum
Anhydrite
Dolomite
Basal Breccia
Metasedimentary
Sulfides
Void
SELWYN RESOURCES LTD.
Scale Bar (meters): 1: 1000
mercator GEOLOGICAL SERVICES
Getty Project
Section D - 6575 E
Looking North
12.5m Influence
Scale: 1: 1000
Gays River Grid
Date: 31-Oct-08


6500E
6600E
6700E
6800E
6900E
7000E
7100E
700El
600El
500El
400El
300El
S1022-07
S1005-07
S1051-07
S1019-07
S1024-07
GGR208
S1035-07
GGR214
S1046-07
S1091-08
Inferred Resources
Indicated Resources
Measured Resources
Block Grade (Zn% + Pb%)
> 5.00
3.50 - 5.00
3.00 - 3.50
2.50 - 3.00
2.00 - 2.50
1.00 - 2.00
0.01 - 1.00
< 0.01
Lithology
Overburden
Gypsum
Anhydrite
Dolomite
Basal Breccia
Metasedimentary
Sulfides
Void
SELWYN
RESOURCES LTD.
Scale Bar (meters): 1: 1000
mercator
GEOLOGICAL SERVICES
Getty Project
Section A - 6725 N
Looking North
12.5m Influence
Scale: 1: 1000
Gays River Grid
Date: 31-Oct-08



Inferred Resources

Indicated Resources

Measured Resources

Block Grade (Zn% + Pb%)

- > 5.00
- 3.50 - 5.00
- 3.00 - 3.50
- 2.50 - 3.00
- 2.00 - 2.50
- 1.00 - 2.00
- 0.01 - 1.00
- < 0.01

Lithology

- Overburden
- Gypsum
- Anhydrite
- Dolomite
- Basal Breccia
- Metasedimentary
- Sulfides
- Void

SELWYN RESOURCES LTD.

Scale Bar (meters): 1: 1000

mercator GEOLOGICAL SERVICES

Getty Project
Section B - 6825 N
Looking North
12.5m Influence

Scale: 1: 1000	Gays River Grid	Date: 31-Oct-08